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**Morton et al.**

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(54) **COMPACT MOBILE CARGO SCANNING SYSTEM**

(71) Applicant: **Rapiscan Systems, Inc.**, Torrance, CA (US)

(72) Inventors: **Edward James Morton**, Guildford (GB); **Francis Baldwin**, Petersfield (GB); **Andreas F. Kotowski**, Rancho Palos Verdes, CA (US)

(73) Assignee: **Rapiscan Systems, Inc.**, Torrance, CA (US)

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(56) **References Cited**  
**U.S. PATENT DOCUMENTS**  
  
2,420,845 A 5/1947 Slack  
2,636,619 A 4/1953 Alexander  
(Continued)

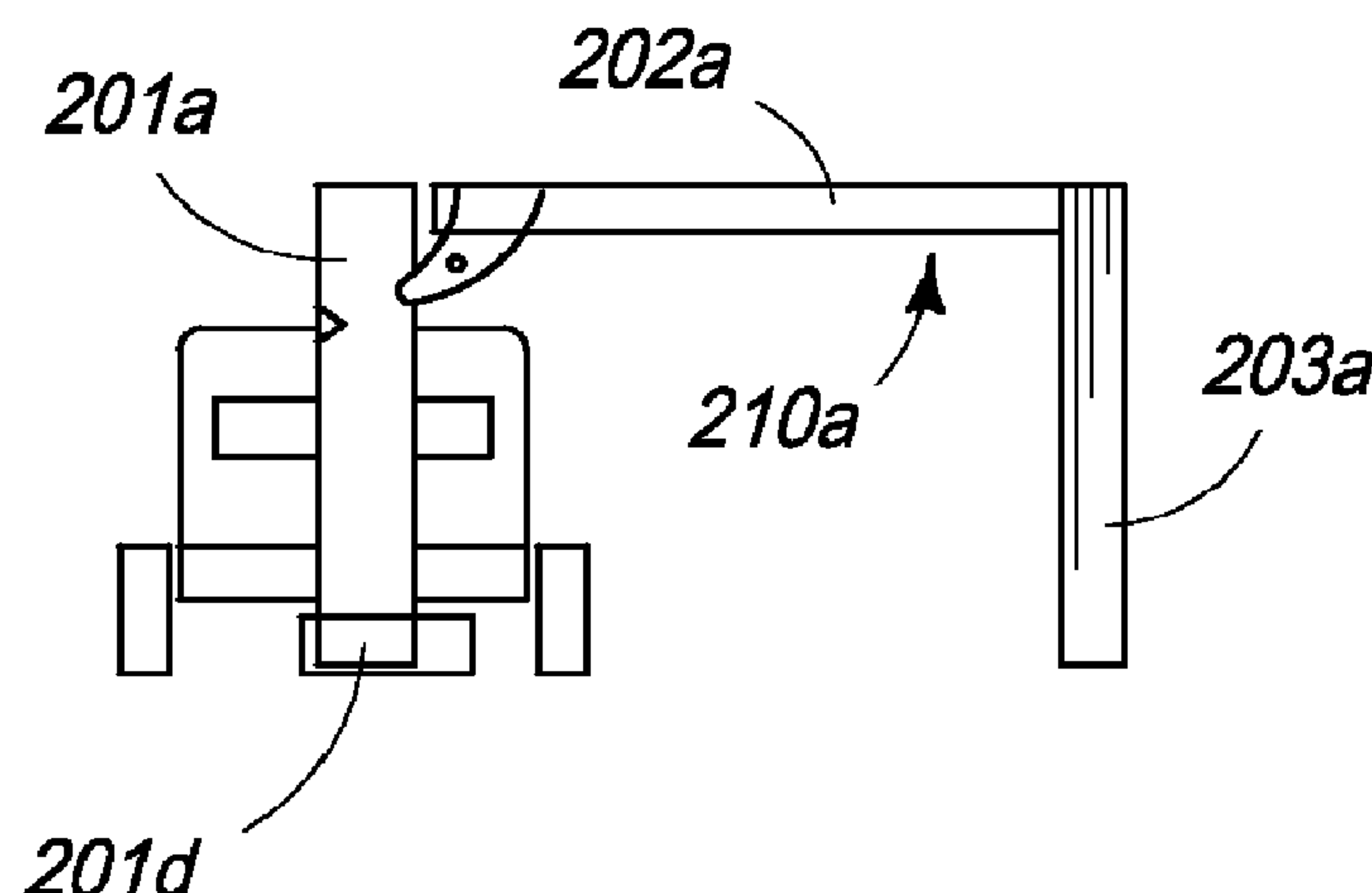
**FOREIGN PATENT DOCUMENTS**  
  
DE 2729353 A1 1/1979  
DE 3214910 A1 5/1983  
(Continued)

**OTHER PUBLICATIONS**  
  
US 5,987,079, 11/1999, Scott (withdrawn)  
(Continued)

*Primary Examiner* — Irakli Kiknadze  
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(57) **ABSTRACT**  
  
The present invention is a self-contained mobile inspection system and method and, more specifically, improved methods and systems for detecting materials concealed within a wide variety of receptacles and/or cargo containers. In particular, the present invention is an improved method and system with a novel boom structure that reduces the weight of the boom. The single, light-weight boom of the inspection system is relatively compact in a stowed configuration and has a low height and center of gravity lending to greater maneuverability.

**20 Claims, 18 Drawing Sheets**



**Related U.S. Application Data**

continuation of application No. 13/598,945, filed on Aug. 30, 2012, now Pat. No. 8,668,386, which is a continuation of application No. 12/784,630, filed on May 21, 2010, now Pat. No. 8,275,091, which is a continuation-in-part of application No. 12/339,591, filed on Dec. 19, 2008, now Pat. No. 7,963,695, which is a continuation-in-part of application No. 11/948,814, filed on Nov. 30, 2007, now Pat. No. 7,517,149, which is a continuation of application No. 10/915,687, filed on Aug. 9, 2004, now Pat. No. 7,322,745, which is a continuation-in-part of application No. 10/201,543, filed on Jul. 23, 2002, now Pat. No. 6,843,599, said application No. 12/339,591 is a continuation-in-part of application No. 12/051,910, filed on Mar. 20, 2008, now Pat. No. 7,519,148, which is a continuation of application No. 11/622,560, filed on Jan. 12, 2007, now Pat. No. 7,369,643, which is a continuation-in-part of application No. 10/915,687, said application No. 12/784,360 is a continuation-in-part of application No. 12/263,160, filed on Oct. 31, 2008, now Pat. No. 7,783,004, which is a continuation-in-part of application No. 10/915,687, said application No. 12/784,630 is a continuation-in-part of application No. 12/349,534, filed on Jan. 7, 2009, now Pat. No. 7,720,195, which is a continuation of application No. 10/939,986, filed on Sep. 13, 2004, now Pat. No. 7,486,768, which is a continuation-in-part of application No. 10/915,687.

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(58) **Field of Classification Search**

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See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

2,831,123 A 4/1958 Daly  
2,885,069 A 5/1959 Bowen  
2,952,790 A 9/1960 Steen  
2,971,433 A 2/1961 Akin  
3,032,207 A \* 5/1962 McIntyre ..... B66C 23/54  
212/238

3,056,510 A *	10/1962	Garnett .....	B66C 23/36 182/2.11
3,070,399 A	12/1962	Bartlett	
3,073,960 A	1/1963	Guentner	
3,146,349 A	8/1964	Jordan	
3,239,706 A	3/1966	Farrell	
3,275,831 A	9/1966	Martin	
3,374,355 A	3/1968	Parratt	
3,458,026 A	7/1969	Lauzon	
3,485,339 A	12/1969	Miller	
3,676,783 A	7/1972	Kinbara	
3,766,387 A	10/1973	Heffan	
3,767,850 A	10/1973	Mc	
3,768,645 A	10/1973	Conway	
3,770,955 A	11/1973	Tomita	
3,784,837 A	1/1974	Holmstrom	
3,837,502 A	9/1974	Hornagold	
3,904,923 A	9/1975	Schwartz	
3,919,467 A	11/1975	Peugeot	
3,955,678 A	5/1976	Moyer	
3,958,377 A *	5/1976	Milner, Jr. ....	B66F 11/044 182/2.8
3,961,186 A	6/1976	Leunbach	
3,980,889 A	9/1976	Haas	
4,047,035 A	9/1977	Dennhoven	
4,057,725 A	11/1977	Wagner	
4,064,440 A	12/1977	Roder	
4,105,922 A	8/1978	Lambert	
4,139,771 A	2/1979	Dennhoven	
4,164,138 A	8/1979	Burkhart	
4,210,811 A	7/1980	Dennhoven	
4,216,499 A	8/1980	Dennhoven	
4,228,353 A	10/1980	Johnson	
4,259,721 A	3/1981	Kuznia	
4,266,425 A	5/1981	Allport	
4,274,005 A	6/1981	Yamamura	
4,340,816 A	7/1982	Schott	
4,352,021 A	9/1982	Boyd	
4,366,382 A	12/1982	Kotowski	
4,380,817 A	4/1983	Harding	
4,430,568 A	2/1984	Yoshida	
4,468,802 A	8/1984	Friedel	
4,481,403 A	11/1984	Del	
4,501,011 A	2/1985	Hauck	
4,525,854 A	6/1985	Molbert	
4,563,707 A	1/1986	Kishida	
4,566,113 A	1/1986	Doenges	
4,599,740 A	7/1986	Cable	
4,602,462 A *	7/1986	Anderson .....	B66F 11/044 182/2.9
4,626,688 A	12/1986	Barnes	
4,641,330 A	2/1987	Herwig	
4,672,649 A	6/1987	Rutt	
4,675,890 A	6/1987	Plessis	
4,709,382 A	11/1987	Sones	
4,736,401 A	4/1988	Donges	
4,752,948 A	6/1988	MacMahon	
4,788,704 A	11/1988	Donges	
4,799,247 A	1/1989	Annis	
4,809,312 A	2/1989	Annis	
4,809,857 A	3/1989	Steuck	
4,817,123 A	3/1989	Sones	
4,825,454 A	4/1989	Annis	
4,831,260 A	5/1989	DiBianca	
RE32,961 E	6/1989	Wagner	
4,853,595 A	8/1989	Alfano	
4,864,142 A	9/1989	Gomberg	
4,866,439 A	9/1989	Kraus	
4,866,745 A	9/1989	Akai	
4,868,856 A	9/1989	Frith	
4,870,670 A	9/1989	Geus	
4,872,188 A	10/1989	Lauro	
4,879,735 A	11/1989	Owens	
4,884,289 A	11/1989	Glockmann	
4,887,604 A	12/1989	Shefer	
4,979,137 A	12/1990	Gerstenfeld	
4,979,202 A	12/1990	Siczek	
4,987,584 A	1/1991	Doenges	
4,991,189 A	2/1991	Boomgaarden	



# US 10,007,019 B2

Page 3

(56)

## References Cited

### U.S. PATENT DOCUMENTS

4,991,708 A	2/1991	Francioni	5,738,202 A	4/1998	Ydoate
5,006,299 A	4/1991	Gozani	5,744,919 A	4/1998	Mishin
5,014,293 A	5/1991	Boyd	5,751,837 A	5/1998	Watanabe
5,016,767 A *	5/1991	Thibault	5,763,886 A	6/1998	Schulte
		..... B66F 11/044	5,764,683 A	6/1998	Swift
		182/2.9	5,768,334 A	6/1998	Maitrejean
5,022,062 A	6/1991	Annis	5,787,145 A	7/1998	Geus
5,033,106 A	7/1991	Kita	5,796,802 A	8/1998	Gordon
5,040,199 A	8/1991	Stein	5,805,660 A	9/1998	Perion
5,065,418 A	11/1991	Bermbach	5,818,897 A	10/1998	Gordon
5,067,145 A	11/1991	Siczek	5,826,666 A *	10/1998	Tozawa
5,076,993 A	12/1991	Sawa			..... E02F 3/437
5,086,300 A	2/1992	Ash more			172/2
5,091,924 A	2/1992	Bermbach	5,838,758 A	11/1998	Krug
5,092,451 A	3/1992	Jones	5,838,759 A	11/1998	Armistead
5,097,939 A	3/1992	Shanklin	5,841,831 A	11/1998	Hell
5,098,640 A	3/1992	Gozani	5,859,891 A	1/1999	Hibbard
5,114,662 A	5/1992	Gozani	5,870,449 A	2/1999	Lee
5,144,191 A	9/1992	Jones	5,881,122 A	3/1999	Crawford
5,179,581 A	1/1993	Annis	5,882,206 A	3/1999	Gillio
5,181,234 A	1/1993	Smith	5,887,047 A	3/1999	Bailey
5,182,764 A	1/1993	Peschmann	5,901,198 A	5/1999	Crawford
5,185,778 A	2/1993	Magram	5,903,623 A	5/1999	Swift
5,202,932 A	4/1993	Cambier	5,905,806 A	5/1999	Eberhard
5,221,843 A	6/1993	Alvarez	5,909,477 A	6/1999	Crawford
5,224,144 A	6/1993	Annis	5,909,478 A	6/1999	Polichar
5,237,598 A	8/1993	Albert	5,910,973 A	6/1999	Grodzins
5,243,693 A	9/1993	Maron	5,930,326 A	7/1999	Rothschild
5,247,556 A	9/1993	Eckert	5,940,468 A	8/1999	Huang
5,247,561 A	9/1993	Kotowski	5,949,811 A	9/1999	Baba
5,253,283 A	10/1993	Annis	5,949,842 A	9/1999	Schafer
5,259,014 A	11/1993	Brettschneider	5,963,211 A	10/1999	Oikawa
5,260,983 A	11/1993	Ono	5,966,422 A	10/1999	Dafni
5,272,627 A	12/1993	Maschhoff	5,970,113 A	10/1999	Crawford
5,313,511 A	5/1994	Annis	5,974,111 A	10/1999	Krug
5,319,547 A	6/1994	Krug	5,982,843 A	11/1999	Bailey
5,321,271 A	6/1994	Schonberg	5,987,097 A	11/1999	Salasoo
5,341,916 A	8/1994	Doane	6,018,562 A	1/2000	Willson
5,367,552 A	11/1994	Peschmann	6,021,174 A	2/2000	Campbell
5,379,334 A	1/1995	Zimmer	6,026,143 A	2/2000	Simanovsky
5,394,454 A	2/1995	Harding	6,026,171 A	2/2000	Hiraoglu
5,410,156 A	4/1995	Miller	6,031,888 A	2/2000	Ivan
5,412,702 A	5/1995	Sata	6,031,890 A	2/2000	Bermbach
5,418,372 A	5/1995	Schonberg	6,032,808 A	3/2000	Henson
5,430,787 A	7/1995	Norton	6,035,014 A	3/2000	Hiraoglu
5,467,377 A	11/1995	Dawson	6,037,597 A	3/2000	Karavolos
5,490,196 A	2/1996	Rudich	6,044,353 A	3/2000	Pugliese
5,490,218 A	2/1996	Krug	6,056,671 A	5/2000	Marmer
5,493,596 A	2/1996	Annis	6,058,158 A	5/2000	Eiler
5,505,291 A	4/1996	Huang	6,067,344 A	5/2000	Grodzins
5,511,104 A	4/1996	Mueller	6,067,366 A	5/2000	Simanovsky
5,524,133 A	6/1996	Neale	6,073,751 A	6/2000	Worzishek
5,548,123 A	8/1996	Perez-Mendez	6,075,871 A	6/2000	Simanovsky
5,557,108 A	9/1996	Tumer	6,076,400 A	6/2000	Bechwati
5,590,057 A	12/1996	Fletcher	6,078,642 A	6/2000	Simanovsky
5,600,303 A	2/1997	Husseiny	6,081,580 A	6/2000	Grodzins
5,600,700 A	2/1997	Krug	6,088,423 A	7/2000	Krug
5,604,778 A	2/1997	Polacin	6,091,795 A	7/2000	Schafer
5,606,167 A	2/1997	Miller	6,094,472 A	7/2000	Smith
5,633,907 A	5/1997	Gravelle	6,108,396 A	8/2000	Bechwati
5,634,551 A	6/1997	Francioni	6,111,974 A	8/2000	Hiraoglu
5,638,420 A	6/1997	Armistead	6,118,852 A	9/2000	Rogers
5,638,817 A	6/1997	Morgan	6,122,343 A	9/2000	Pidcock
5,642,393 A	6/1997	Krug	6,128,365 A	10/2000	Bechwati
5,642,394 A	6/1997	Rothschild	6,134,299 A	10/2000	Artig
5,660,549 A	8/1997	Witt	6,137,895 A	10/2000	Al-Sheikh
5,661,377 A	8/1997	Mishin	6,149,592 A	11/2000	Yanof
5,661,774 A	8/1997	Gordon	6,151,381 A	11/2000	Grodzins
5,666,393 A	9/1997	Annis	6,163,591 A	12/2000	Benjamin
5,687,210 A	11/1997	Maitrejean	6,181,765 B1	1/2001	Sribar
5,689,541 A	11/1997	Schardt	6,183,139 B1	2/2001	Solomon
5,692,028 A *	11/1997	Geus	6,185,272 B1	2/2001	Hiraoglu
		..... G01V 5/0008	6,188,745 B1	2/2001	Gordon
		378/196	6,188,747 B1	2/2001	Geus
5,692,029 A	11/1997	Husseiny	6,192,101 B1	2/2001	Grodzins
5,696,806 A	12/1997	Grodzins	6,192,104 B1	2/2001	Adams
5,712,926 A	1/1998	Eberhard	6,195,413 B1	2/2001	Geus
			6,195,444 B1	2/2001	Simanovsky
			6,198,795 B1	3/2001	Naumann



(56)

**References Cited**

## U.S. PATENT DOCUMENTS

6,200,024 B1 *	3/2001	Negrelli .....	A61B 6/4233 378/196
6,212,251 B1	4/2001	Tomura	
6,216,540 B1	4/2001	Nelson	
6,218,943 B1	4/2001	Ellenbogen	
6,236,709 B1	5/2001	Perry	
6,236,712 B1	5/2001	Tomasetti	
6,246,320 B1	6/2001	Monroe	
6,249,567 B1	6/2001	Rothschild	
6,252,929 B1	6/2001	Swift	
6,256,369 B1	7/2001	Lai	
6,256,404 B1	7/2001	Gordon	
6,269,142 B1	7/2001	Smith	
6,272,230 B1	8/2001	Hiraoglu	
6,278,115 B1	8/2001	Annis	
6,282,260 B1	8/2001	Grodzins	
6,292,533 B1	9/2001	Swift	
6,301,326 B2	10/2001	Bjorkholm	
6,301,327 B1	10/2001	Martens	
6,304,629 B1	10/2001	Conway	
6,317,509 B1	11/2001	Simanovsky	
6,320,933 B1	11/2001	Grodzins	
6,324,249 B1	11/2001	Fazzio	
6,345,113 B1	2/2002	Crawford	
6,347,132 B1	2/2002	Annis	
6,356,620 B1	3/2002	Rothschild	
6,396,899 B2	5/2002	Kuwabara	
6,418,189 B1	7/2002	Schafer	
6,418,194 B1	7/2002	McPherson	
6,421,420 B1	7/2002	Grodzins	
6,424,695 B1	7/2002	Grodzins	
6,427,891 B1	8/2002	Anderson	
6,429,578 B1	8/2002	Danielsson	
6,430,255 B2	8/2002	Fenkart	
6,431,344 B1	8/2002	Emmermann	
6,434,219 B1	8/2002	Rothschild	
6,435,715 B1	8/2002	Betz	
6,438,201 B1	8/2002	Mazess	
6,442,233 B1	8/2002	Grodzins	
6,445,765 B1	9/2002	Frank	
6,446,782 B1	9/2002	Patrick	
6,448,564 B1	9/2002	Johnson	
6,453,003 B1	9/2002	Springer	
6,453,007 B2	9/2002	Adams	
6,456,684 B1	9/2002	Mun	
6,459,755 B1	10/2002	Li	
6,459,761 B1	10/2002	Grodzins	
6,459,764 B1	10/2002	Chalmers	
6,473,487 B1	10/2002	Le	
RE37,899 E	11/2002	Grodzins	
6,483,894 B2	11/2002	Hartick	
6,507,025 B1	1/2003	Verbinski	
6,528,787 B2	3/2003	Katagami	
6,532,276 B1	3/2003	Hartick	
6,542,574 B2	4/2003	Grodzins	
6,542,578 B2	4/2003	Ries	
6,542,580 B1	4/2003	Carver	
6,543,599 B2	4/2003	Jasinetzky	
6,546,072 B1	4/2003	Chalmers	
6,552,346 B2	4/2003	Verbinski	
6,556,653 B2	4/2003	Hussein	
6,563,903 B2	5/2003	Kang	
6,563,906 B2	5/2003	Hussein	
6,567,496 B1	5/2003	Sychev	
6,580,778 B2	6/2003	Meder	
6,584,170 B2	6/2003	Aust	
6,590,956 B2	7/2003	Fenkart	
6,591,130 B2	7/2003	Shahidi	
6,597,760 B2	7/2003	Beneke	
6,606,516 B2	8/2003	Levine	
6,618,466 B1	9/2003	Ning	
6,621,888 B2	9/2003	Grodzins	
6,629,593 B2	10/2003	Zeitler	
6,636,581 B2	10/2003	Sorenson	
6,636,623 B2	10/2003	Nelson	
6,647,091 B2	11/2003	Fenkart	
6,647,094 B2	11/2003	Harding	
6,647,095 B2	11/2003	Hsieh	
6,653,588 B1	11/2003	Gillard-Hickman	
6,658,087 B2	12/2003	Chalmers	
6,661,876 B2	12/2003	Turner	
6,663,280 B2	12/2003	Doenges	
6,665,373 B1	12/2003	Kotowski	
6,665,433 B2	12/2003	Roder	
6,687,333 B2	2/2004	Carroll	
6,690,766 B2	2/2004	Kresse	
6,707,879 B2	3/2004	McClelland	
6,713,773 B1	3/2004	Lyons	
6,715,533 B2	4/2004	Kresse	
6,721,387 B1	4/2004	Naidu	
6,721,391 B2	4/2004	McClelland	
6,727,506 B2	4/2004	Mallette	
6,735,271 B1	5/2004	Rand	
6,737,652 B2	5/2004	Lanza	
6,744,845 B2	6/2004	Harding	
6,748,043 B1	6/2004	Dobbs	
6,754,298 B2	6/2004	Fessler	
6,760,407 B2	7/2004	Price	
6,763,083 B2	7/2004	Fernandez	
6,763,635 B1 *	7/2004	Lowman .....	B60P 1/5433 378/198
6,770,884 B2	8/2004	Bryman	
6,775,348 B2	8/2004	Hoffman	
6,785,357 B2	8/2004	Bernardi	
6,788,761 B2	9/2004	Bijjani	
6,812,426 B1	11/2004	Kotowski	
6,813,374 B1	11/2004	Karimi	
6,816,571 B2	11/2004	Bijjani	
6,827,265 B2	12/2004	Knowles	
6,829,585 B1	12/2004	Grewal	
6,830,185 B2	12/2004	Tsikos	
6,837,422 B1	1/2005	Meder	
6,837,432 B2	1/2005	Tsikos	
6,839,134 B2	1/2005	Saito	
6,839,403 B1	1/2005	Kotowski	
6,843,599 B2	1/2005	Le	
6,856,344 B2	2/2005	Frantz	
6,856,667 B2	2/2005	Ellenbogen	
6,859,514 B2	2/2005	Hoffman	
6,869,217 B2	3/2005	Rasche	
6,876,719 B2	4/2005	Ozaki	
6,876,724 B2	4/2005	Zhou	
6,879,657 B2	4/2005	Hoffman	
6,899,540 B1	5/2005	Neiderman	
6,901,135 B2	5/2005	Fox	
6,901,346 B2	5/2005	Tracy	
6,906,329 B2	6/2005	Bryman	
6,907,101 B2	6/2005	Hoffman	
6,920,197 B2	7/2005	Kang	
6,922,455 B2	7/2005	Jurczyk	
6,922,460 B2	7/2005	Skatter	
6,922,461 B2	7/2005	Kang	
6,928,141 B2	8/2005	Carver	
6,933,504 B2	8/2005	Hoffman	
6,934,354 B2	8/2005	Hoffman	
6,937,692 B2	8/2005	Johnson	
6,940,071 B2	9/2005	Ramsden	
6,944,264 B2	9/2005	Bijjani	
6,947,517 B2	9/2005	Hoffman	
6,950,492 B2	9/2005	Besson	
6,950,493 B2	9/2005	Besson	
6,952,163 B2	10/2005	Huey	
6,953,935 B1	10/2005	Hoffman	
6,957,913 B2	10/2005	Renkart	
6,962,289 B2	11/2005	Vatan	
6,965,314 B2	11/2005	Jerry	
6,968,030 B2	11/2005	Hoffman	
6,968,034 B2	11/2005	Ellenbogen	
6,971,577 B2	12/2005	Tsikos	
6,973,158 B2	12/2005	Besson	
6,975,698 B2	12/2005	Katcha	
6,978,936 B2	12/2005	Tsikos	
6,980,627 B2	12/2005	Qiu	
6,990,171 B2	1/2006	Toth	



(56)

**References Cited**

## U.S. PATENT DOCUMENTS

6,990,172 B2	1/2006	Toth	7,166,458 B2	1/2007	Ballerstadt
6,991,371 B2	1/2006	Georgeson	7,166,844 B1	1/2007	Gormley
6,993,115 B2	1/2006	McGuire	7,167,539 B1	1/2007	Hoffman
6,996,209 B2	2/2006	Marek	7,173,998 B2	2/2007	Hoffman
7,010,083 B2	3/2006	Hoffman	7,177,387 B2	2/2007	Yasunaga
7,010,094 B2	3/2006	Grodzins	7,177,391 B2	2/2007	Chapin
7,016,459 B2	3/2006	Ellenbogen	7,187,756 B2	3/2007	Gohn
7,020,241 B2	3/2006	Beneke	7,190,757 B2	3/2007	Ying
7,020,242 B2	3/2006	Ellenbogen	7,192,031 B2	3/2007	Dunham
7,023,956 B2	4/2006	Heaton	7,197,113 B1	3/2007	Katcha
7,023,957 B2	4/2006	Bijjani	7,197,172 B1	3/2007	Naidu
7,027,553 B2	4/2006	Dunham	7,203,276 B2	4/2007	Arsenault
7,027,554 B2	4/2006	Gaultier	7,203,629 B2	4/2007	Oezis
7,031,430 B2	4/2006	Kaucic	7,204,125 B2	4/2007	Fine
7,031,434 B1	4/2006	Saunders	7,206,379 B2	4/2007	Lemaitre
7,034,313 B2	4/2006	Hoffman	7,207,713 B2	4/2007	Lowman
7,039,154 B1	5/2006	Ellenbogen	7,212,113 B2	5/2007	Zanovitch
7,039,159 B2	5/2006	Muenchau	7,215,731 B1	5/2007	Basu
7,042,975 B2	5/2006	Heuscher	7,215,737 B2	5/2007	Li
7,045,787 B1	5/2006	Verbinski	7,215,738 B2	5/2007	Muenchau
7,045,788 B2	5/2006	Iwatschenko-Borho	7,218,700 B2	5/2007	Huber
7,046,756 B2	5/2006	Hoffman	7,218,704 B1	5/2007	Adams
7,046,761 B2	5/2006	Ellenbogen	7,224,763 B2	5/2007	Naidu
7,046,768 B1	5/2006	Gilevich	7,224,765 B2	5/2007	Ellenbogen
7,050,536 B1	5/2006	Fenkart	7,224,766 B2	5/2007	Jiang
7,050,541 B2	5/2006	Bittl	7,224,769 B2	5/2007	Turner
7,054,408 B2	5/2006	Jiang	7,233,640 B2	6/2007	Ikhlef
7,062,009 B2	6/2006	Karimi	7,236,564 B2	6/2007	Hopkins
7,062,011 B1	6/2006	Tybinkowski	7,238,945 B2	7/2007	Hoffman
7,062,074 B1	6/2006	Beneke	7,238,951 B2	7/2007	Disdier
7,064,334 B2	6/2006	Hoffman	7,244,947 B2	7/2007	Polichar
7,065,175 B2	6/2006	Green	7,247,856 B2	7/2007	Hoge
7,065,179 B2	6/2006	Block	7,250,940 B2	7/2007	Jayanetti
7,068,749 B2	6/2006	Kollegal	7,251,310 B2	7/2007	Smith
7,068,750 B2	6/2006	Toth	7,257,189 B2	8/2007	Modica
7,068,751 B2	6/2006	Toth	7,260,170 B2	8/2007	Arenson
7,072,434 B1	7/2006	Tybinkowski	7,260,171 B1	8/2007	Arenson
7,076,029 B2	7/2006	Toth	7,260,172 B2	8/2007	Arenson
7,078,699 B2	7/2006	Seppi	7,260,173 B2	8/2007	Wakayama
7,081,628 B2	7/2006	Granfors	7,260,174 B2	8/2007	Hoffman
7,084,404 B2	8/2006	Hoffman	7,260,182 B2	8/2007	Toth
7,087,902 B2	8/2006	Wang	7,260,255 B2	8/2007	Polichar
7,088,799 B2	8/2006	Hoffman	7,263,160 B2	8/2007	Schlomka
7,090,133 B2	8/2006	Zhu	7,266,180 B1	9/2007	Saunders
7,092,481 B2	8/2006	Hoffman	7,272,208 B2	9/2007	Yatsenko
7,092,485 B2	8/2006	Kravis	7,272,429 B2	9/2007	Walker
7,099,434 B2	8/2006	Adams	7,274,767 B2	9/2007	Clayton
7,099,435 B2	8/2006	Heumann	7,277,577 B2	10/2007	Ying
7,103,137 B2	9/2006	Seppi	7,279,120 B2	10/2007	Cheng
7,110,488 B2	9/2006	Katcha	7,280,631 B2	10/2007	De
7,112,797 B2	9/2006	Hoge	7,282,727 B2	10/2007	Retsky
7,116,235 B2	10/2006	Alioto	7,283,604 B2	10/2007	De
7,116,749 B2	10/2006	Besson	7,283,609 B2	10/2007	Possin
7,116,751 B2	10/2006	Ellenbogen	7,295,019 B2	11/2007	Yang
7,119,553 B2	10/2006	Yang	7,295,651 B2	11/2007	Delgado
7,123,681 B2	10/2006	Ellenbogen	7,298,812 B2	11/2007	Tkaczyk
7,127,027 B2	10/2006	Hoffman	7,302,083 B2	11/2007	Larson
7,130,374 B1	10/2006	Jacobs	7,308,073 B2	12/2007	Tkaczyk
RE39,396 E	11/2006	Swift	7,308,074 B2	12/2007	Jiang
7,133,491 B2	11/2006	Bernardi	7,308,077 B2	12/2007	Bijjani
7,136,450 B2	11/2006	Ying	7,317,195 B2	1/2008	Eikman
7,136,451 B2	11/2006	Naidu	7,317,259 B2	1/2008	Yamauchi
7,139,367 B1	11/2006	Le	7,317,390 B2	1/2008	Huey
7,139,406 B2	11/2006	McClelland	7,319,737 B2	1/2008	Singh
7,142,208 B2	11/2006	Lorenz	7,322,745 B2	1/2008	Agrawal
7,142,629 B2	11/2006	Edic	7,324,625 B2	1/2008	Eilbert
7,149,278 B2	12/2006	Arenson	7,327,853 B2	2/2008	Ying
7,149,339 B2	12/2006	Veneruso	7,330,527 B2	2/2008	Hoffman
7,154,989 B2	12/2006	Ueno	7,330,535 B2	2/2008	Arenson
7,155,812 B1	1/2007	Peterson	7,333,587 B2	2/2008	De
7,158,611 B2	1/2007	Heismann	7,333,588 B2	2/2008	Mistretta
7,162,005 B2	1/2007	Bjorkholm	7,333,589 B2	2/2008	Ellenbogen
7,162,285 B2	1/2007	Owens	7,335,887 B1	2/2008	Verbinski
7,164,747 B2	1/2007	Ellenbogen	7,336,769 B2	2/2008	Arenson
7,164,750 B2	1/2007	Nabors	7,349,525 B2	3/2008	Morton
			7,352,843 B2	4/2008	Hu
			7,356,174 B2	4/2008	Leue
			7,369,463 B1	5/2008	Van Dulleman
			7,369,640 B2	5/2008	Seppi



(56)

## References Cited

## U.S. PATENT DOCUMENTS

7,369,643	B2	5/2008	Kotowski
7,372,040	B2	5/2008	Polichar
7,372,944	B2	5/2008	Bernhardt
7,379,530	B2	5/2008	Hoff
7,386,092	B2	6/2008	Kang
7,397,891	B2	7/2008	Johnson
7,400,701	B1	7/2008	Cason
7,420,174	B2	9/2008	Kurita
7,429,738	B2	9/2008	Li
7,440,543	B2	10/2008	Morton
7,453,987	B1	11/2008	Richardson
7,460,639	B2	12/2008	Tudor
7,470,914	B2	12/2008	Li
7,475,428	B2	1/2009	Smith
7,475,866	B2	1/2009	Hu
7,483,510	B2	1/2009	Carver
7,483,511	B2	1/2009	Bendahan
7,486,768	B2	2/2009	Allman
7,492,855	B2	2/2009	Hopkins
7,500,931	B2	3/2009	Rosemeier
7,505,556	B2	3/2009	Chalmers
7,505,557	B2	3/2009	Modica
7,505,562	B2	3/2009	Dinca
7,512,215	B2	3/2009	Morton
7,517,149	B2	4/2009	Agrawal
7,519,148	B2	4/2009	Kotowski
7,525,101	B2	4/2009	Grodzins
7,526,064	B2	4/2009	Akery
7,538,325	B2	5/2009	Mishin
7,547,888	B2	6/2009	Cooke
7,551,714	B2	6/2009	Rothschild
7,551,715	B2	6/2009	Rothschild
7,551,718	B2	6/2009	Rothschild
7,555,099	B2	6/2009	Rothschild
7,564,939	B2	7/2009	Morton
7,580,505	B2	8/2009	Kang
7,593,506	B2	9/2009	Cason
7,593,510	B2	9/2009	Rothschild
7,649,976	B2	1/2010	Georgeson
7,663,109	B2	2/2010	Kang
7,684,538	B2	3/2010	Morton
7,720,195	B2	5/2010	Allman
7,724,869	B2	5/2010	Wang
7,734,066	B2	6/2010	Delia
7,738,687	B2	6/2010	Tortora
7,741,612	B2	6/2010	Clothier
7,742,568	B2	6/2010	Smith
7,760,103	B2	7/2010	Frank
7,762,760	B2	7/2010	Takehara
7,769,133	B2	8/2010	Carver
7,783,003	B2	8/2010	Clayton
7,783,004	B2	8/2010	Kotowski
7,796,734	B2	9/2010	Mastronardi
7,800,073	B2	9/2010	Clothier
7,809,104	B2	10/2010	Foland
7,809,109	B2	10/2010	Mastronardi
7,817,775	B2	10/2010	Kang
7,817,776	B2	10/2010	Agrawal
7,835,486	B2	11/2010	Basu
7,860,213	B2	12/2010	Akery
7,876,879	B2	1/2011	Morton
7,876,880	B2	1/2011	Kotowski
7,885,375	B2	2/2011	Bernard
7,903,783	B2	3/2011	Modica
7,952,079	B2	5/2011	Neustadter
7,957,506	B2	6/2011	Smith
7,963,695	B2 *	6/2011	Kotowski
7,965,695	B2	6/2011	Valko
7,973,697	B2	7/2011	Reilly
7,991,113	B2	8/2011	Carver
7,991,117	B2	8/2011	Chen
7,995,705	B2	8/2011	Allman
8,000,436	B2	8/2011	Seppi
8,031,903	B2	10/2011	Parsi

G01N 23/04  
378/198

8,059,781	B2	11/2011	Agrawal
8,148,693	B2	4/2012	Ryge
8,170,177	B2	5/2012	Akery
8,173,970	B2	5/2012	Inbar
8,194,822	B2	6/2012	Rothschild
8,263,938	B2	9/2012	Bjorkholm
8,275,091	B2	9/2012	Morton
8,350,747	B2	1/2013	Delia
8,356,937	B2	1/2013	Kotowski
8,385,501	B2	2/2013	Allman
8,389,941	B2	3/2013	Bendahan
8,389,942	B2	3/2013	Morton
8,401,147	B2	3/2013	Ryge
8,433,036	B2	4/2013	Morton
8,437,448	B2	5/2013	Langeveld
8,451,974	B2	5/2013	Morton
8,457,275	B2	6/2013	Akery
8,483,356	B2	7/2013	Bendahan
8,491,189	B2	7/2013	Kotowski
8,498,376	B2	7/2013	Modica
8,502,699	B2	8/2013	Zerwekh
8,503,605	B2	8/2013	Morton
8,579,506	B2	11/2013	Morton
8,582,720	B2	11/2013	Morton
8,644,453	B2	2/2014	Morton
8,668,386	B2 *	3/2014	Morton
8,687,765	B2	4/2014	Kotowski
8,735,833	B2	5/2014	Morto
8,744,033	B2	6/2014	Oosaka
8,798,232	B2	8/2014	Bendahan
8,831,176	B2	9/2014	Morto
8,837,670	B2	9/2014	Akery
2002/0031202	A1	3/2002	Callerame
2002/0038753	A1	4/2002	Ursu
2002/0045152	A1	4/2002	Viscardi
2003/0023592	A1	1/2003	Modica
2003/0085163	A1	5/2003	Chan
2004/0101098	A1	5/2004	Bijjani
2004/0141584	A1	7/2004	Bernardi
2004/0178339	A1	9/2004	Gentile
2004/0213378	A1	10/2004	Zhou
2004/0258305	A1	12/2004	Burnham
2005/0008119	A1	1/2005	McClelland
2005/0023479	A1	2/2005	Grodzins
2005/0031076	A1	2/2005	McClelland
2005/0100135	A1	5/2005	Lowman
2005/0117683	A1	6/2005	Mishin
2005/0117700	A1	6/2005	Peschmann
2005/0226364	A1	10/2005	Bernard
2005/0251397	A1	11/2005	Zanovitch
2006/0056584	A1	3/2006	Allman
2006/0115109	A1	6/2006	Whitson
2006/0140341	A1	6/2006	Carver
2006/0274916	A1	12/2006	Chan
2007/0009088	A1	1/2007	Edic
2007/0085010	A1	4/2007	Letant
2007/0194909	A1	8/2007	Garfield
2007/0217572	A1	9/2007	Kotowski
2008/0056432	A1	3/2008	Pack
2008/0089476	A1	4/2008	Chen
2008/0211431	A1	9/2008	Mishin
2011/0176660	A1	7/2011	Morton
2011/0216881	A1	9/2011	Modica
2012/0177176	A1	7/2012	Carver
2013/0039472	A1	2/2013	Morton

G01V 5/0016  
378/198

## FOREIGN PATENT DOCUMENTS

EP	77018	4/1983
EP	0077018 A1	4/1983
EP	0176314	4/1986
EP	0261984 A2	3/1988
EP	0287707	10/1988
EP	0417965	3/1991
EP	0432568	6/1991
EP	0531993 A1	3/1993
EP	0584871 A1	3/1994
EP	0864884 A2	9/1998



(56)

**References Cited**

## FOREIGN PATENT DOCUMENTS

EP	0919186	A2	6/1999	
EP	0924742	A2	6/1999	
EP	0930046	A2	7/1999	
EP	0963925	A2	12/1999	
EP	0972743	A1 *	1/2000	..... B66F 11/046
EP	1277439	A1	1/2003	
EP	1374776	A1	1/2004	
EP	1413898	A1	4/2004	
EP	2255224		12/2010	
FR	2328280	A1	5/1977	
GB	1497396	A	1/1978	
GB	1526041	A	9/1978	
GB	2015245	A	9/1979	
GB	2089109	A	6/1982	
GB	2212903	A	8/1989	
GB	2255634	A	11/1992	
GB	2277013	A	10/1994	
GB	2337032	A	11/1999	
GB	2404431		2/2005	
GB	2409268	A	6/2005	
GB	2424065	A	9/2006	
GB	2437777	A	11/2007	
GB	2438317	A	11/2007	
GB	2470161		11/2010	
GB	2470163		11/2010	
GB	2470330		11/2010	
JP	570175247		10/1982	
JP	59016254		1/1984	
JP	5975549		4/1984	
JP	600015546		1/1985	
JP	600021440		2/1985	
JP	H10211196	A	8/1998	
JP	H11230918	A	8/1999	
JP	2001176408		6/2001	
JP	2001233440	A	8/2001	
JP	2003126075	A	5/2003	
JP	2004000605	A	1/2004	
JP	2005013768	A	1/2005	
WO	9528715	A2	10/1995	
WO	9802763	A1	1/1998	
WO	9803889	A1	1/1998	
WO	9820366	A1	5/1998	
WO	9855851	A1	12/1998	
WO	9939189	A2	8/1999	
WO	9960387	A2	11/1999	
WO	0033060	A2	6/2000	
WO	0159485	A1	8/2001	
WO	2001059485		8/2001	
WO	03051201	A2	6/2003	
WO	03105159		12/2003	
WO	2004010127	A1	1/2004	
WO	2004037088		5/2004	
WO	2004111625		12/2004	
WO	2005091227		9/2005	
WO	2005098400	A2	10/2005	
WO	2006036076	A1	4/2006	
WO	2006045019		4/2006	
WO	2006078691	A2	7/2006	
WO	2006095188		9/2006	
WO	2005084351		11/2006	
WO	2006135586		12/2006	
WO	2007035359	A2	3/2007	
WO	2007051092		5/2007	
WO	2007055720	A2	5/2007	
WO	2007068933	A1	6/2007	
WO	2007103216	A2	9/2007	
WO	2008017983	A2	2/2008	
WO	2009027667	A2	3/2009	
WO	2009088706		9/2009	
WO	2009106803		9/2009	
WO	2009106815		9/2009	
WO	2009106857		9/2009	
WO	2009137698		11/2009	
WO	2009141613		11/2009	
WO	2009141615		11/2009	

WO	2009150416	A2	12/2009
WO	2010135620		1/2011
WO	2011008718		1/2011
WO	2011069024	A1	6/2011
WO	2011087861		7/2011
WO	2011095810		8/2011
WO	2012109273		8/2012
WO	2012174265		12/2012

## OTHER PUBLICATIONS

Smith C. R. et al: 'Application of 450 kV computed tomography to engine blocks with steel liners' Materials Evaluation vol. 65, No. 5, 2007, pp. 458-461, XP055108238.

International Search Report for PCT/US10/35720, dated Nov. 15, 2010, Rapiscan Security Products, Inc.

International Search Report for PCT/US2008/087654, dated Jul. 6, 2009, Rapiscan Security Products, Inc.

International preliminary report on patentability PCT/US2012/024184, dated Aug. 13, 2013, Rapiscan Systems Inc.

International Search Report PCT/US2012/024184, dated Jul. 27, 2012, Rapiscan Systems Inc.

International Search Report PCT/US2012/042493, dated Oct. 1, 2012, Rapiscan Systems Inc.

International Search Report PCT/GB2009/000515, dated Feb. 23, 2010, Rapiscan Security Products, Inc.

International Search Report for PCT/GB2009/000497, dated Jan. 22, 2010.

International Search Report PCT/GB2009/001444, dated Apr. 6, 2010, Rapiscan Security Products.

International Search Report for PCT/GB2009/000556, dated Feb. 19, 2010, Rapiscan Security Products, Inc.

International Search Report PCT/GB2009/001277, dated Jul. 20, 2010, Rapiscan Systems, Inc.

Mobile X-Ray Inspection Systems, Internet Citation, Feb. 12, 2007, pp. 1-2, URL: <http://web.archive.org/web/20070212000928/http://www.bombdetecti-on.com/cat--details.php?catid=20>.

Molchanov P A et al: 'Nanosecond gated optical sensors for ocean optic applications' Sensors Applications Symposium, 2006. Proceedings of the 2006 IEEE Houston, Texas, USA Feb. 7-9, 2006, Piscataway, NJ, USA, IEEE, Feb. 7, 2006 (Feb. 7, 2006), pp. 147-150, XP010917671 ISBN: 978-0-7803-9580-0.

International Search Report for PCT/US10/58809; Rapiscan Systems Inc.; dated Apr. 19, 2011.

International Search Report for PCT/GB2009/001250, dated Mar. 2, 2010, Rapiscan Security Products Inc.

International Search Report for PCT/GB2009/001275, dated Jul. 24, 2009, Rapiscan Security Products Inc.

International Search Report for PCT/US2010/041757, dated Oct. 12, 2010, Rapiscan Systems Inc.

International Bureau of WIPO, International Preliminary Report on Patentability, PCT/US2005/011382, dated Oct. 19, 2006, 7 pages.

Mertz, L.N., et al, "Rotational aperture synthesis for x rays", Journal. Optical Society of America, vol. 3, Dec. 1986, pp. 2167-2170.

International Preliminary Report on Patentability, PCT/US2012/024182, dated Aug. 13, 2013, Rapiscan Systems Inc.

International Search Report, PCT/US2012/024182 dated Aug. 20, 2012, Rapiscan Systems Inc.

International Search Report for PCT/US2010/061908, dated Apr. 2, 2012, Rapiscan Systems, Inc.

International Search Report for PCT/GB2006/000859, dated May 19, 2006, Corus UK Ltd.

International Search Report for PCT/GB2011/050182, dated Dec. 28, 2011.

International Search Report for PCT/US11/21758; dated Jul. 7, 2011, Rapiscan Systems Inc.

International Search Report for PCT/GB2009/000575, dated Apr. 7, 2010, Rapiscan Security Products Inc.

International Search Report for PCT/GB2004/001747, dated Aug. 10, 2004, CXR Ltd.

International Search Report for PCT/US2007/005444, dated Oct. 29, 2007, Telesecurity Sciences, Inc.

(56)

**References Cited**

OTHER PUBLICATIONS

International Search Report for PCT/US2006/11492, dated Oct. 11, 2007, United Technologies Corporation.

Sun Olapiriyakul and Sanchoy Das, Design and analysis of a two-stage security screening and inspection system, Journal of Air Transport Management, vol. 13, Issue 2, Mar. 2007, pp. 67-74.

European Patent Office, International Search Report, International Application No. PCT/US99/28266, dated Sep. 6, 2000, 3 pages.

International Search Report, PCT/US2007/066936; dated Sep. 30, 2008, 5 pages.

International Search Report, PCT/US1998/18642, dated Jul. 7, 1999, 4 pages.

International Search Report, PCT/US1999/028035, dated Sep. 15, 2000, 6 pages.

Written Opinion of the International Searching Authority, PCT/US2007/066936, dated Sep. 30, 2008, 7 pages.

Supplementary European Search Report for EP10778449, completed on Jun. 7, 2017.

\* cited by examiner



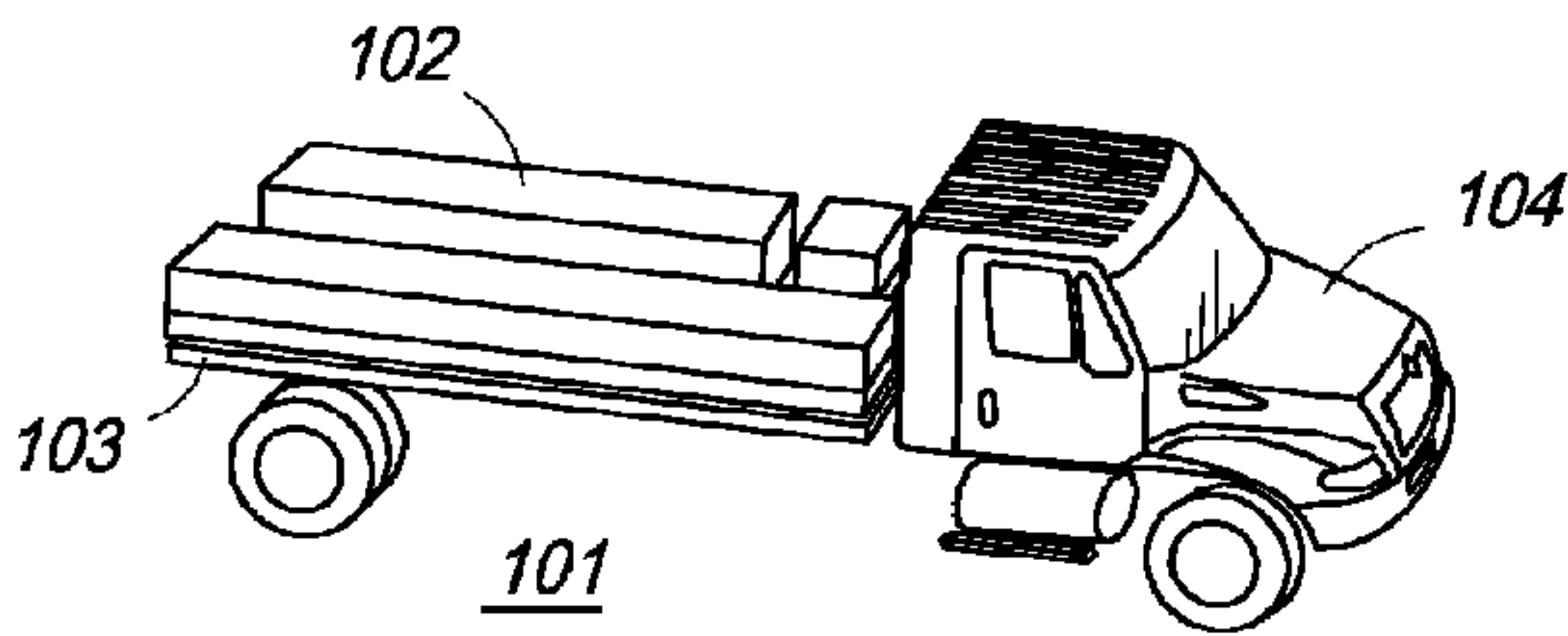


FIG. 1

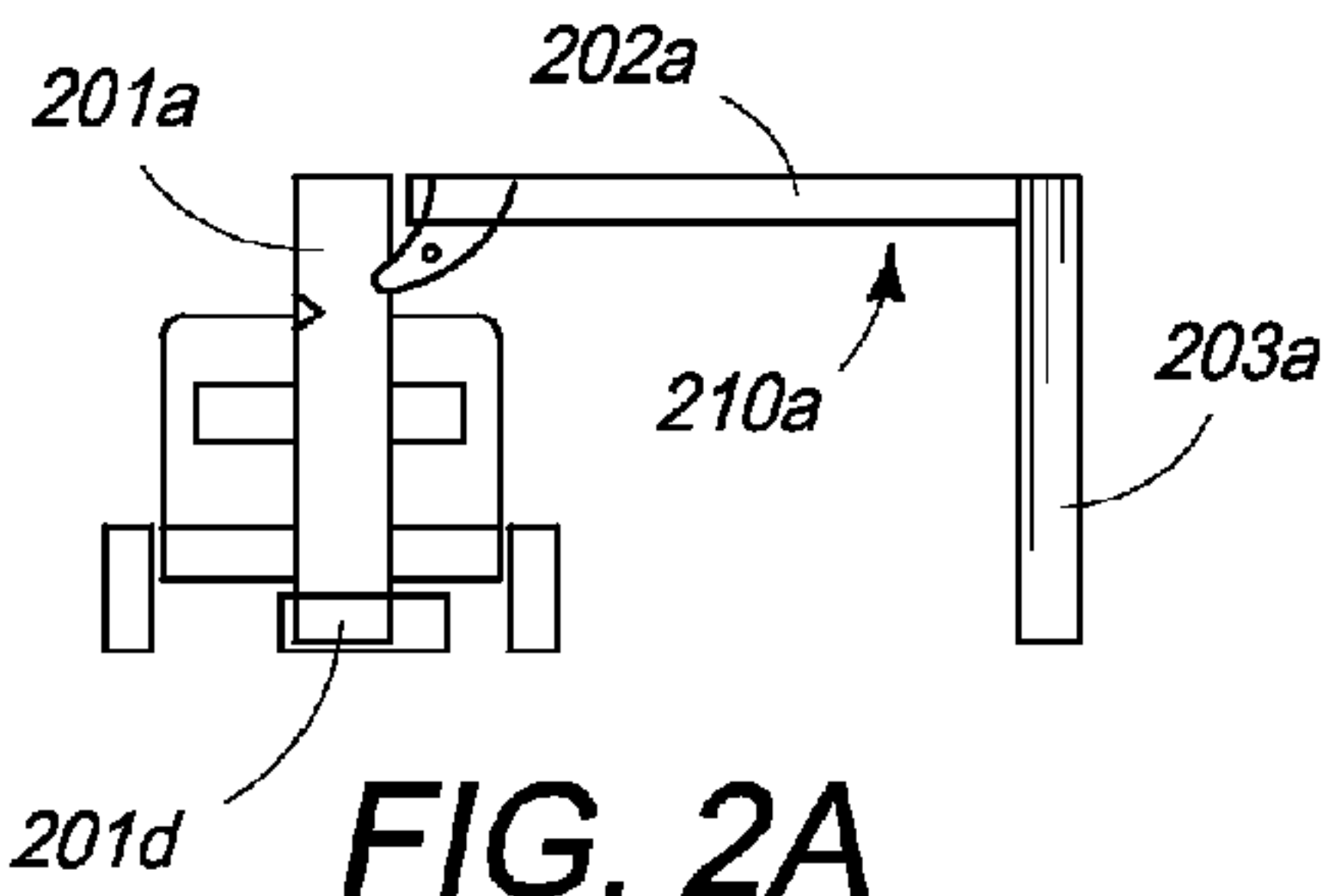


FIG. 2A

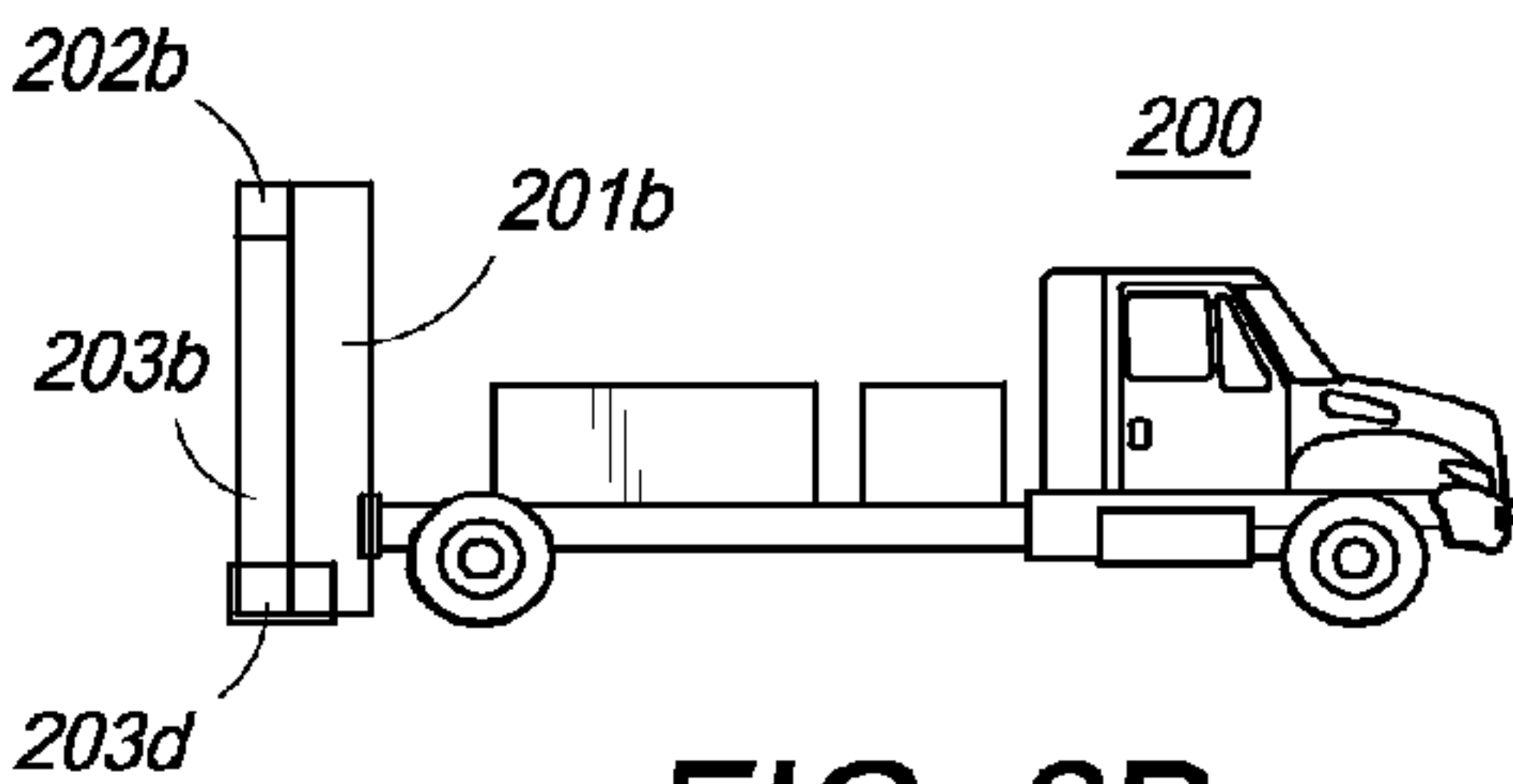


FIG. 2B

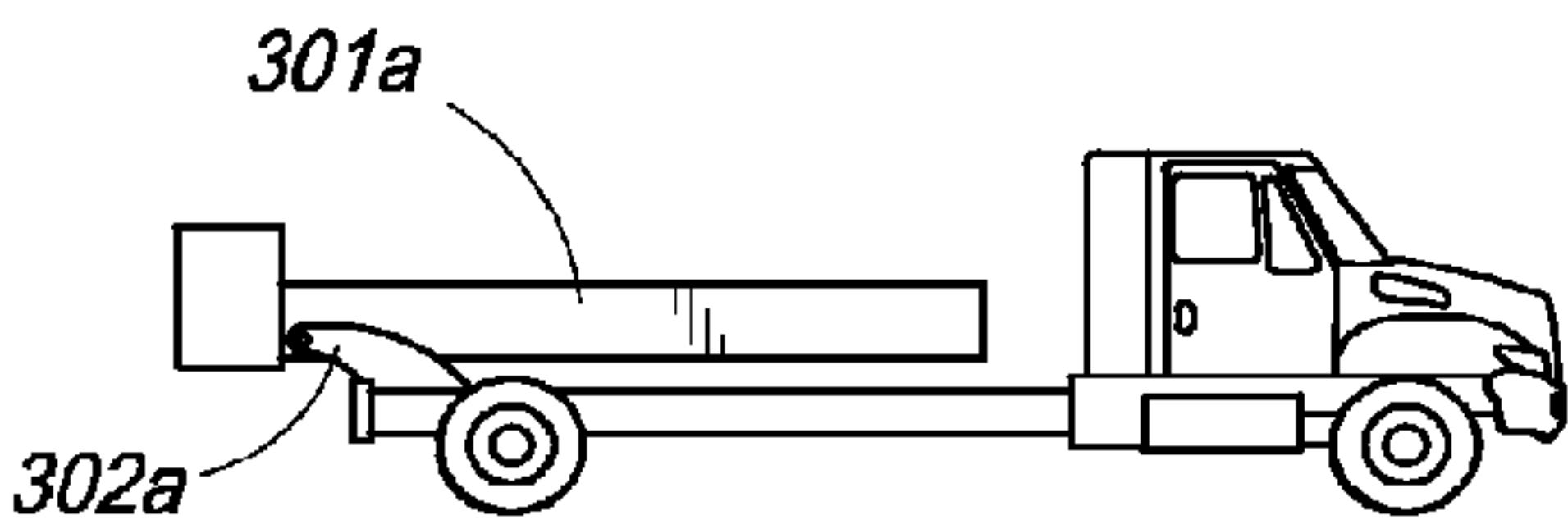


FIG. 3A

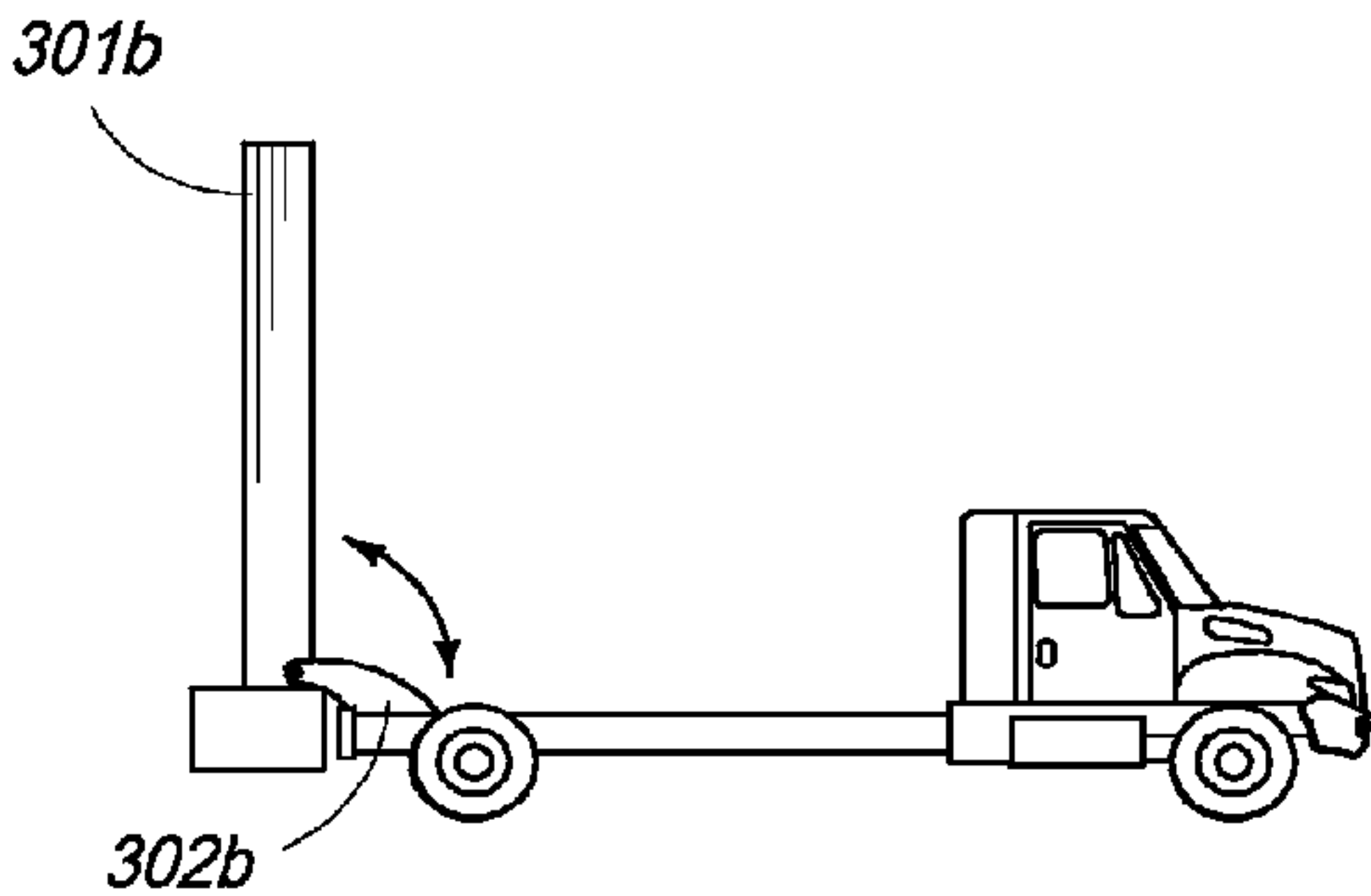


FIG. 3B

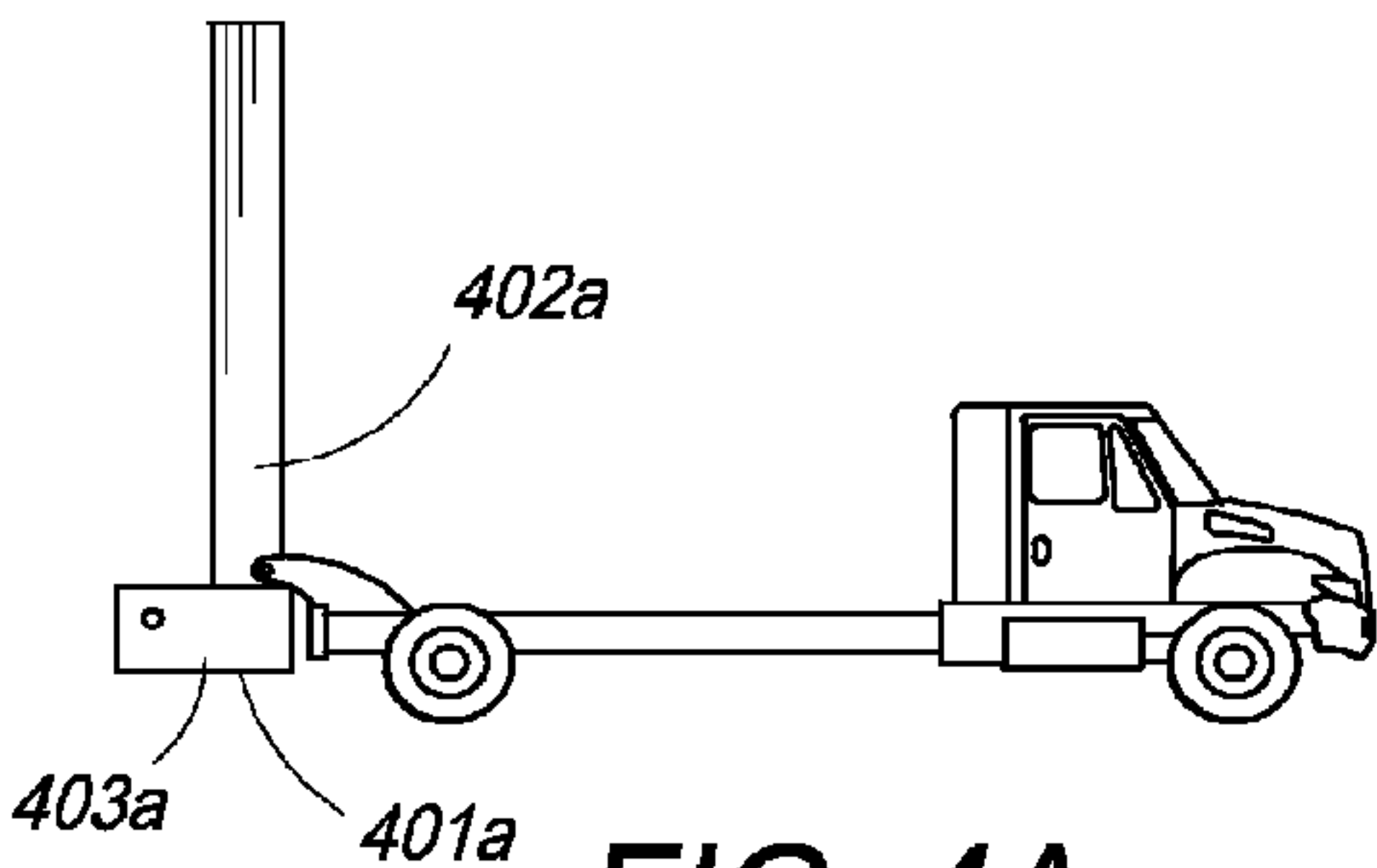


FIG. 4A

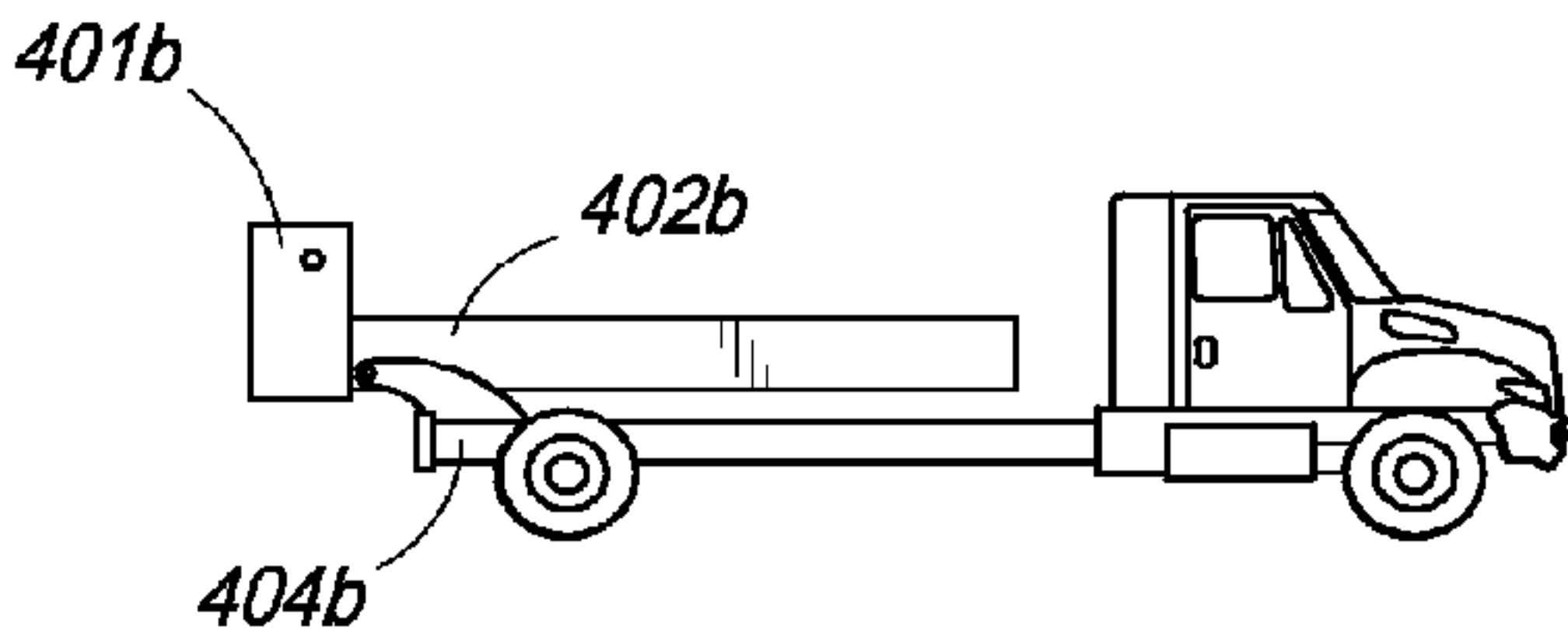


FIG. 4B

FIG. 5A

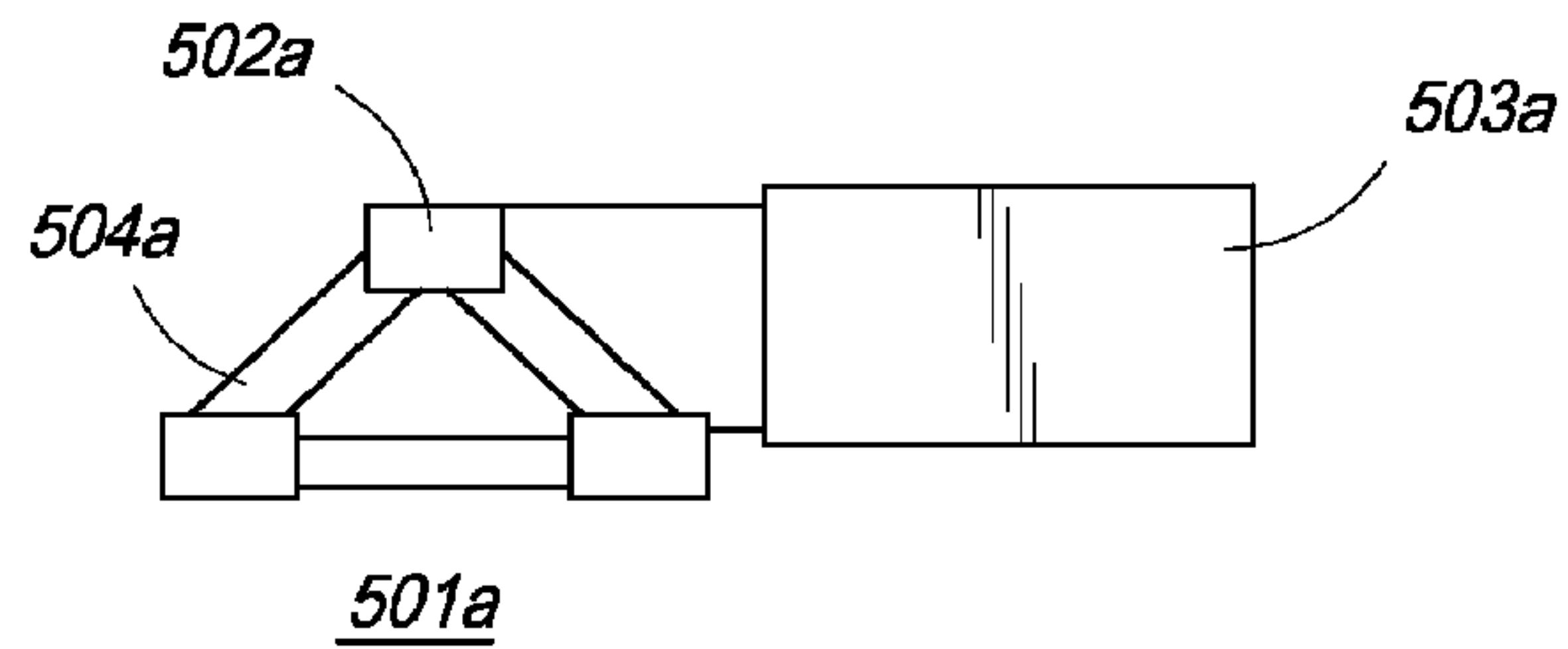


FIG. 5B

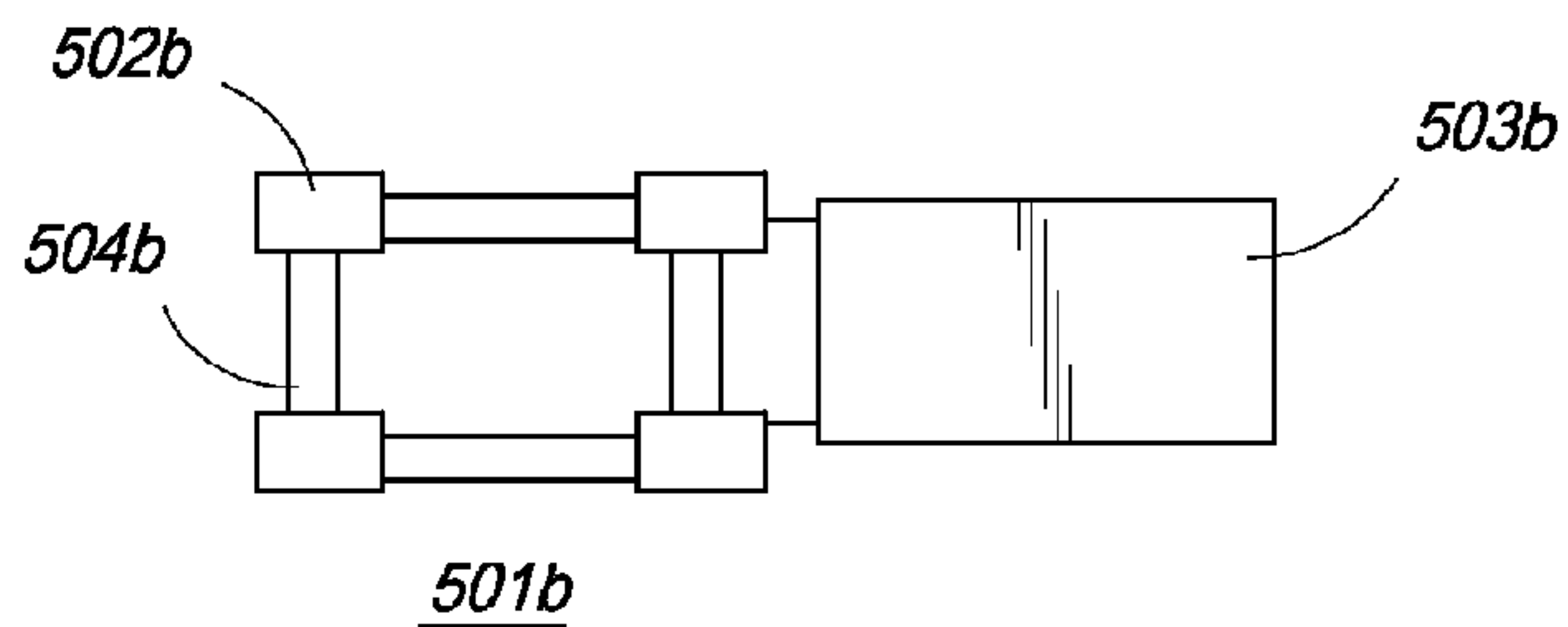


FIG. 5C

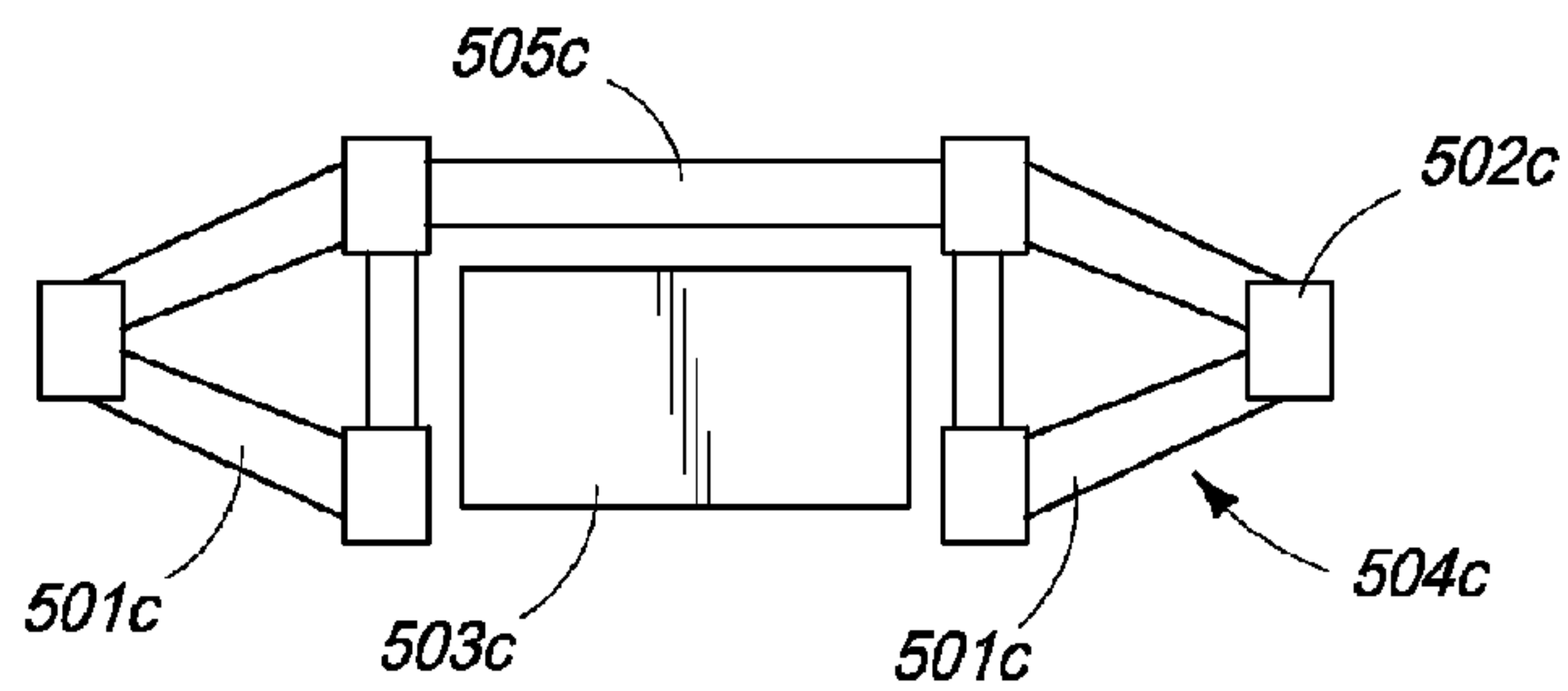


FIG. 5D

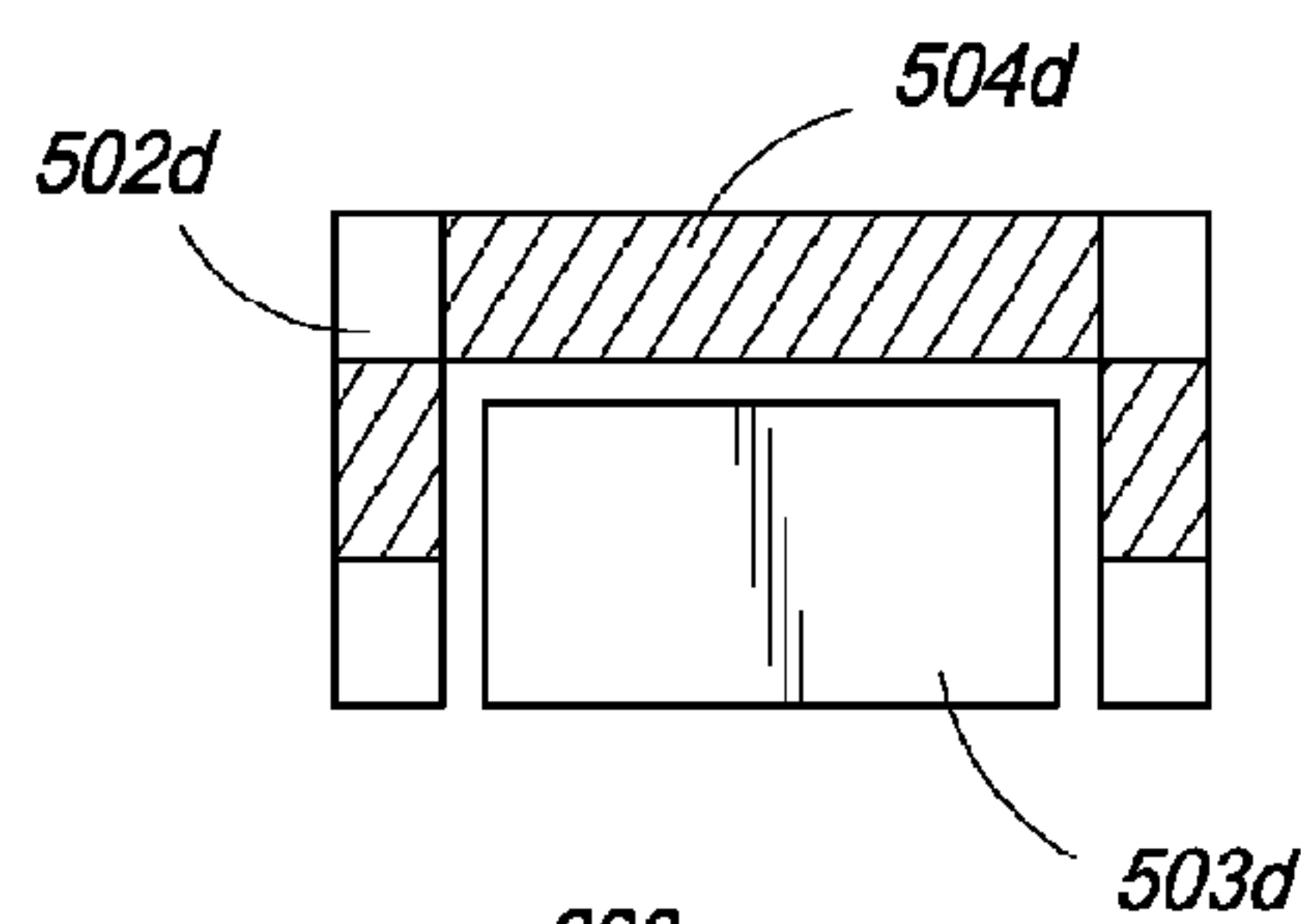
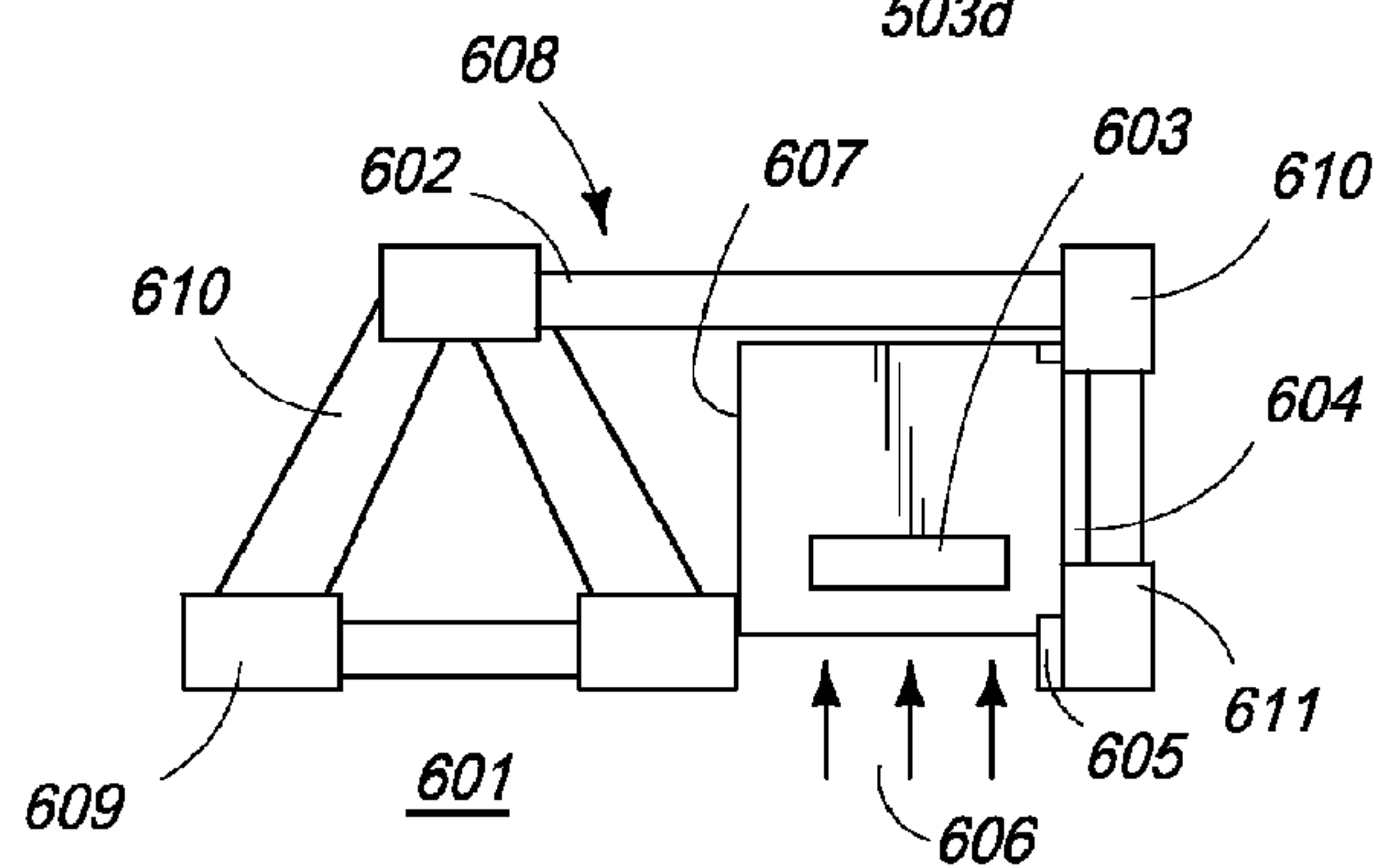
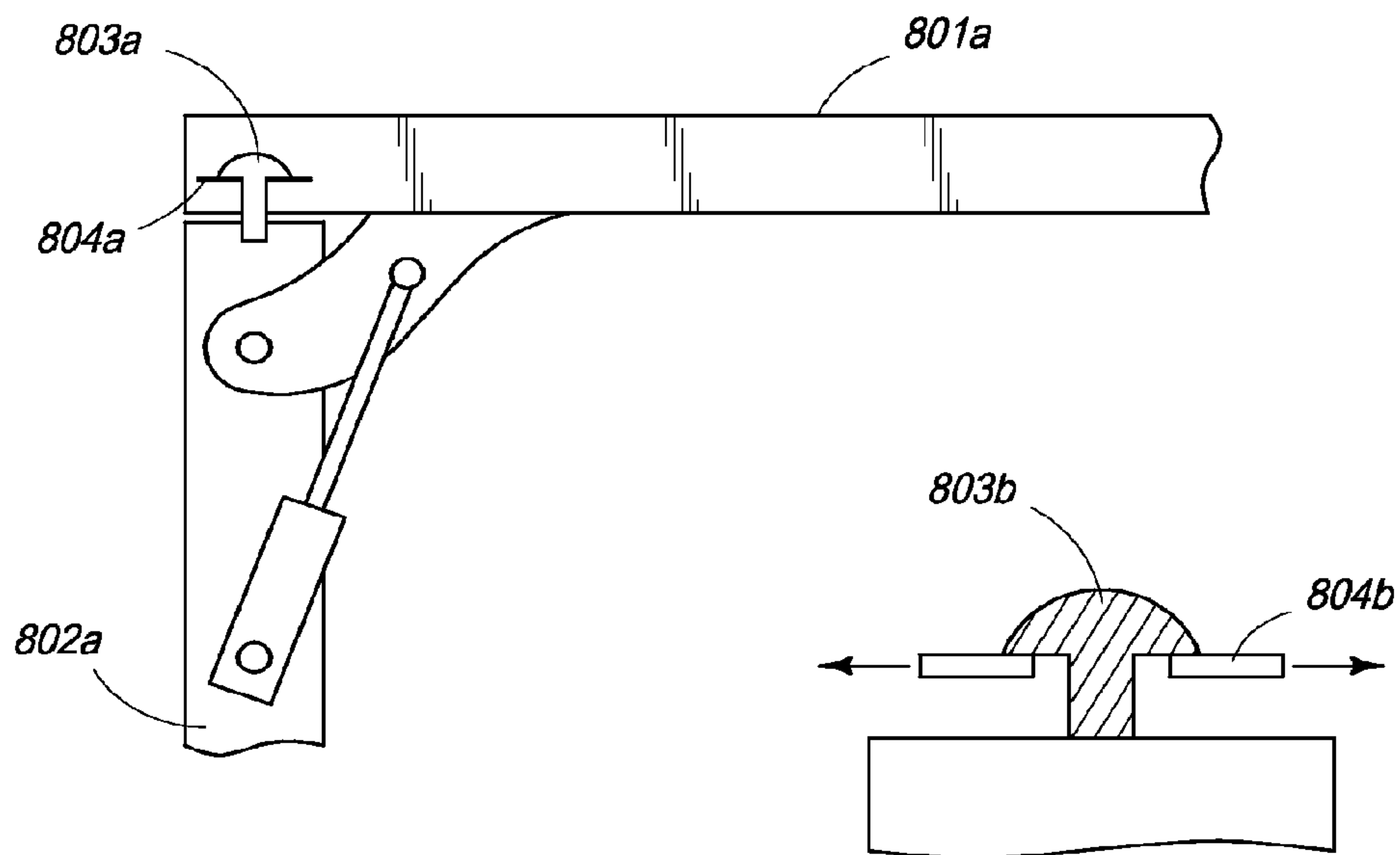
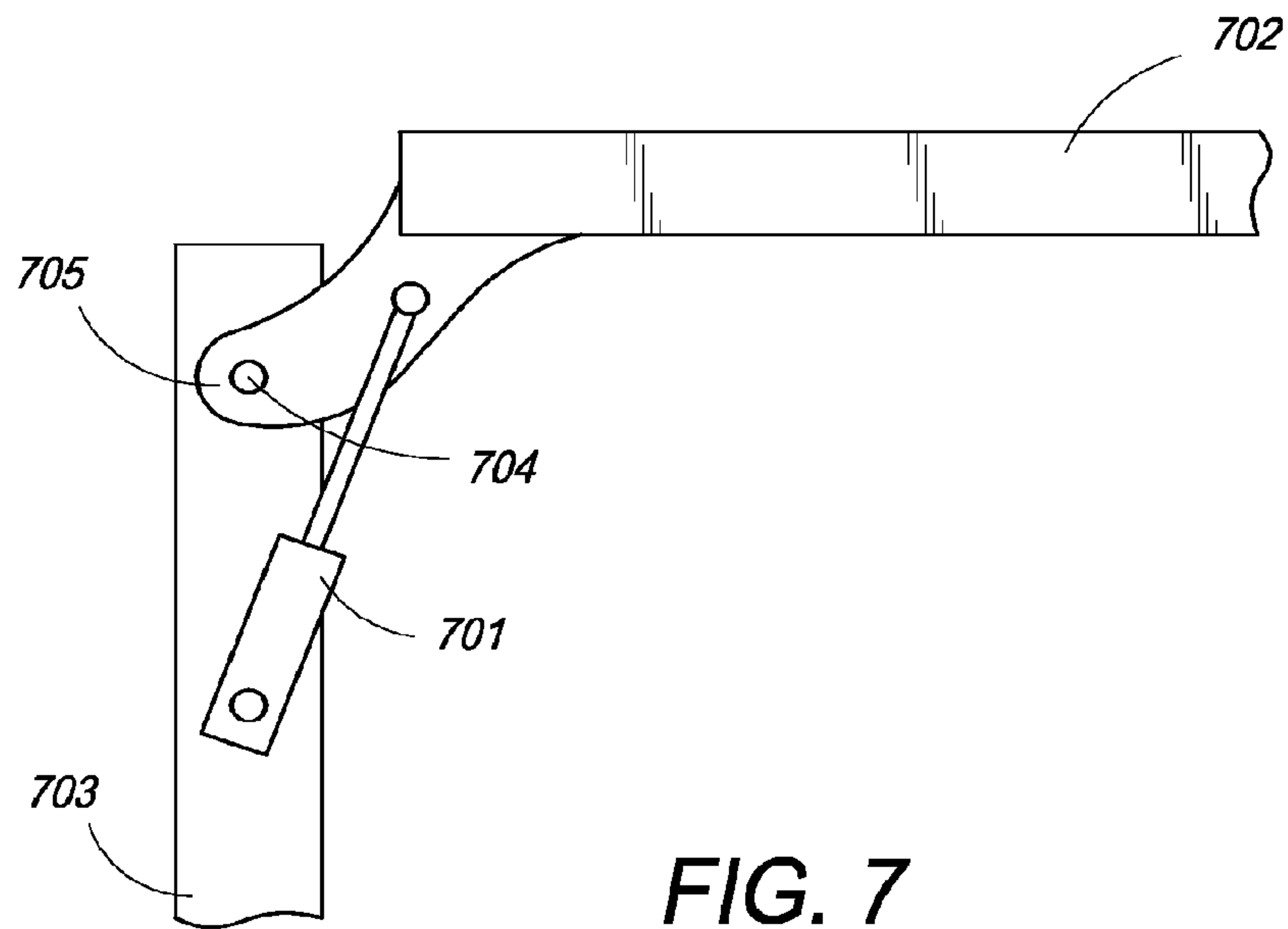
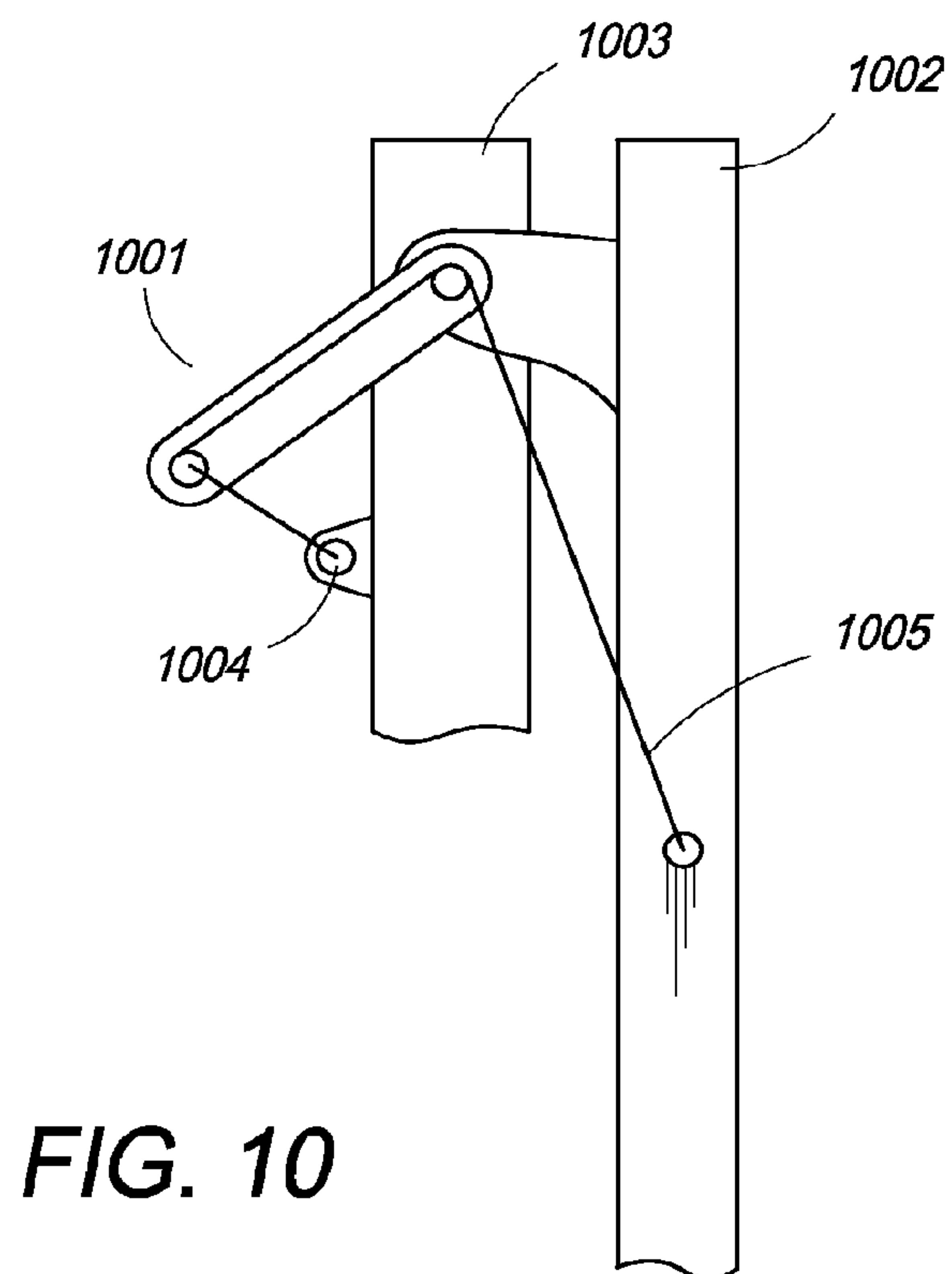
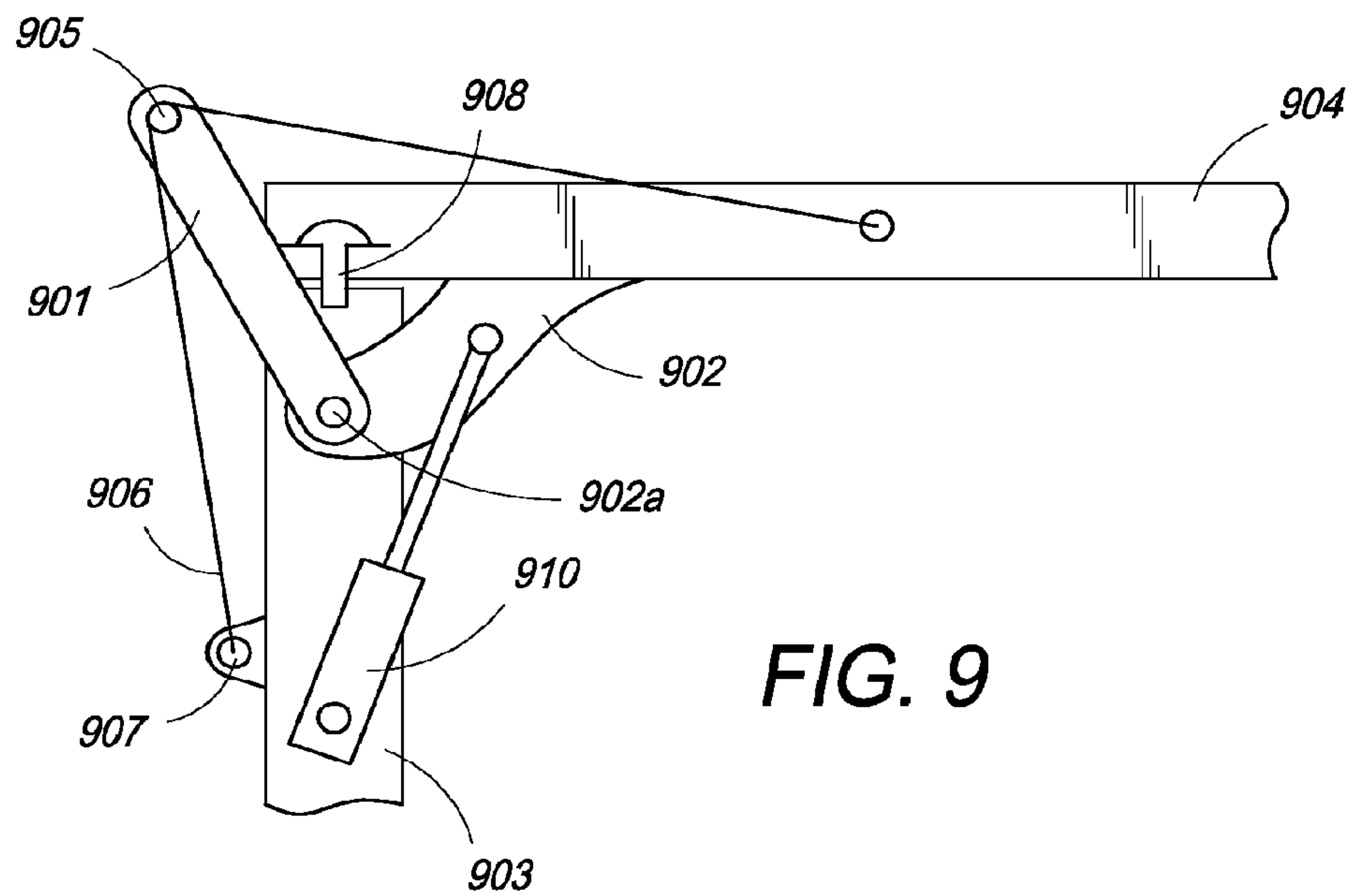


FIG. 6

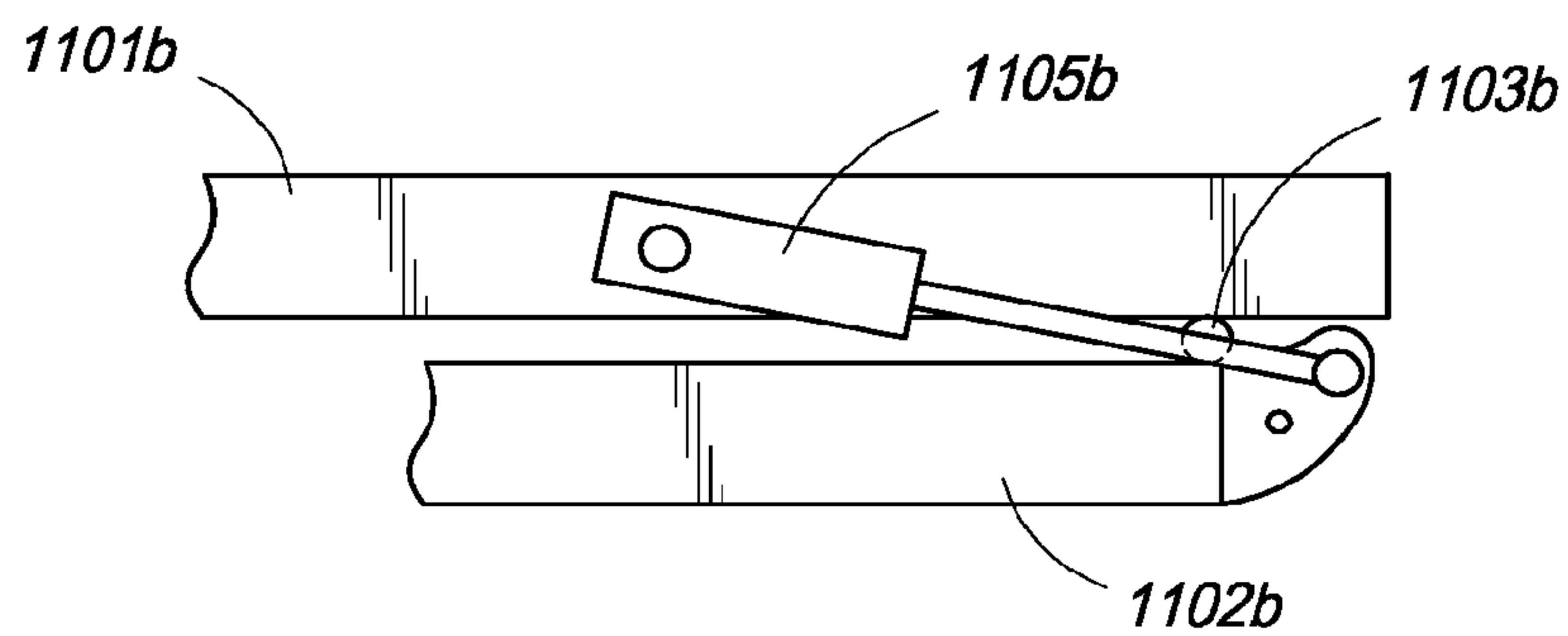
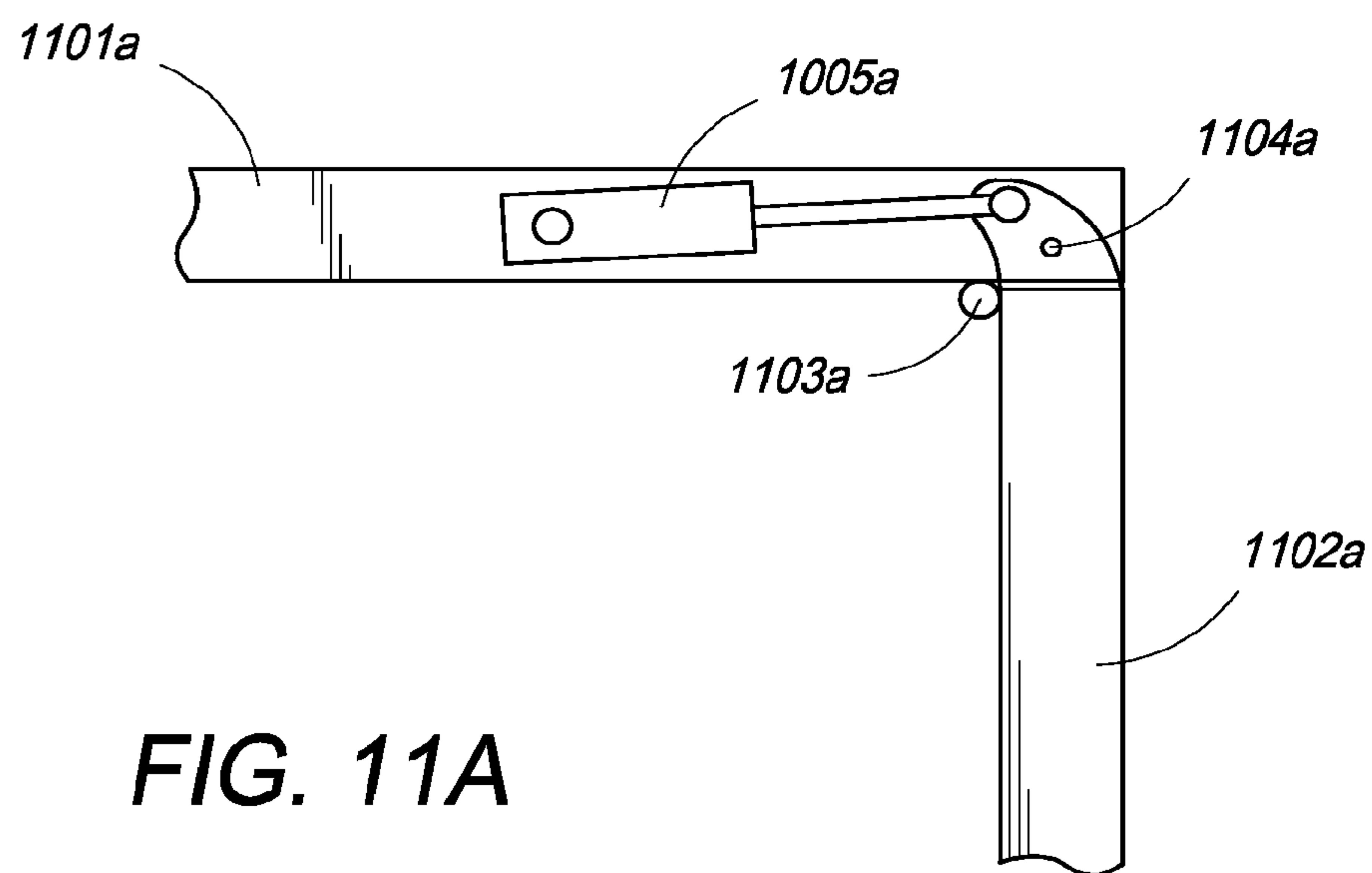












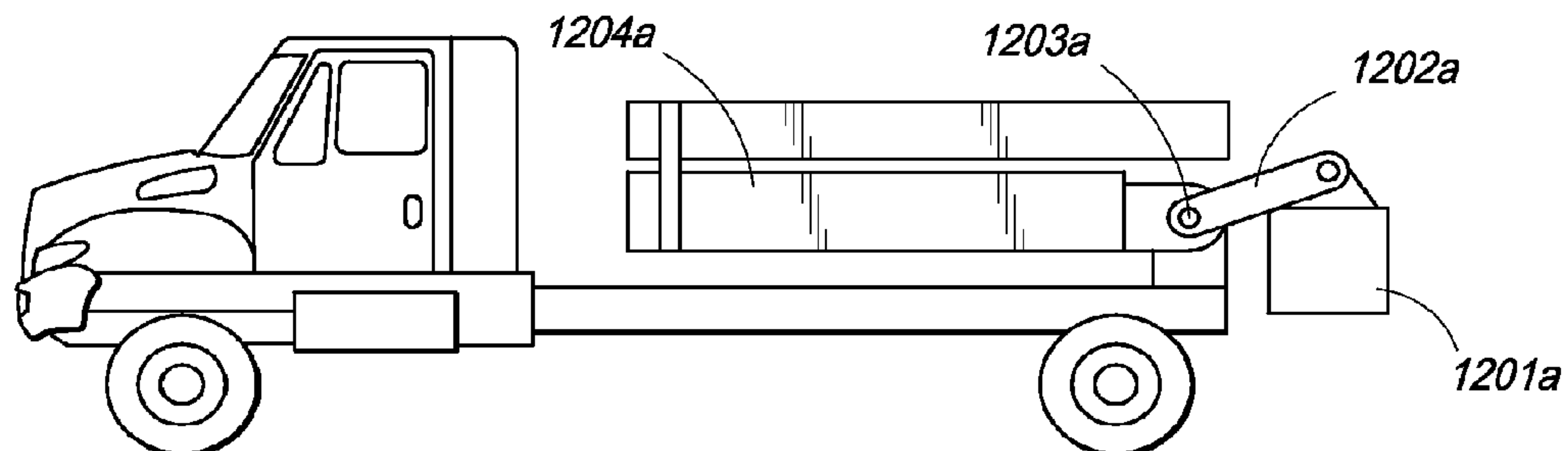


FIG. 12A

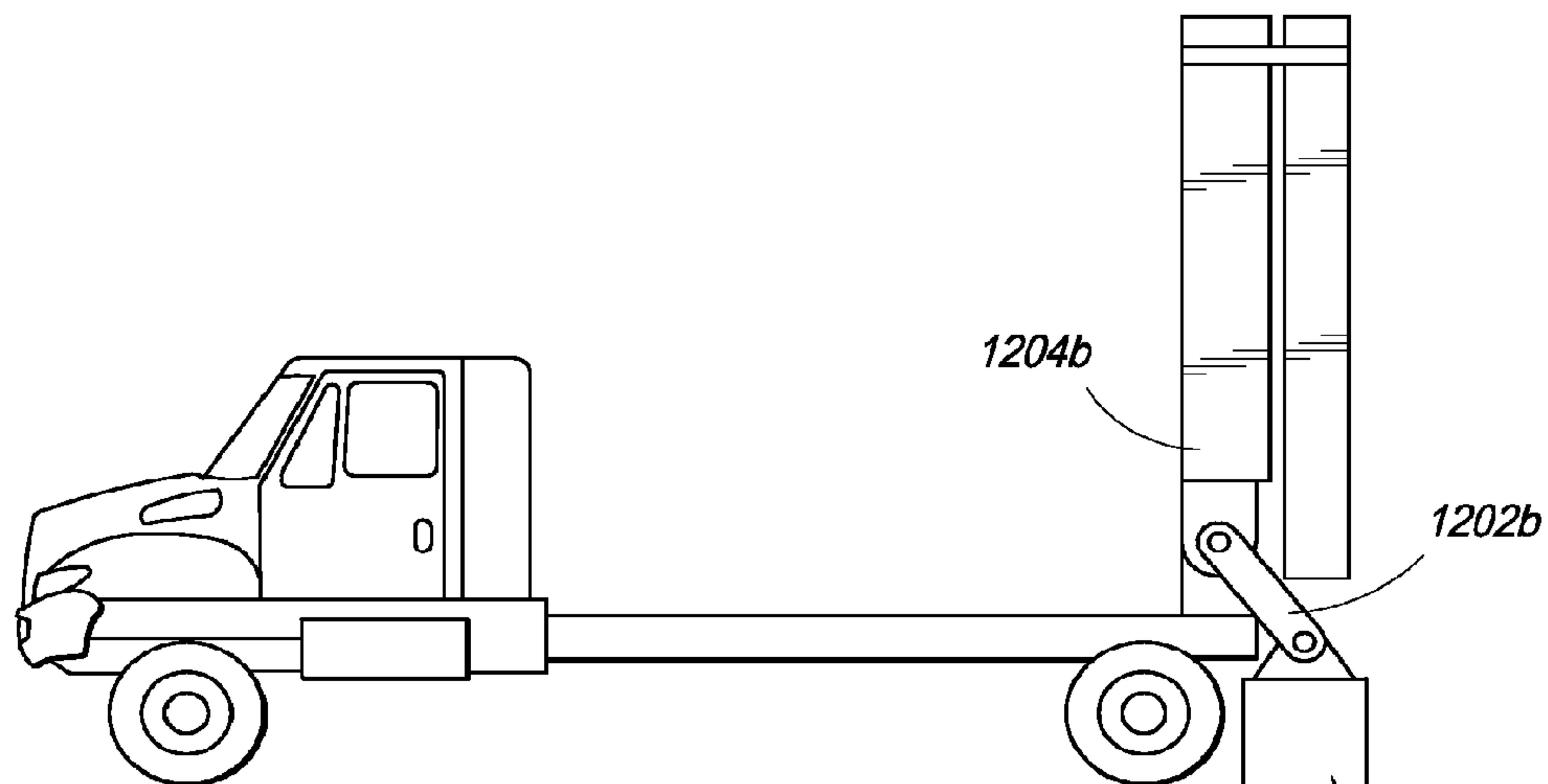


FIG. 12B

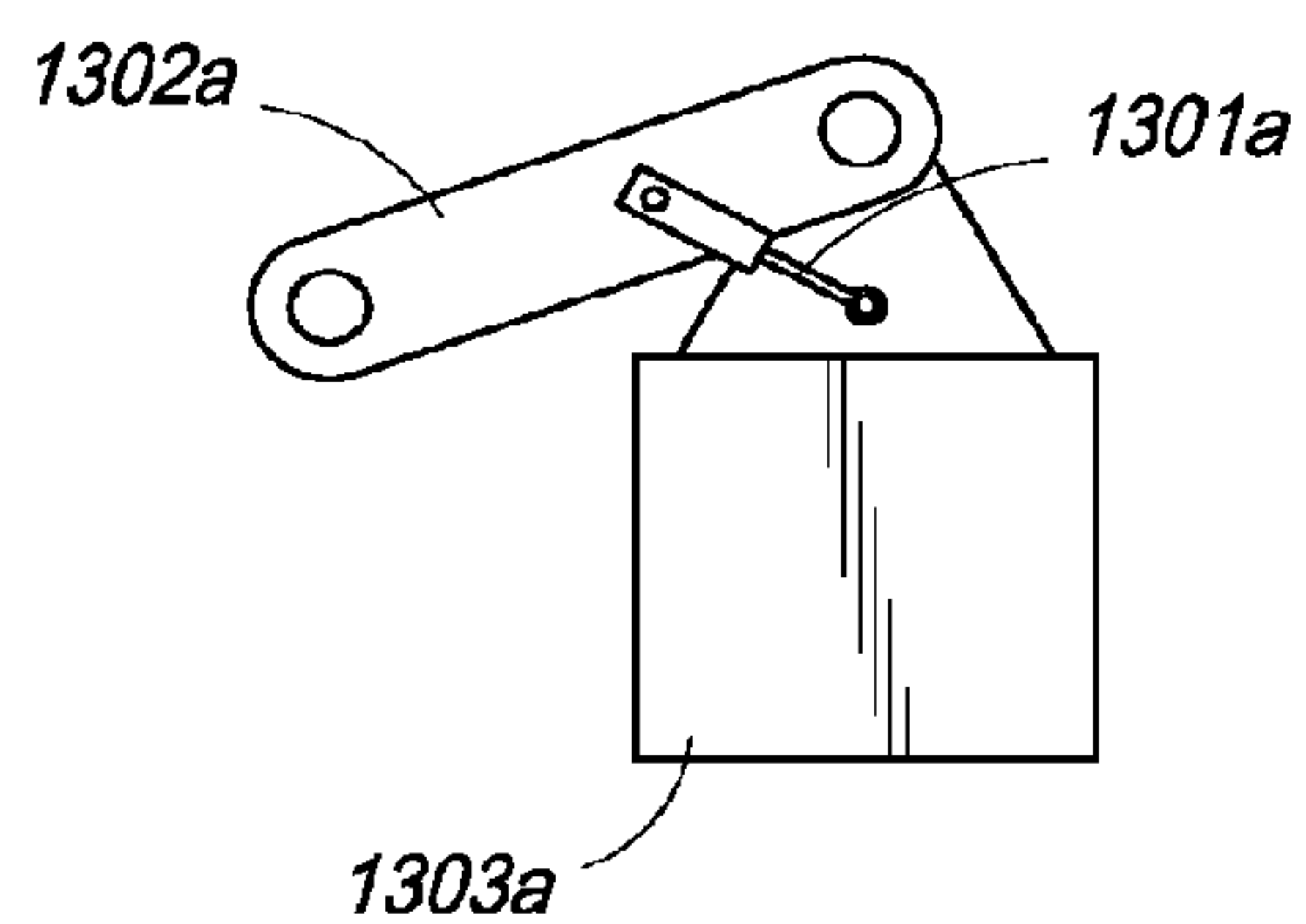


FIG. 13A

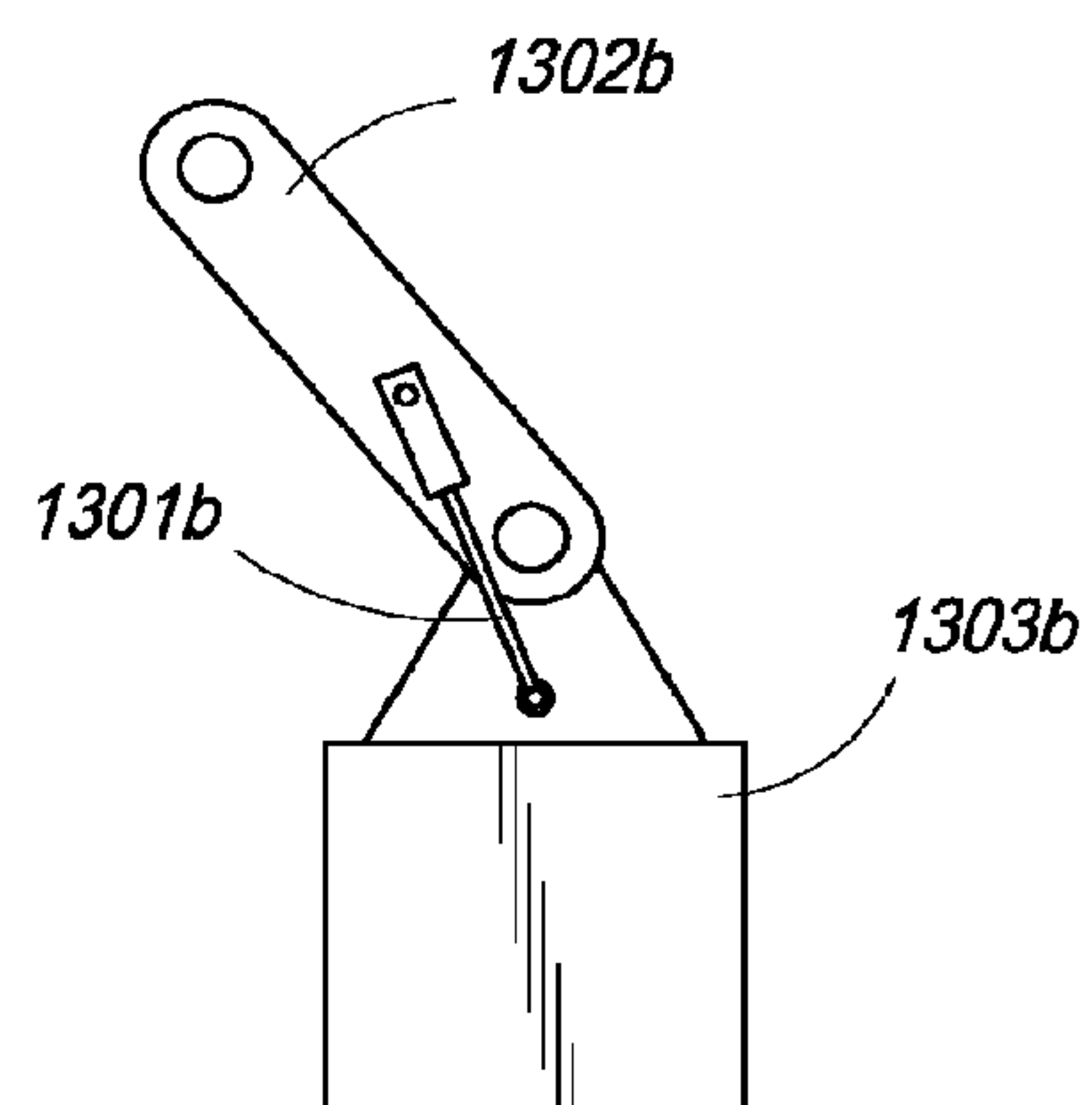


FIG. 13B



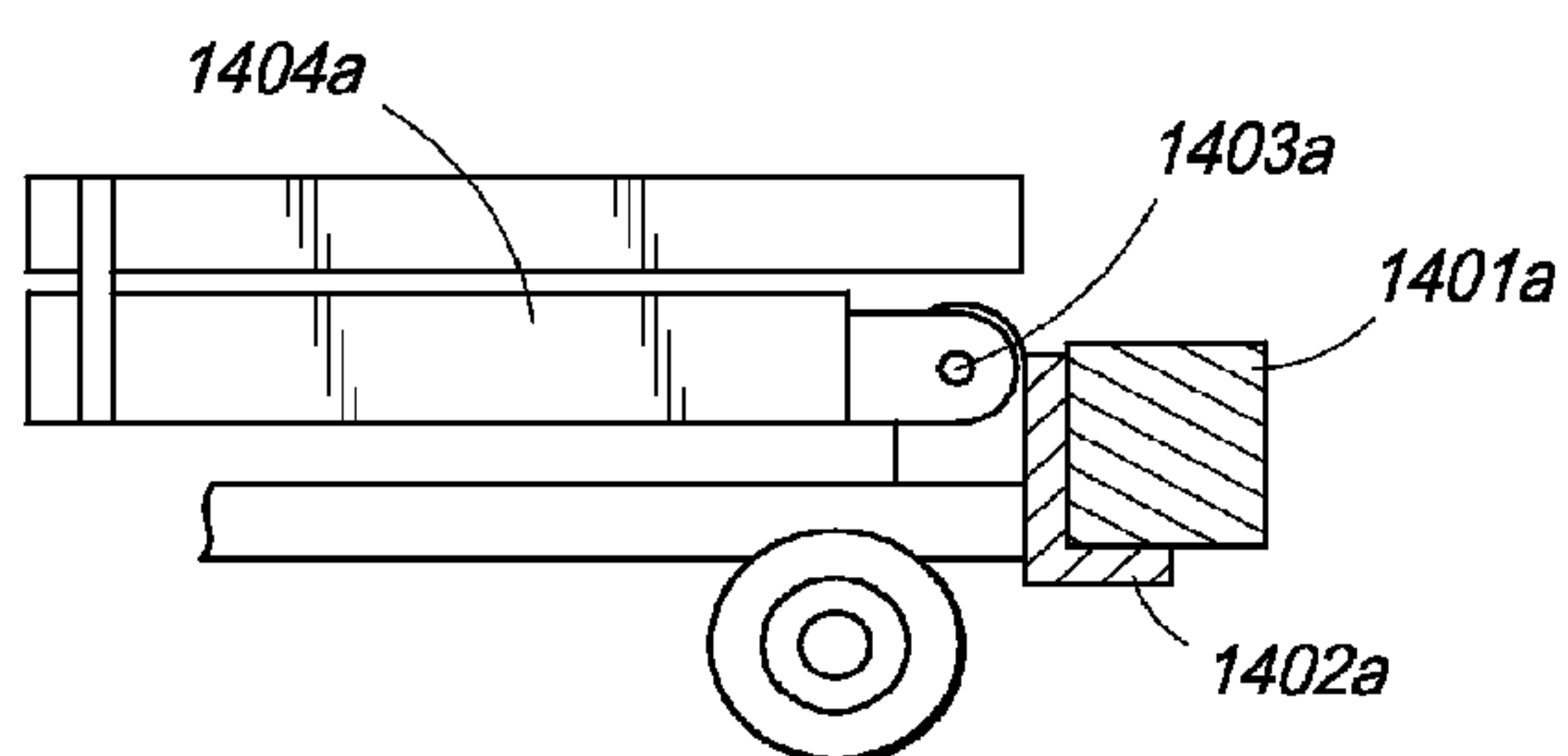


FIG. 14A

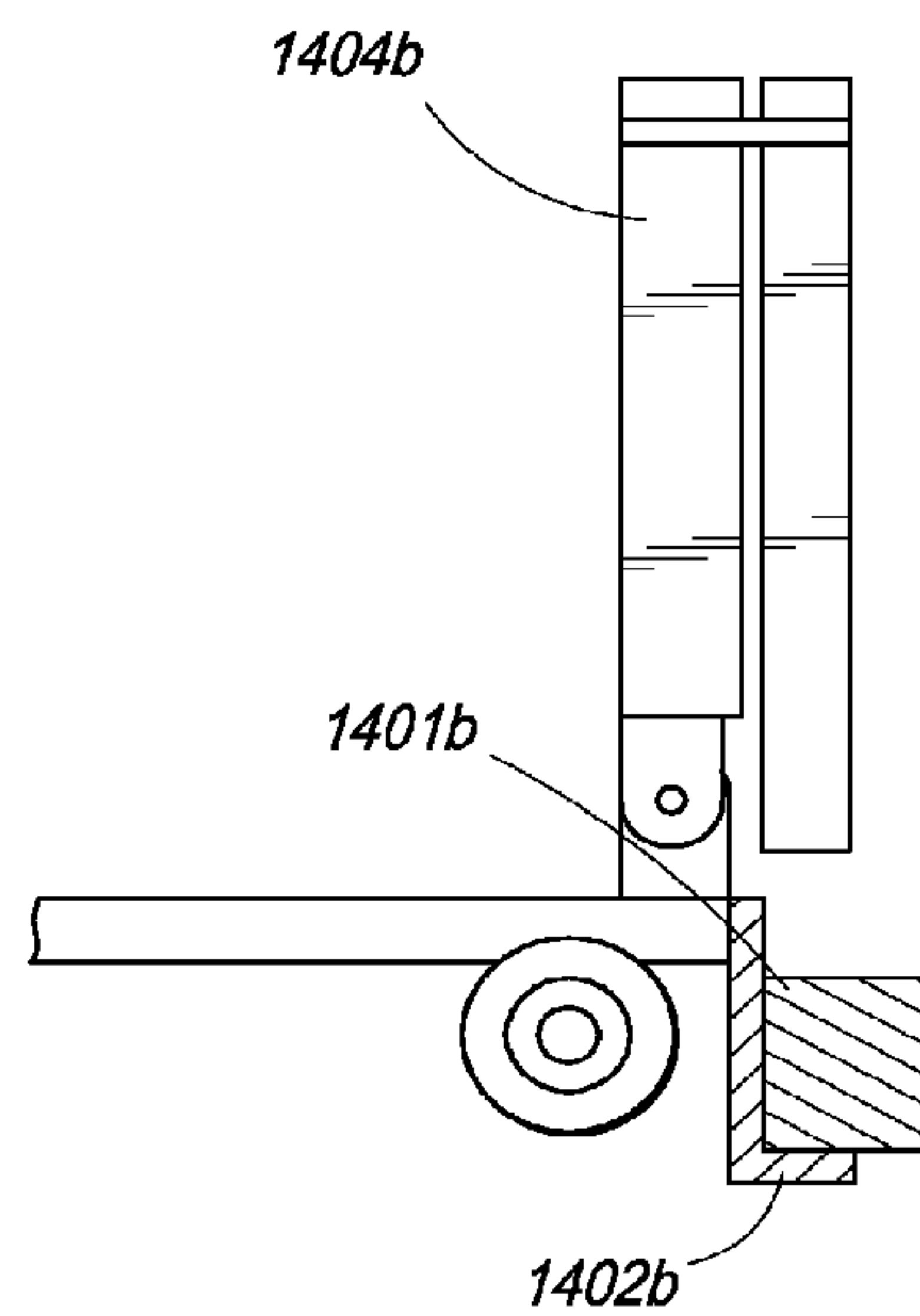


FIG. 14B

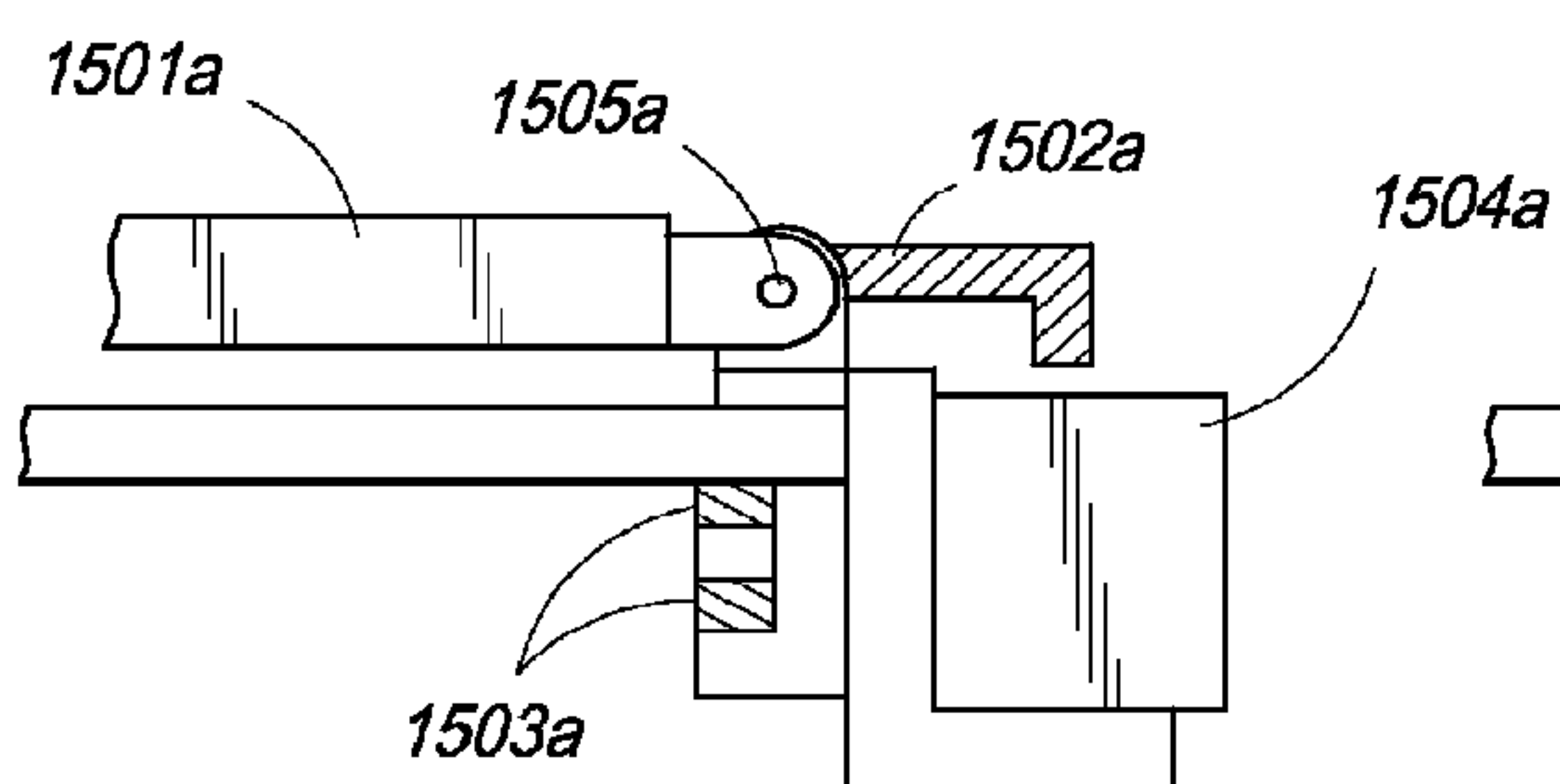


FIG. 15A

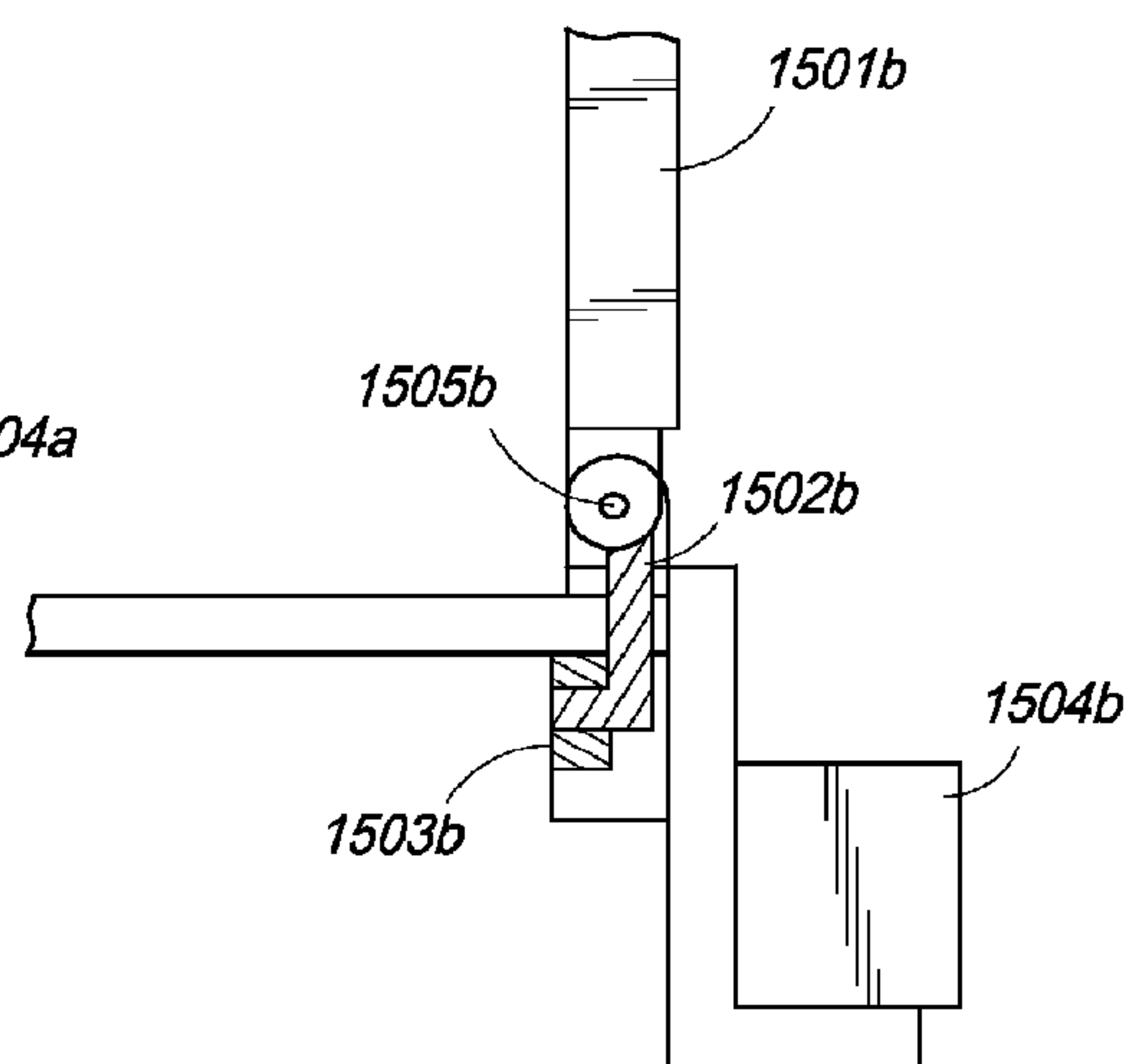


FIG. 15B

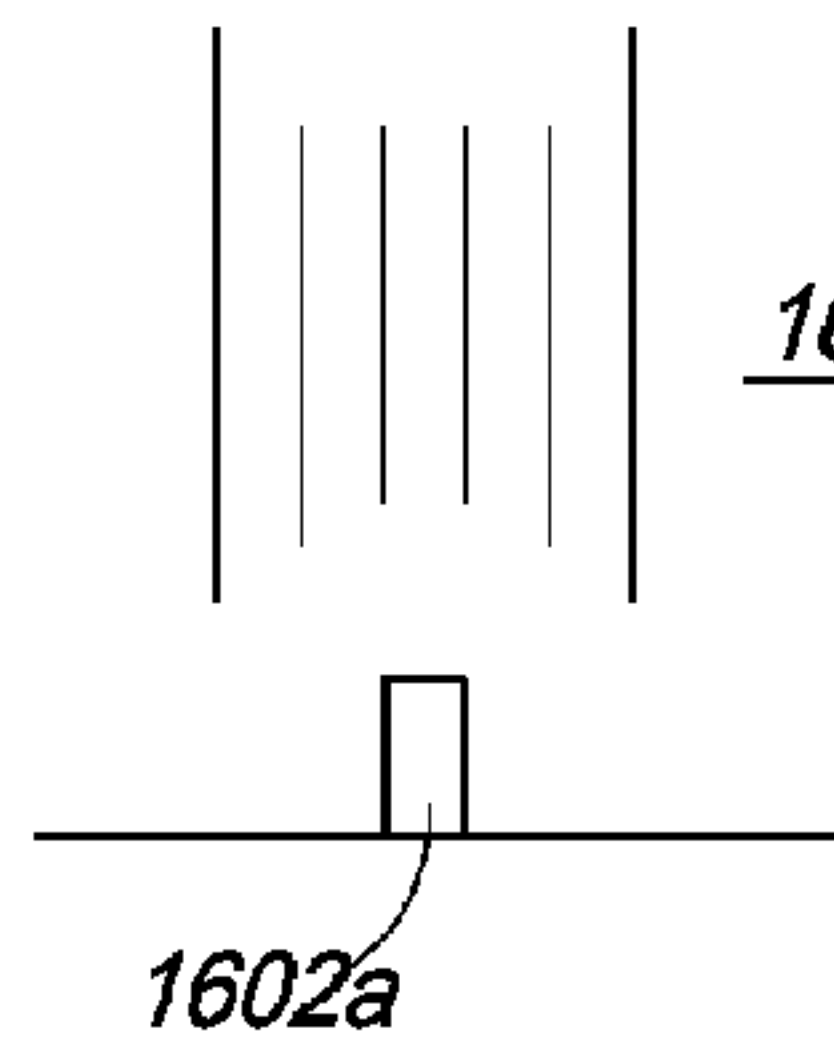


FIG. 16A

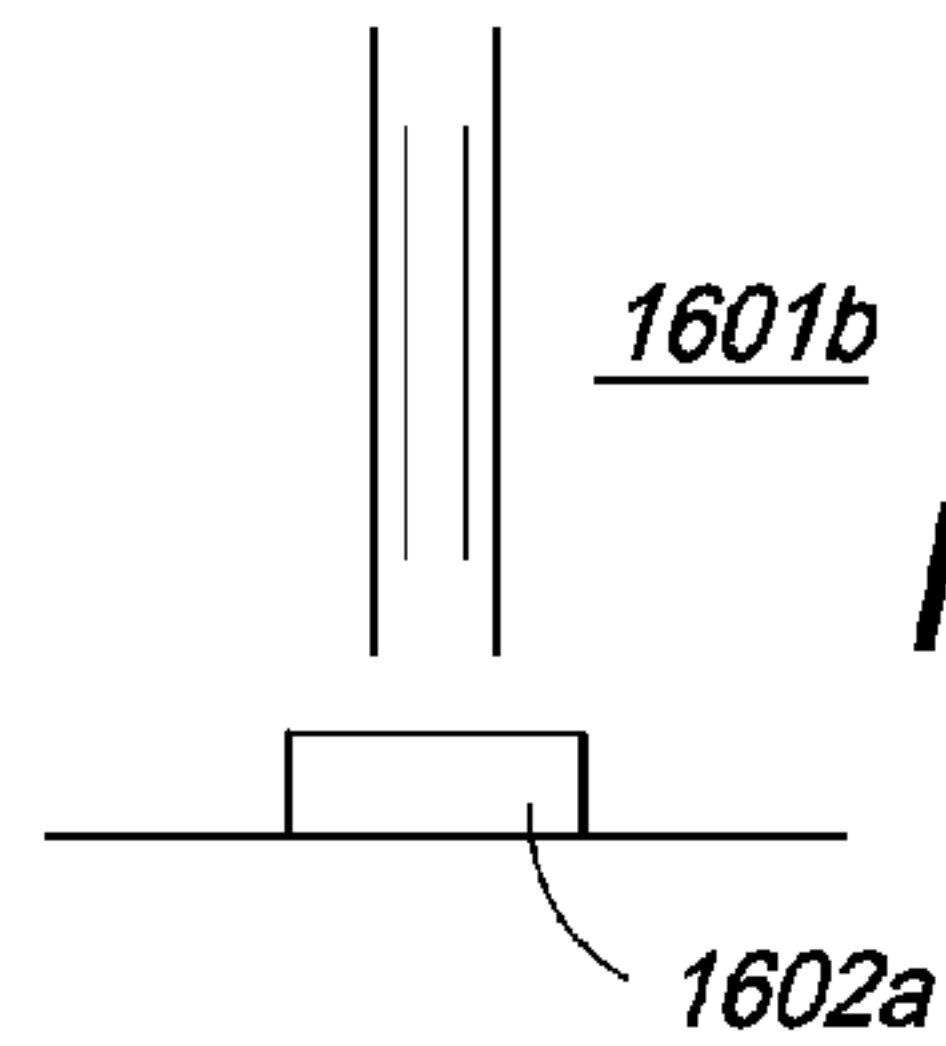


FIG. 16B

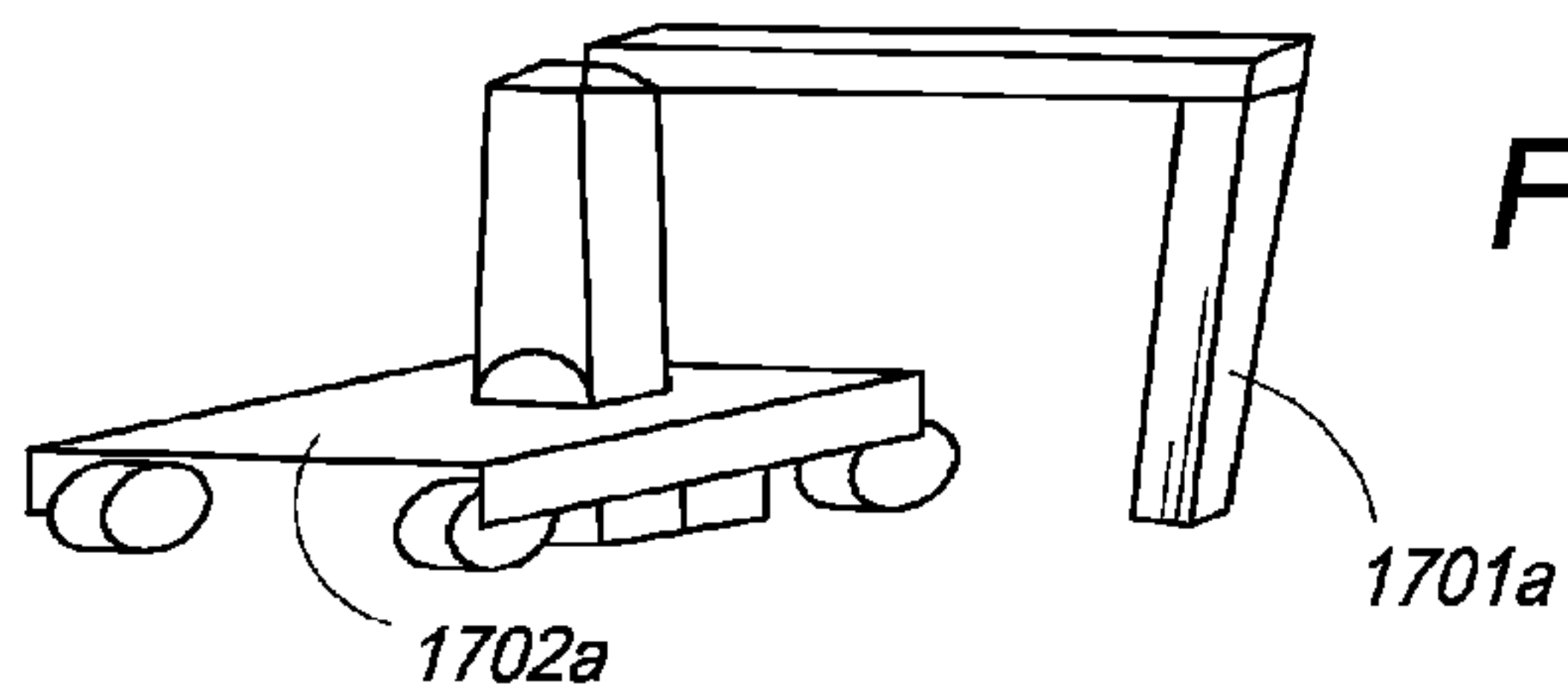


FIG. 17A

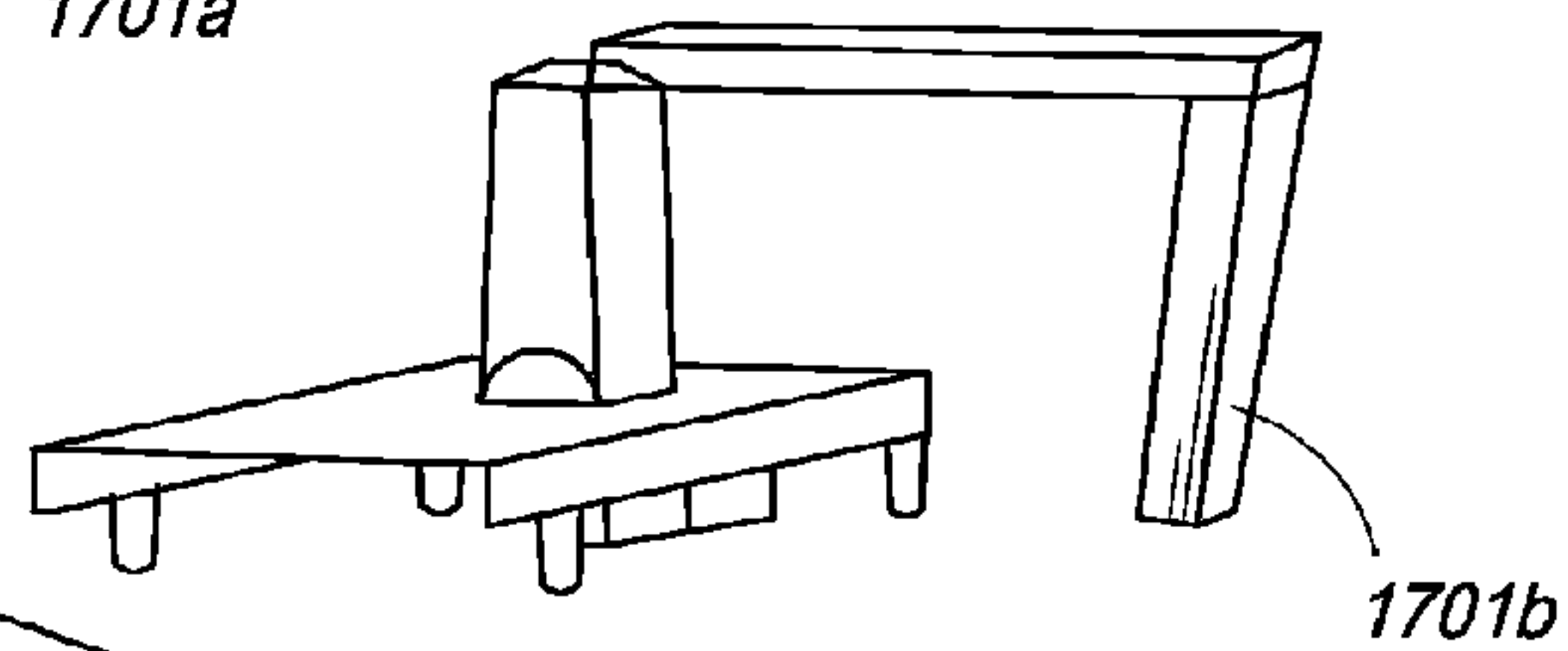


FIG. 17B

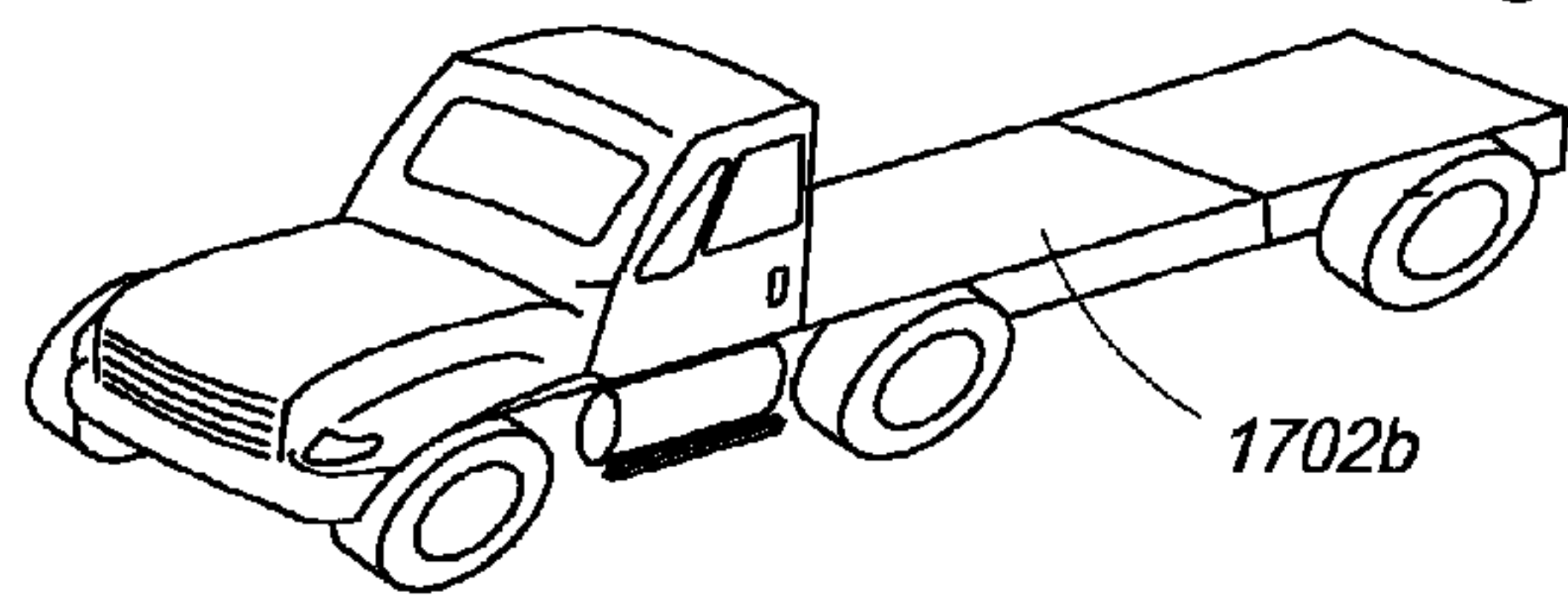


FIG. 17C

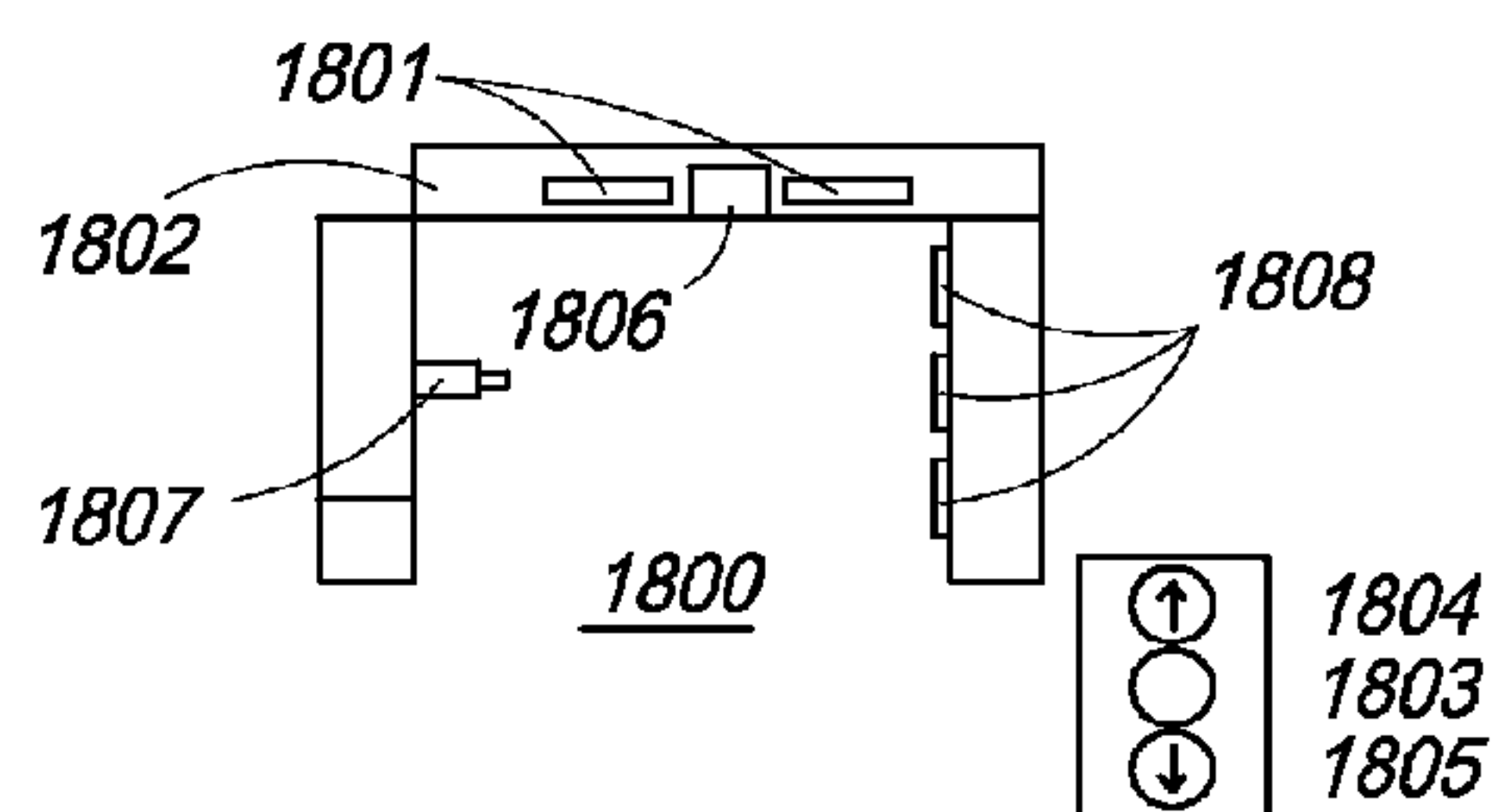


FIG. 18



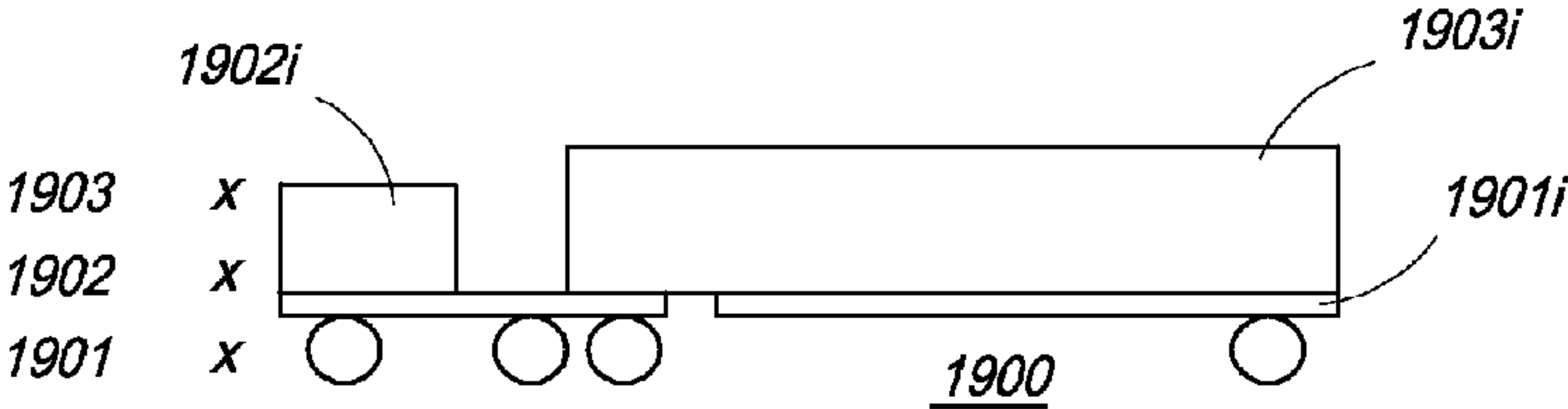


FIG. 19

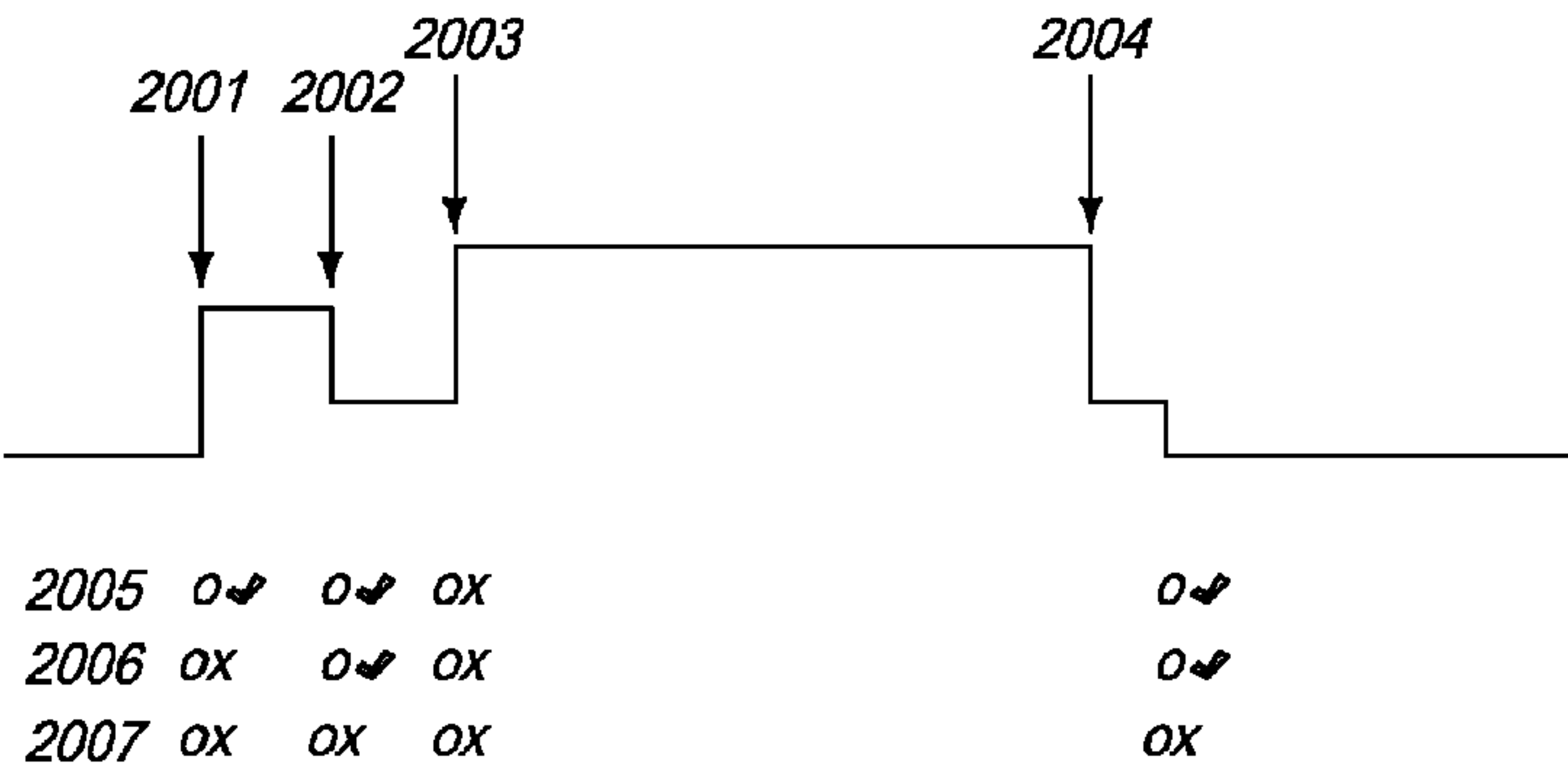


FIG. 20

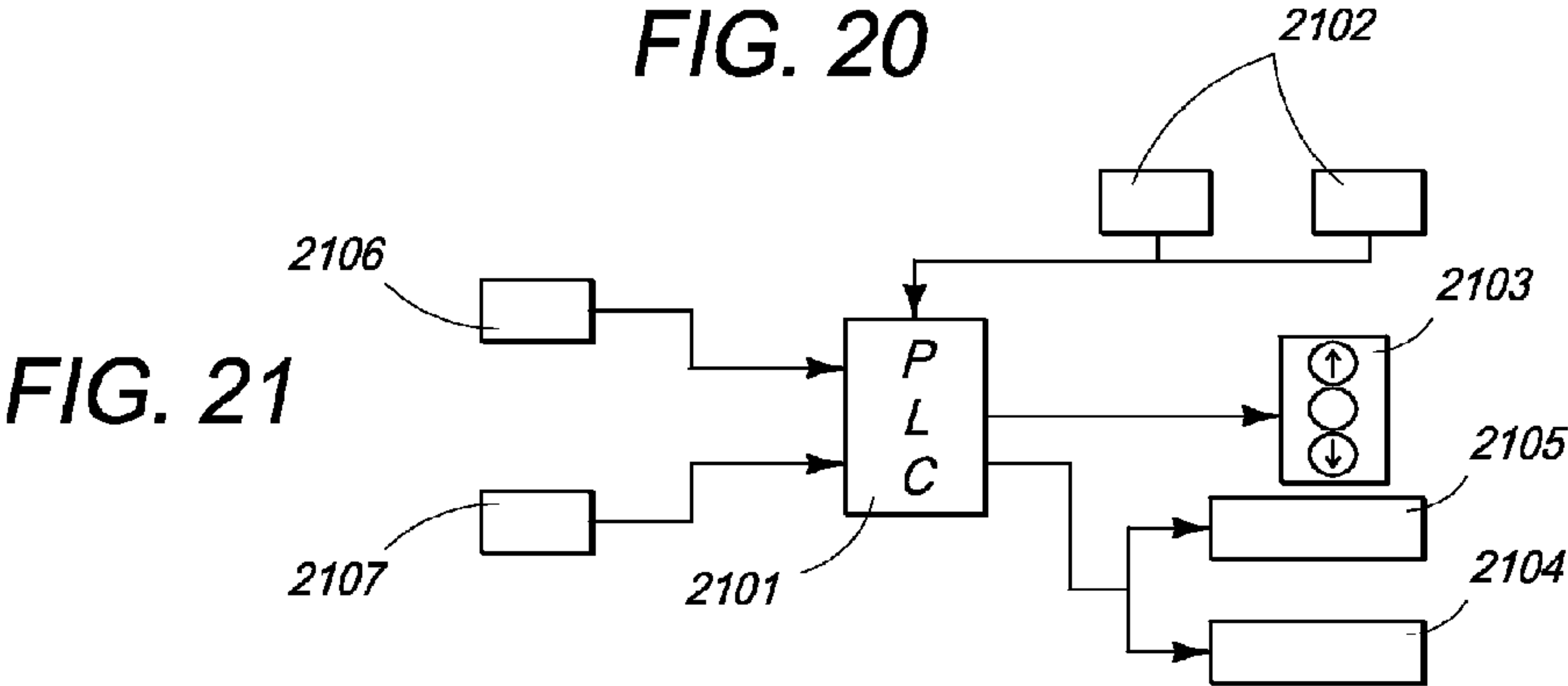


FIG. 21

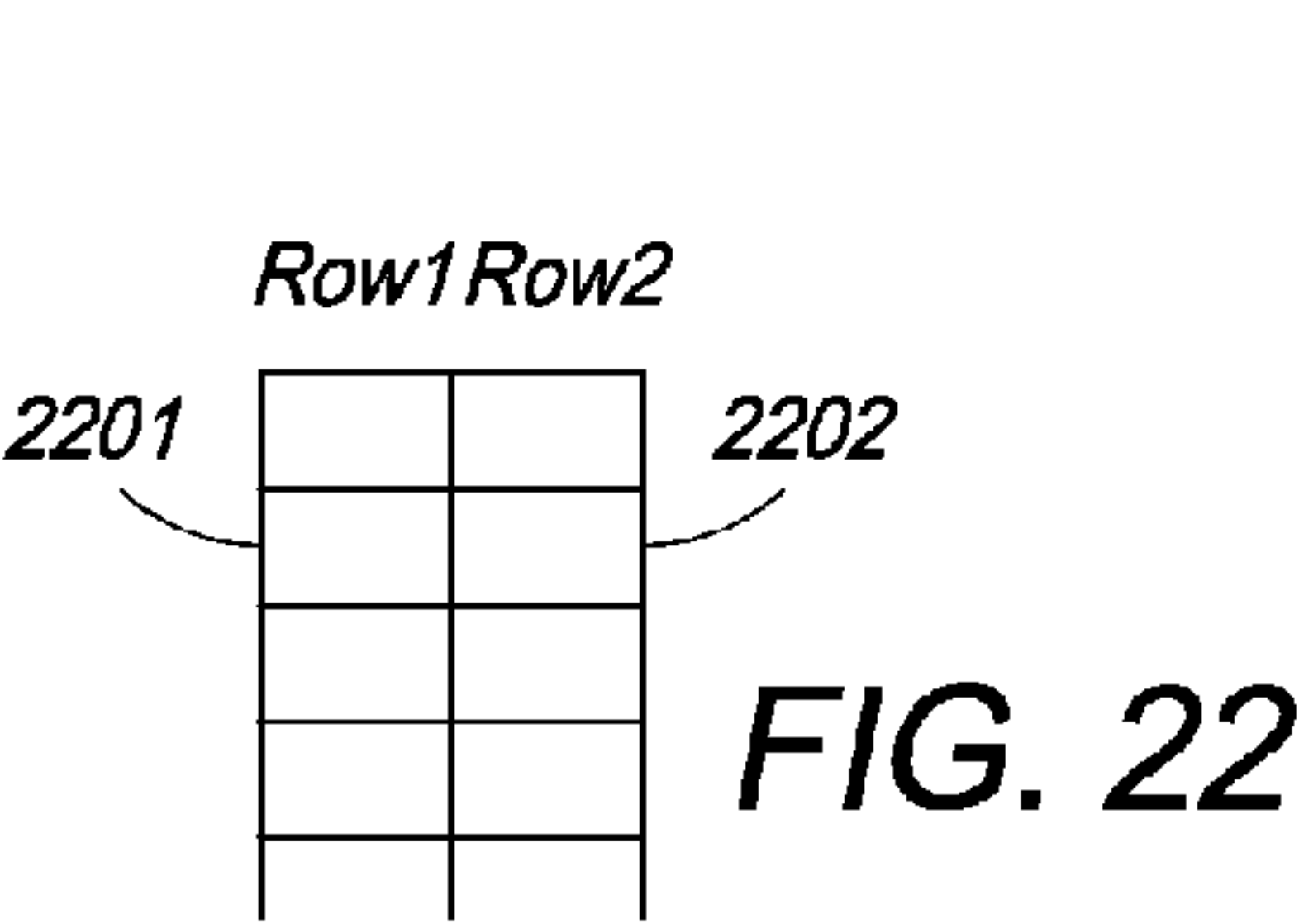


FIG. 22

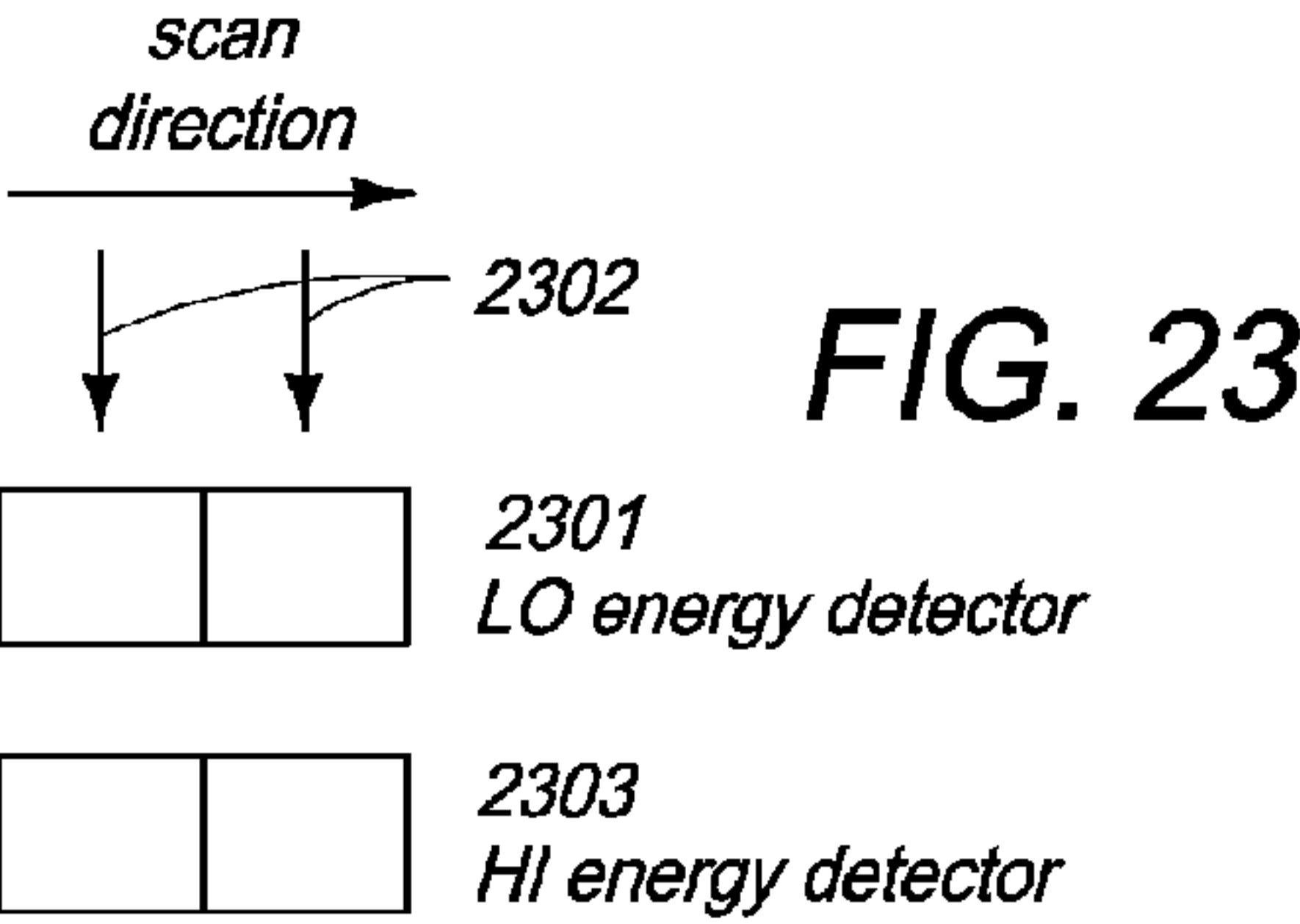


FIG. 23

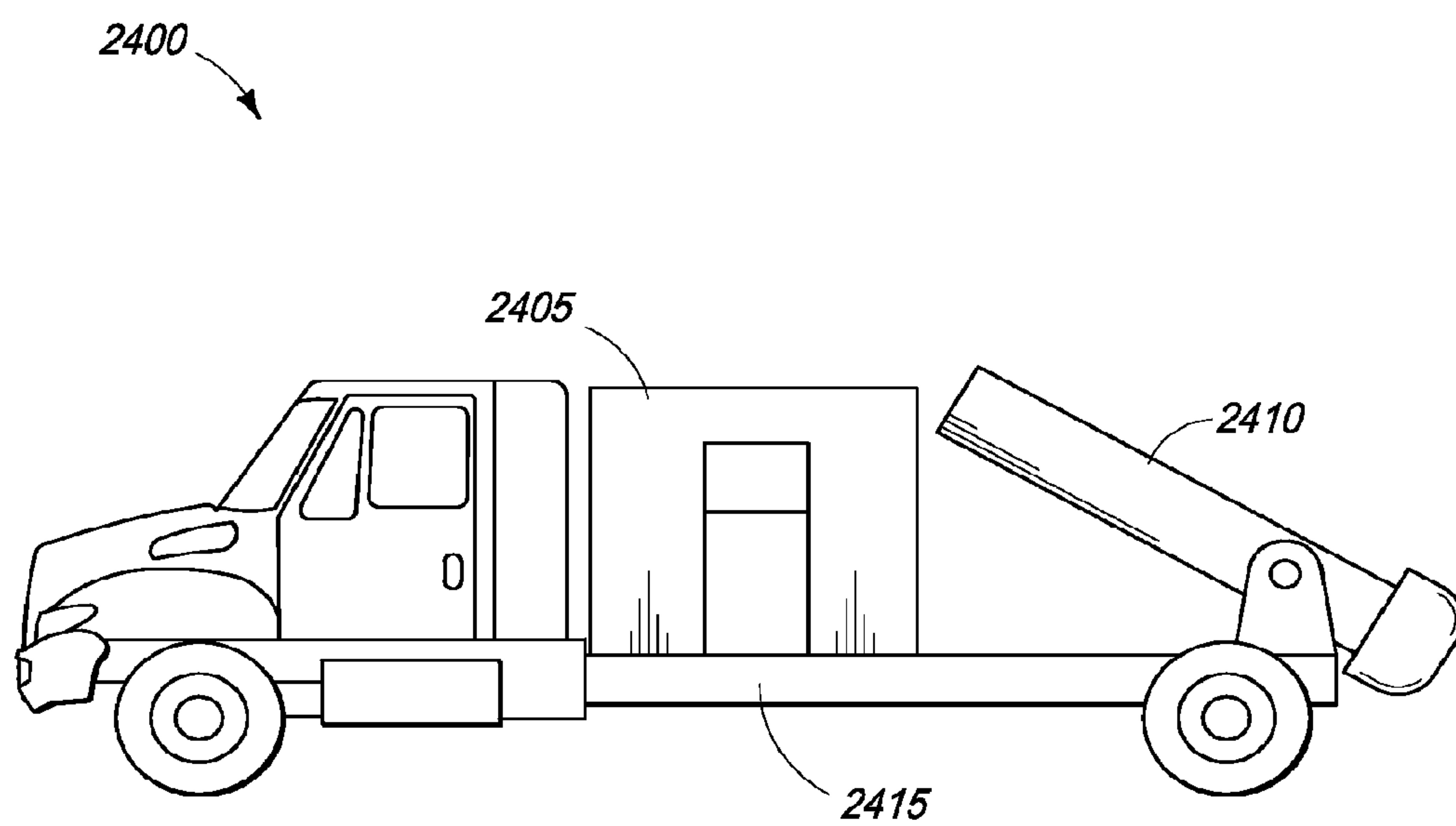
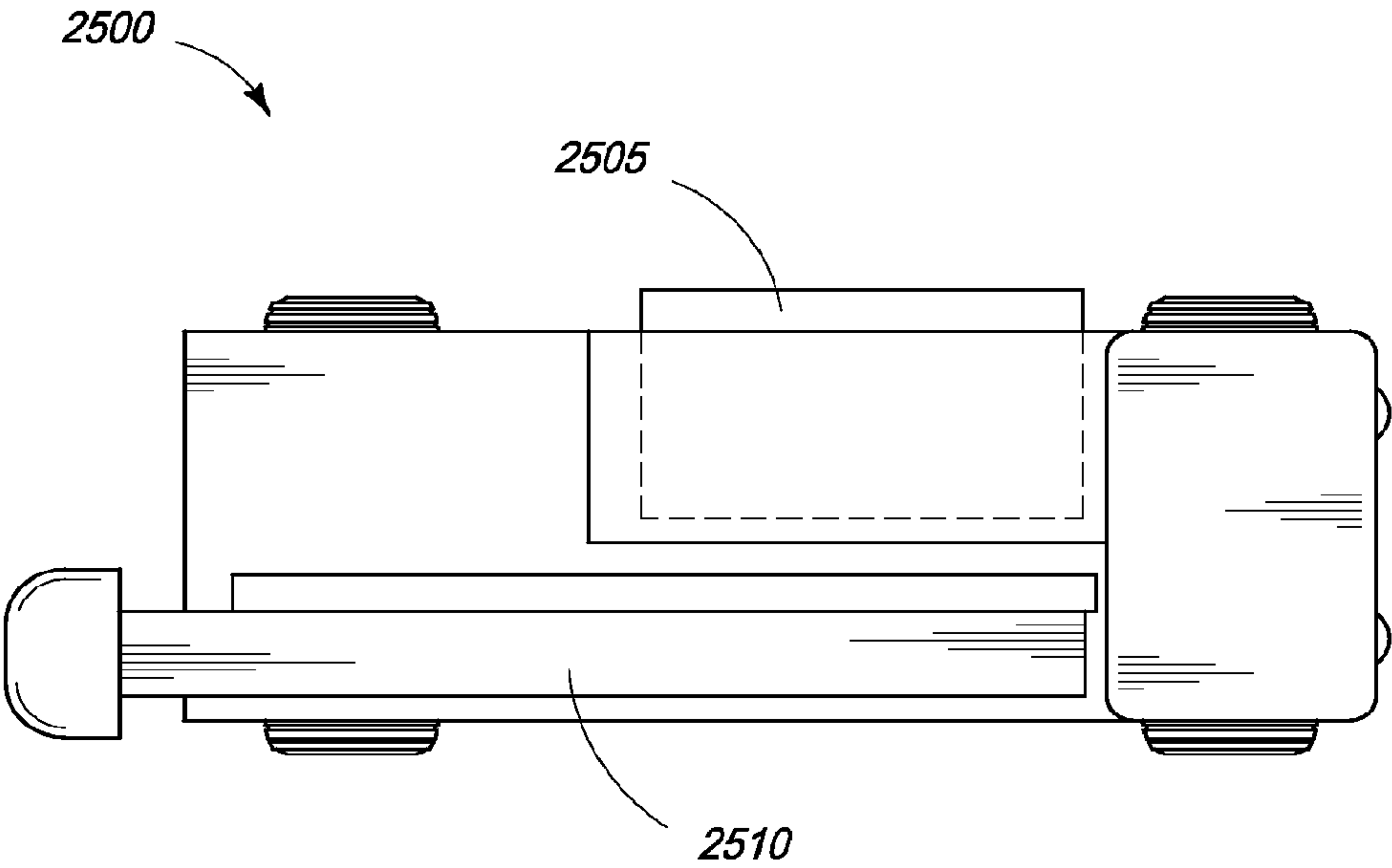
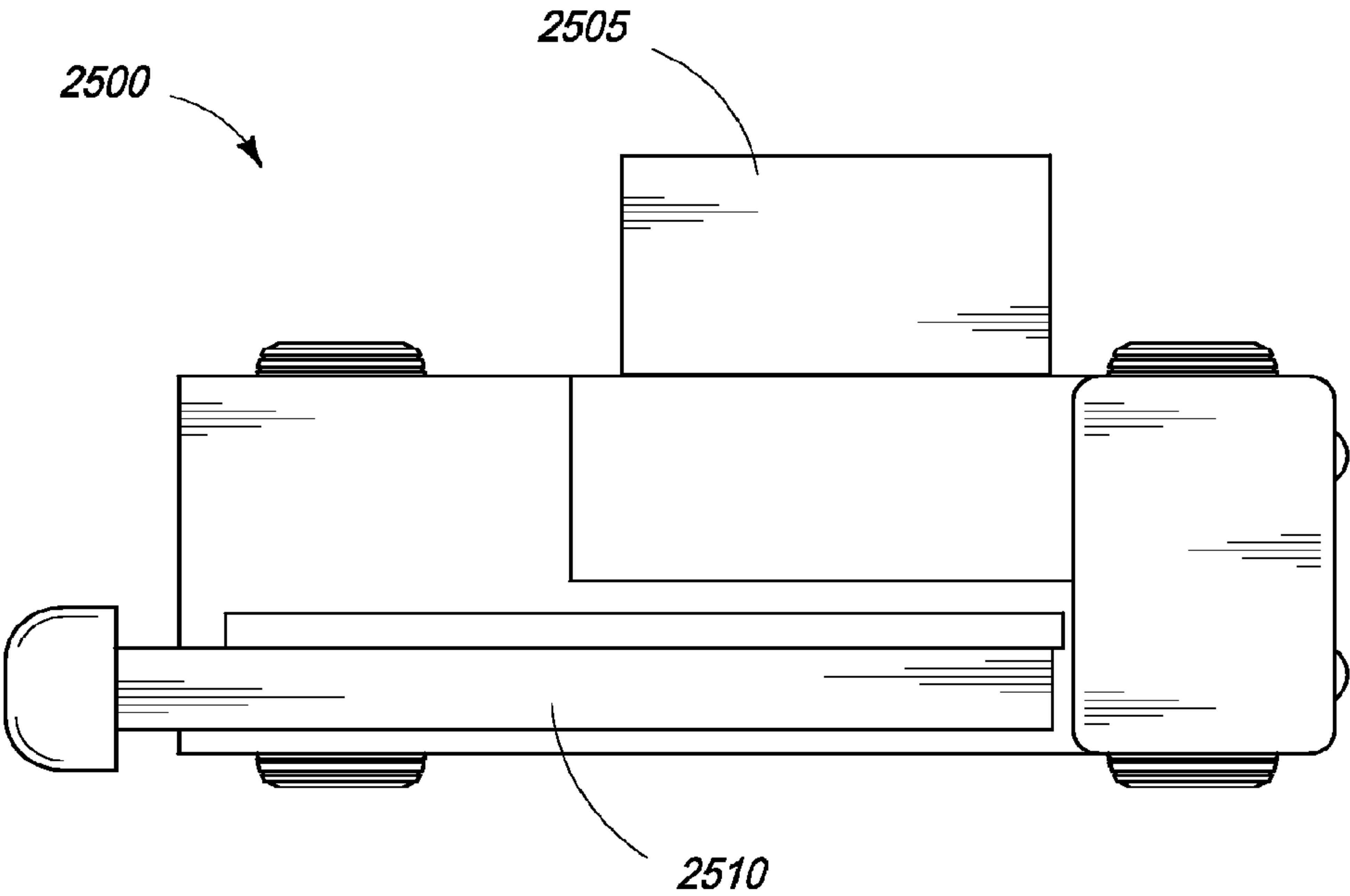


FIG. 24

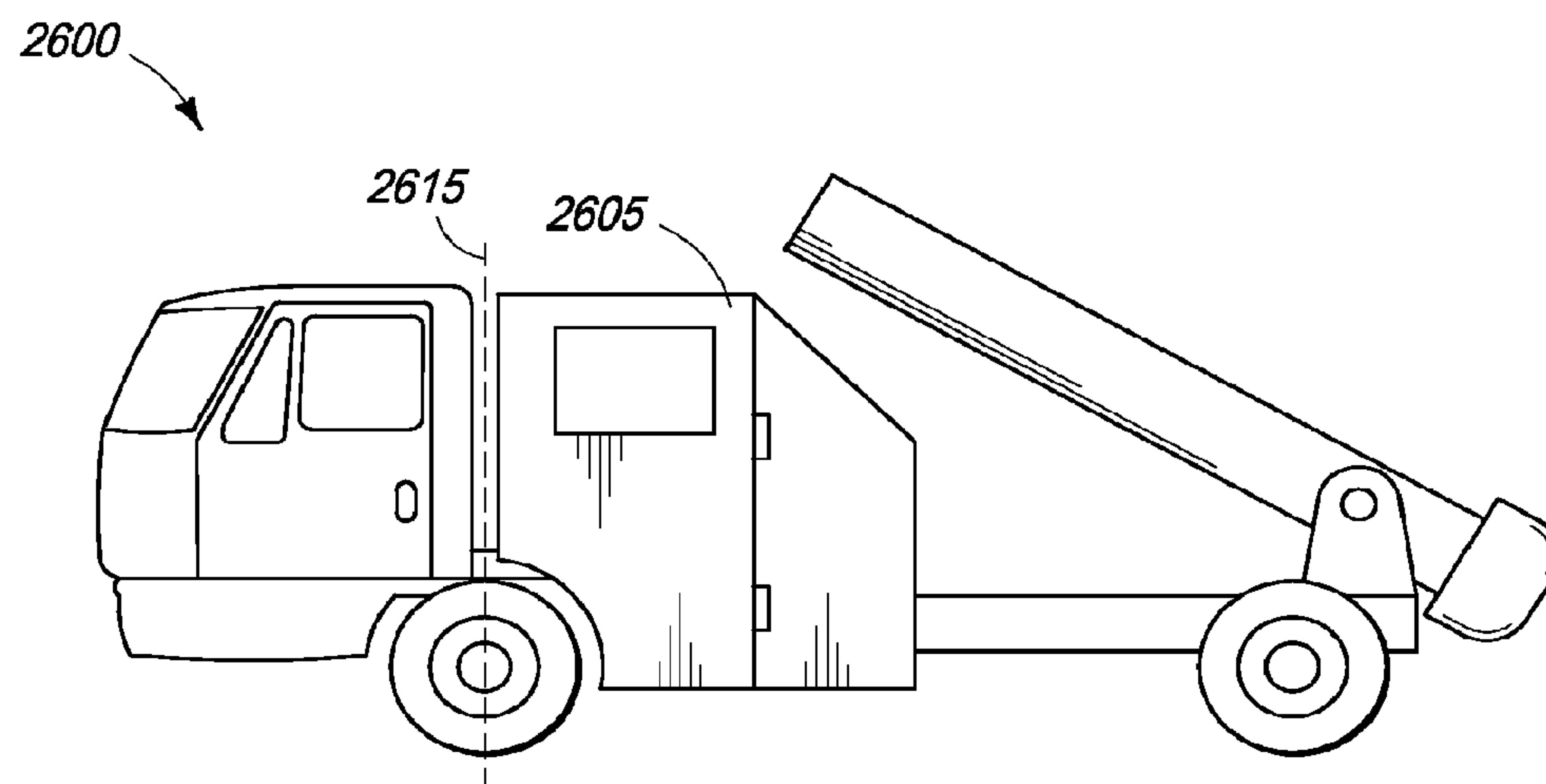


**FIG. 25A**

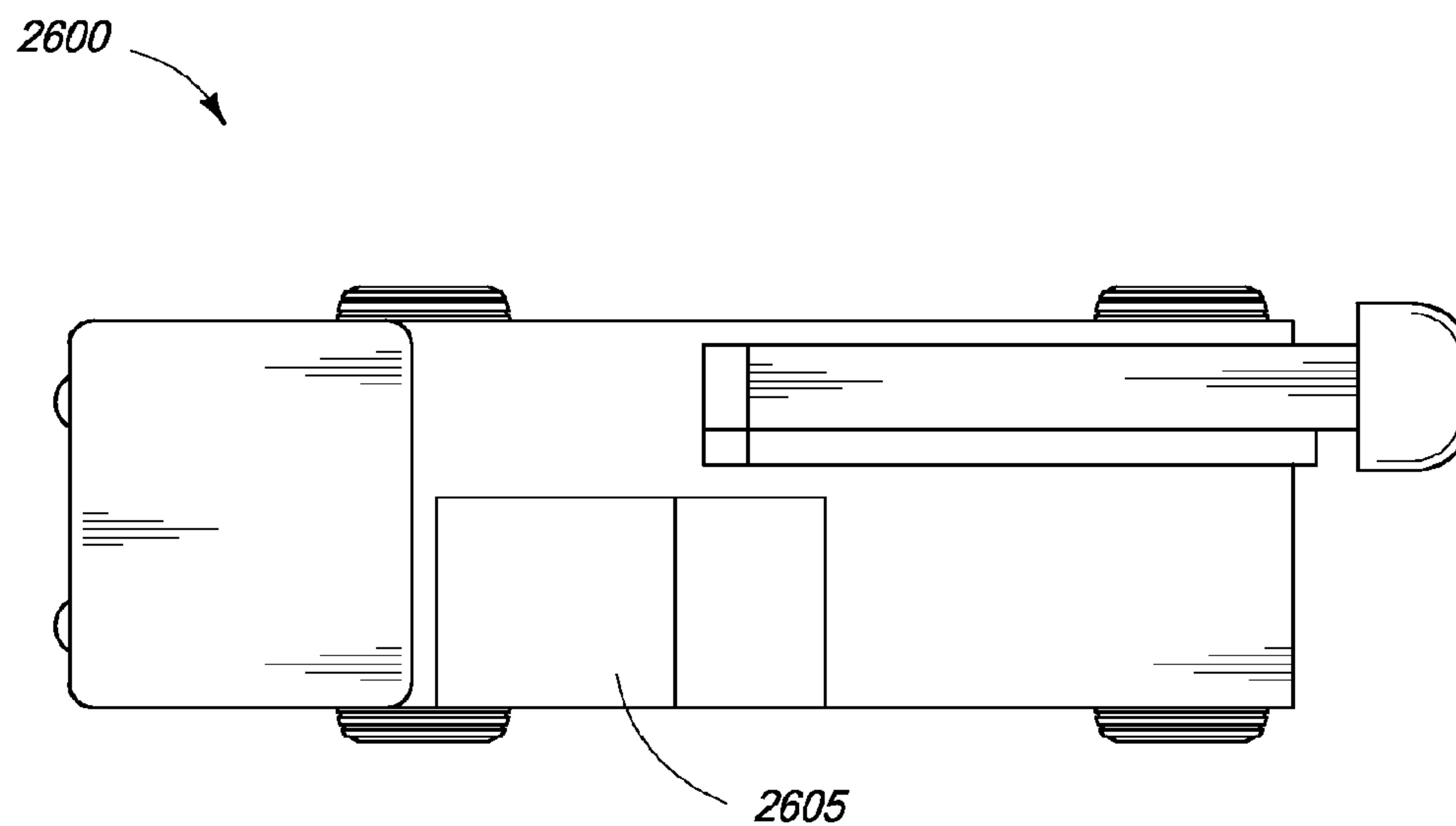


**FIG. 25B**





**FIG. 26A**



**FIG. 26B**

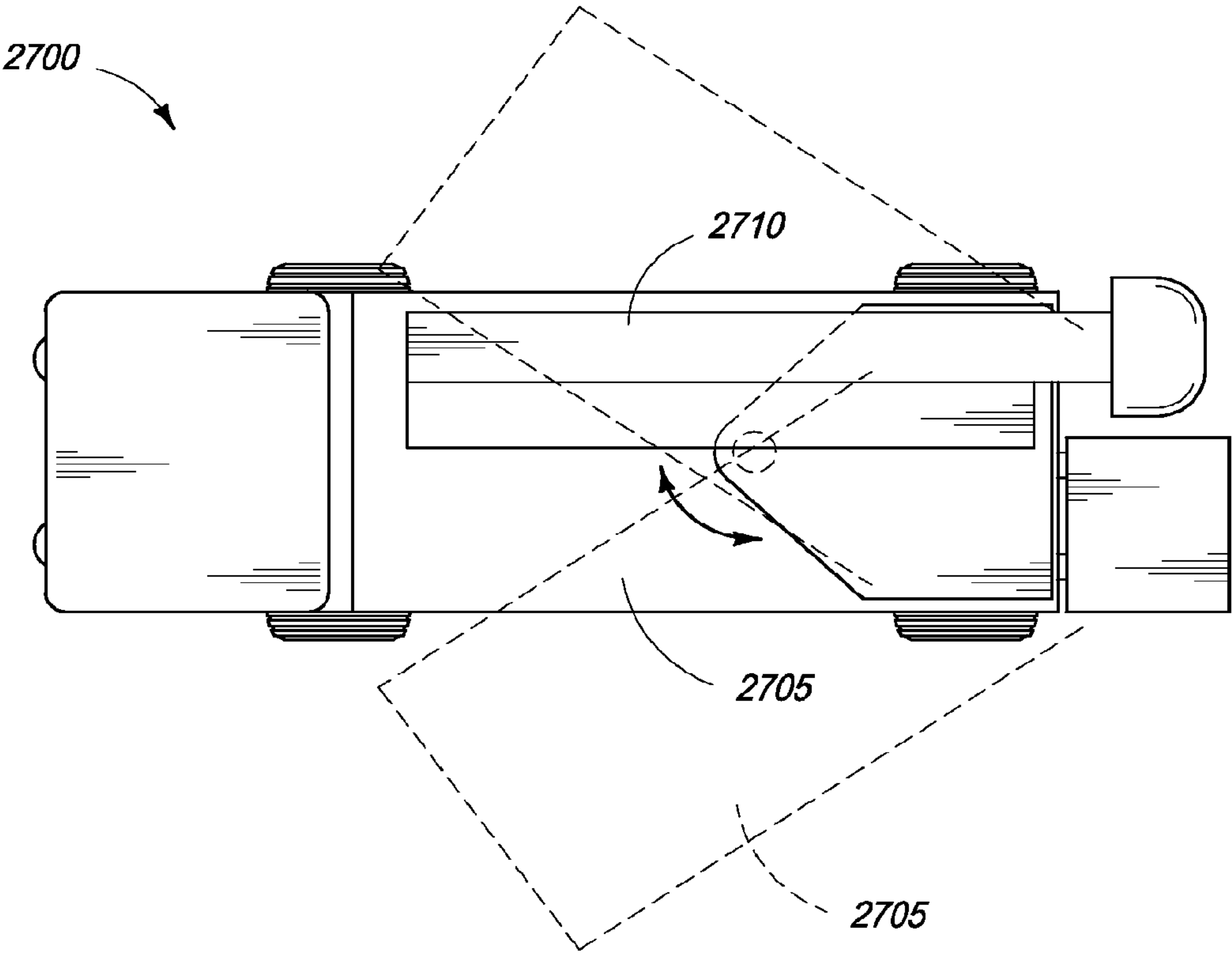


FIG. 27

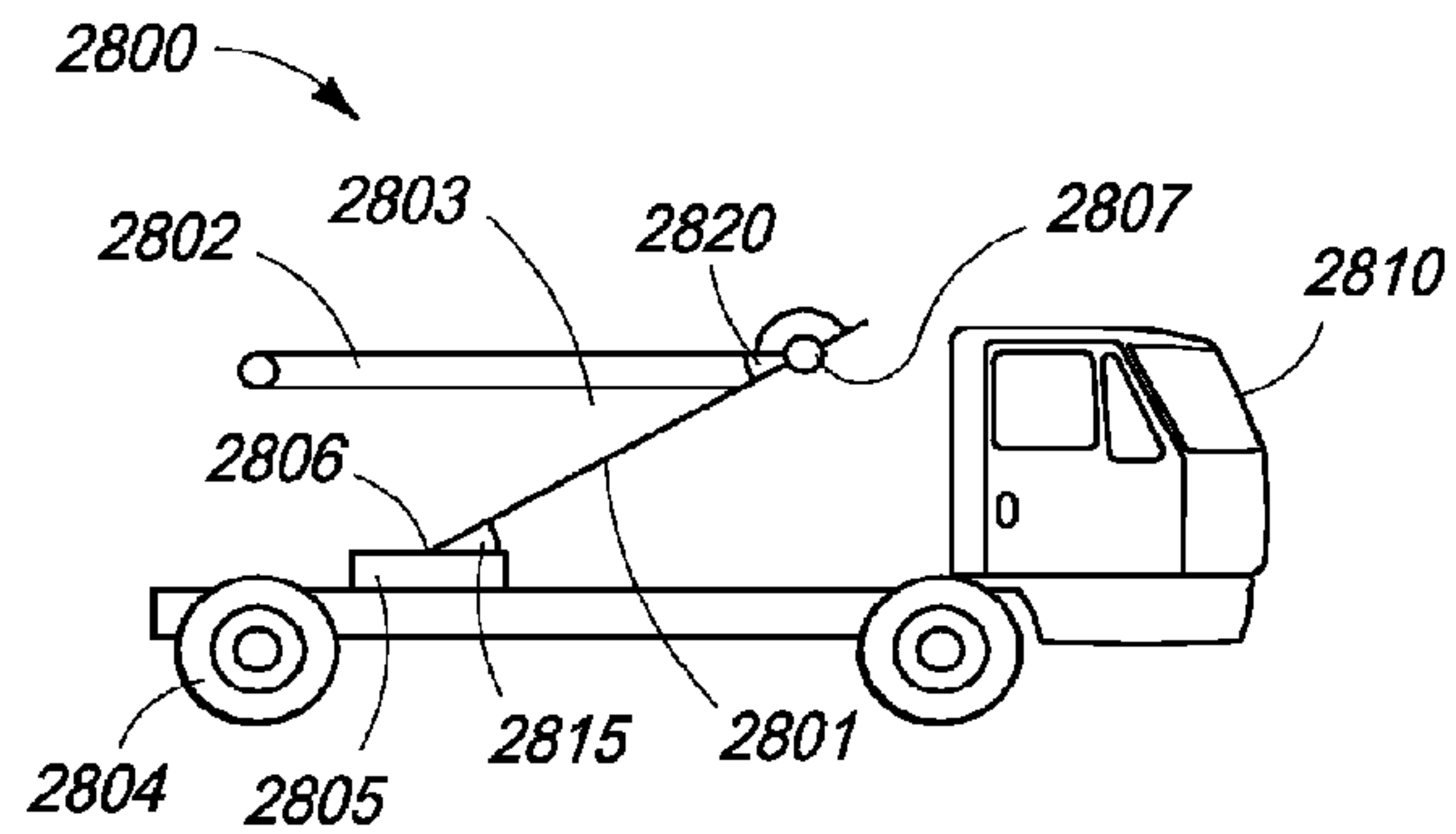


FIG. 28A

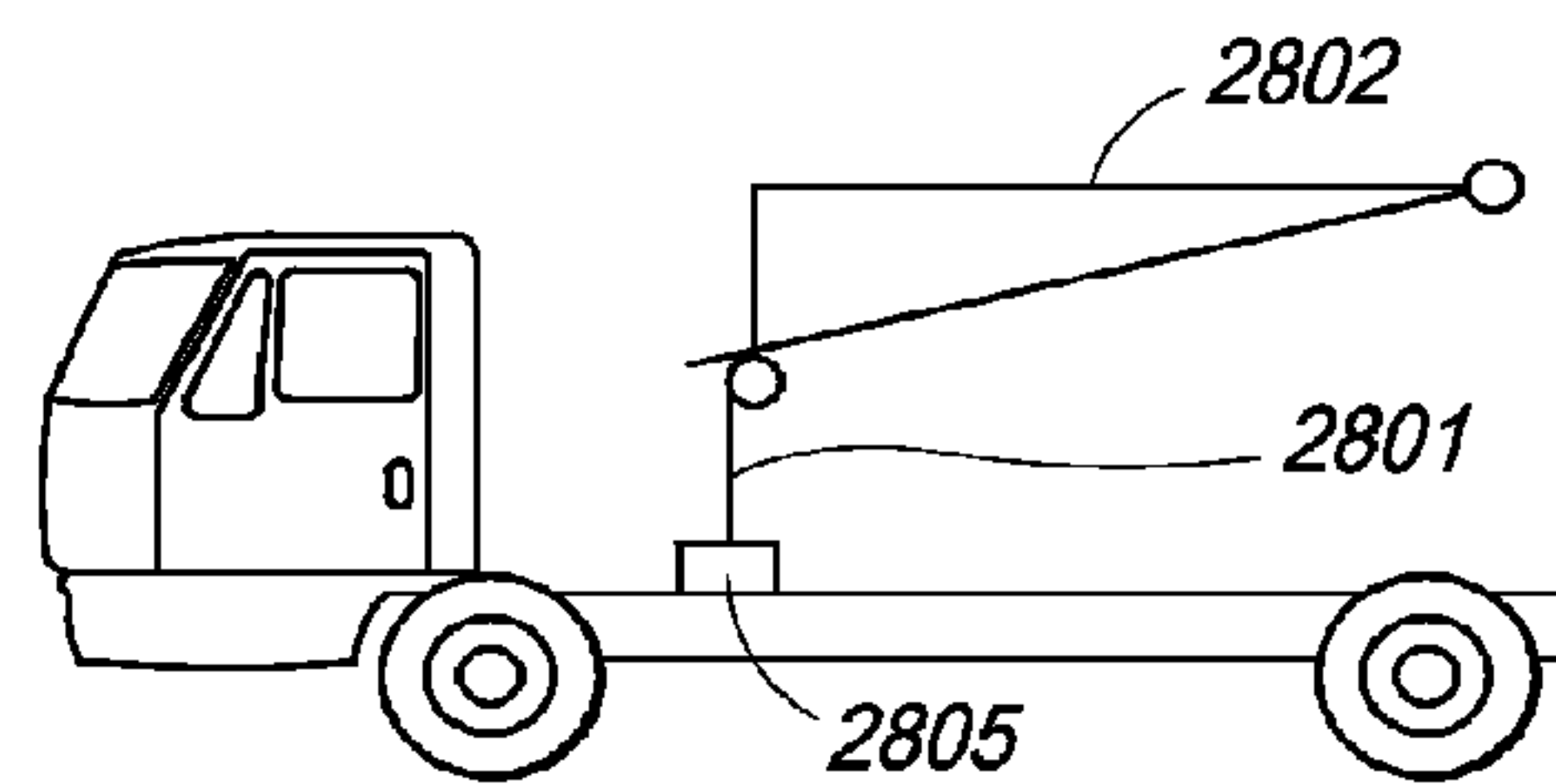


FIG. 28B

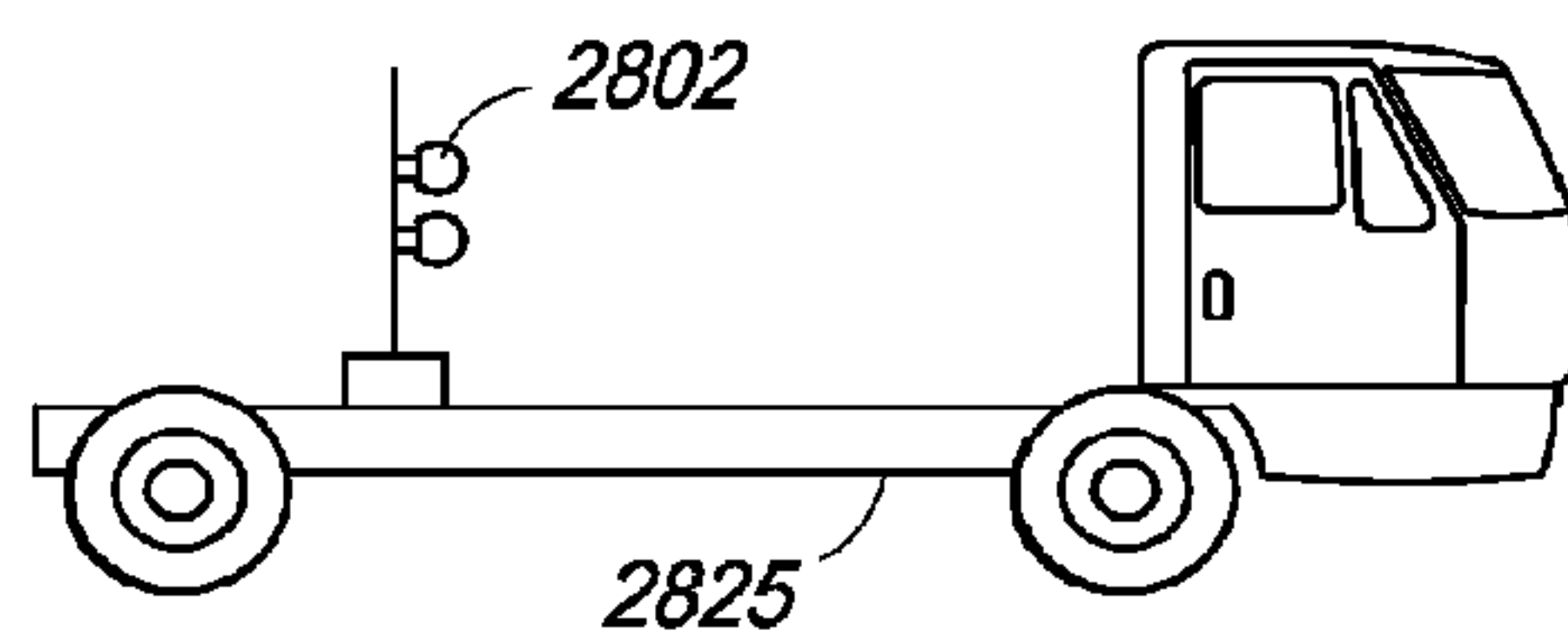


FIG. 28C

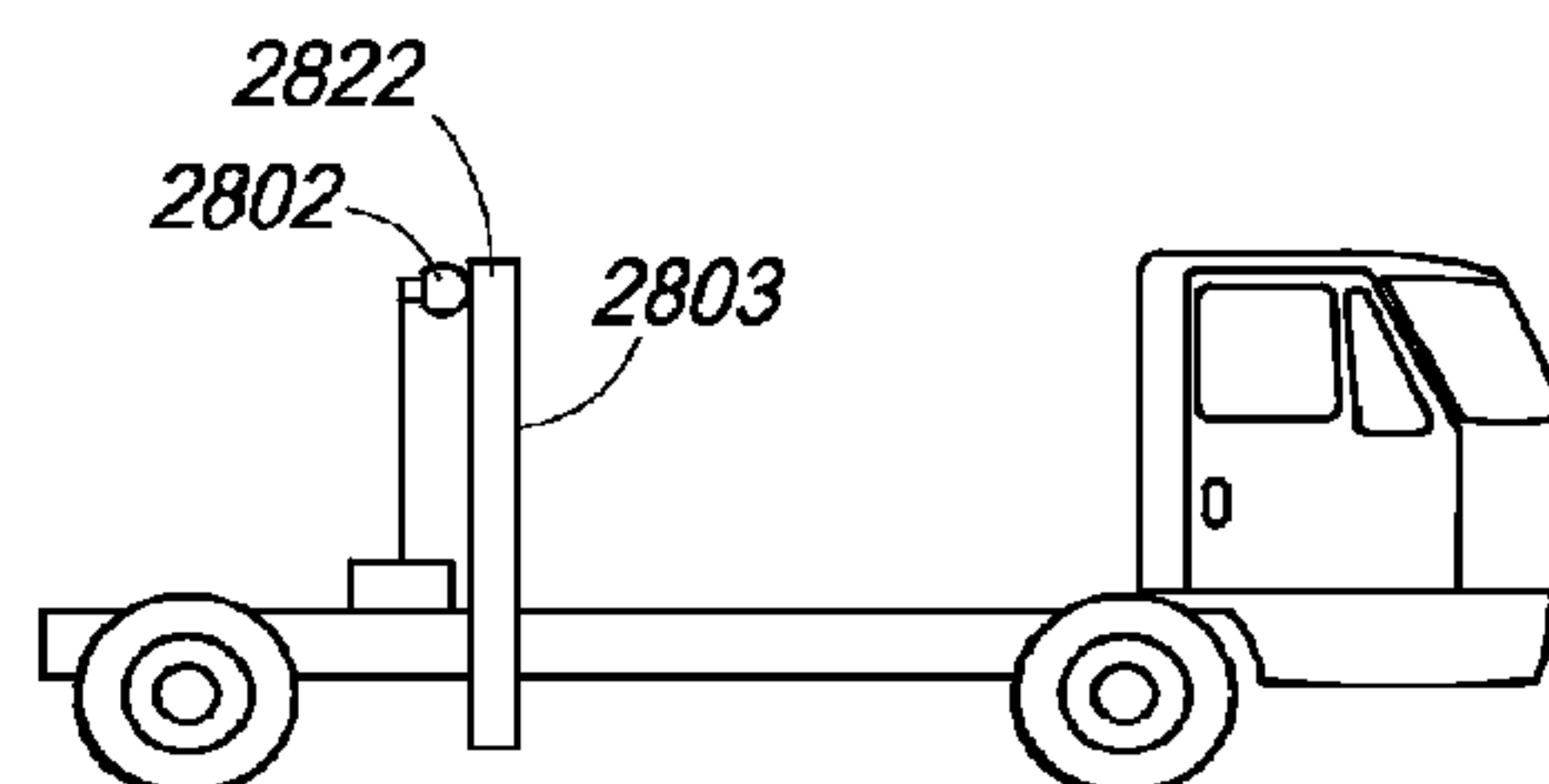


FIG. 28D



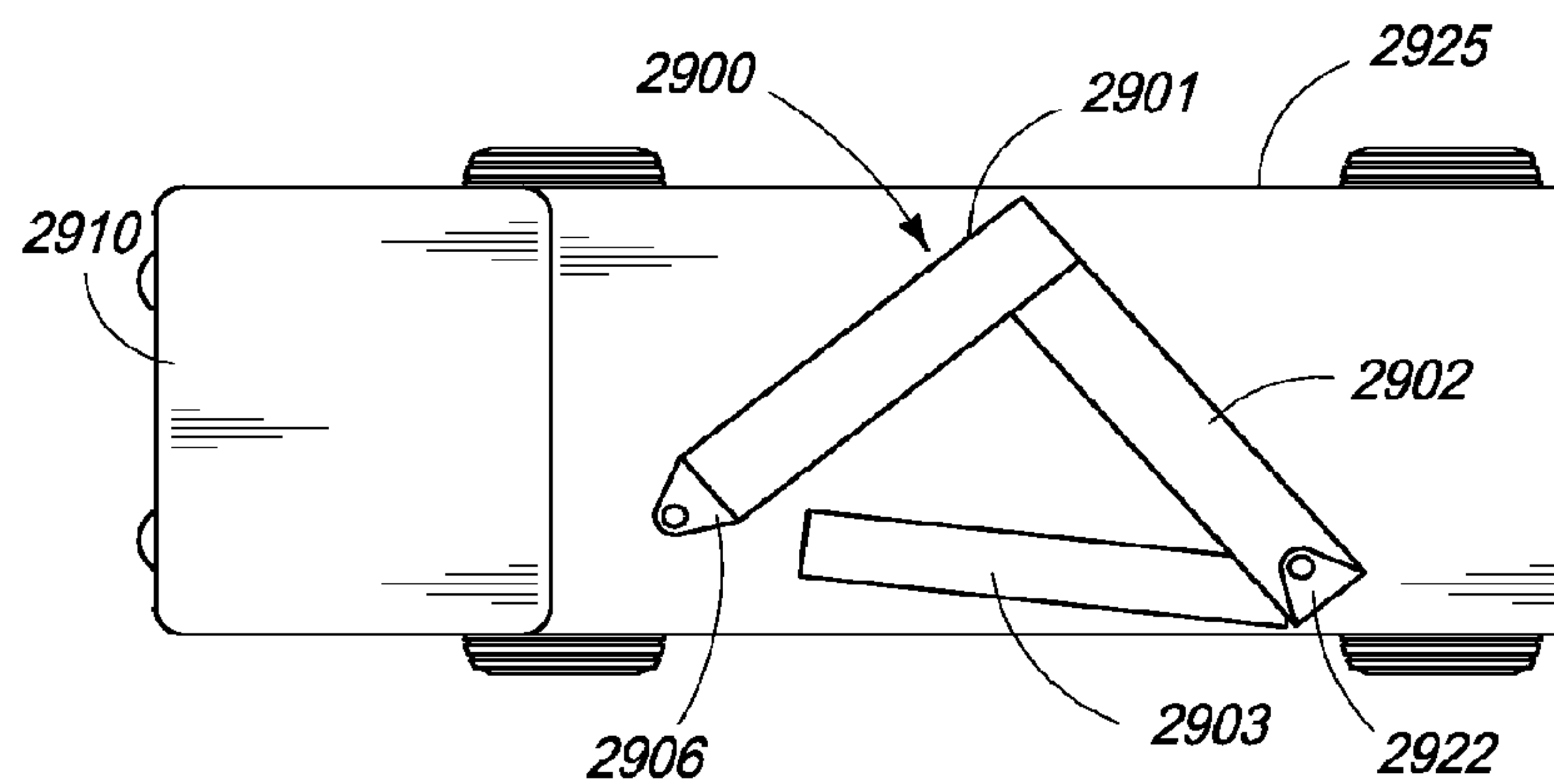


FIG. 29A

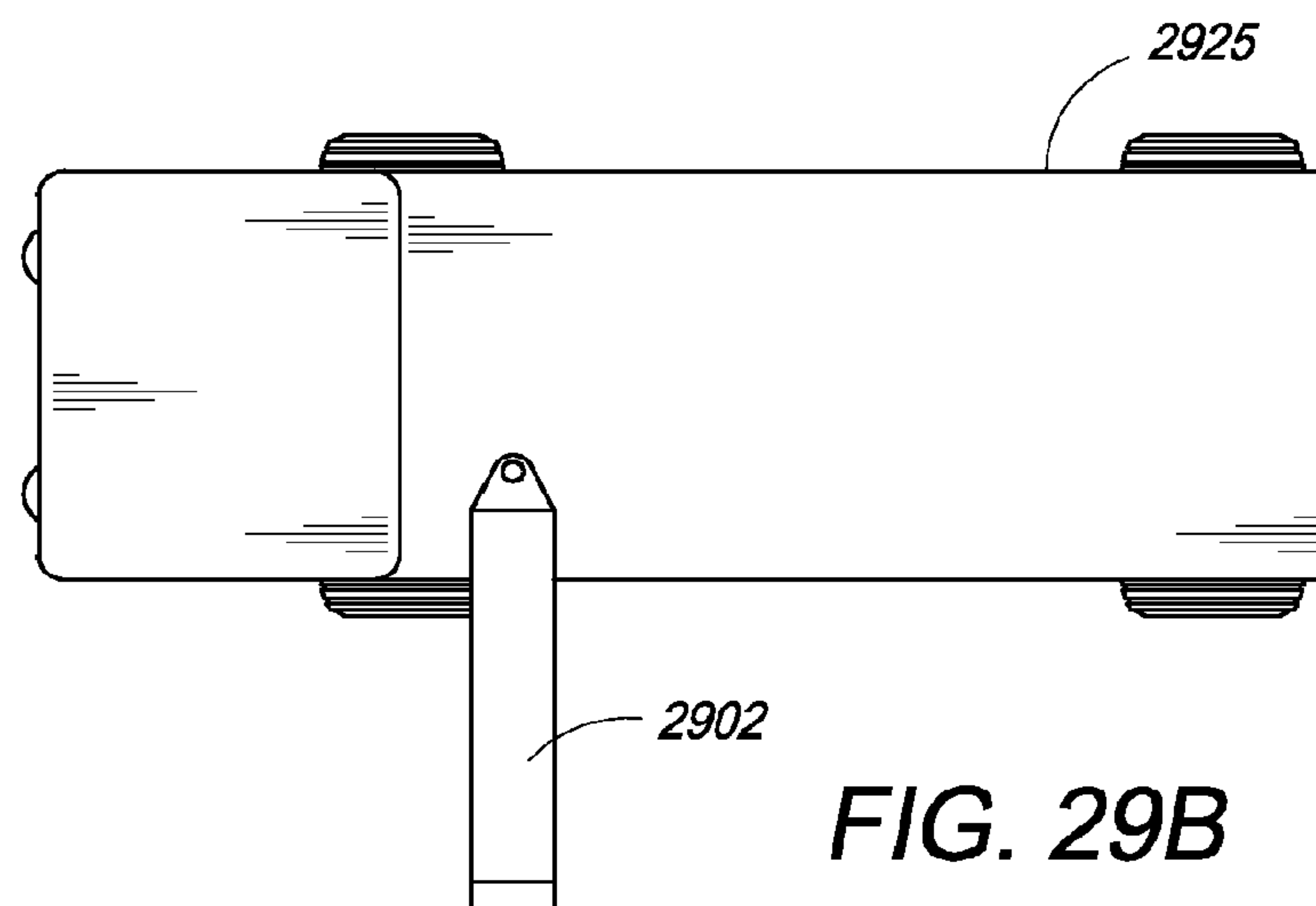


FIG. 29B

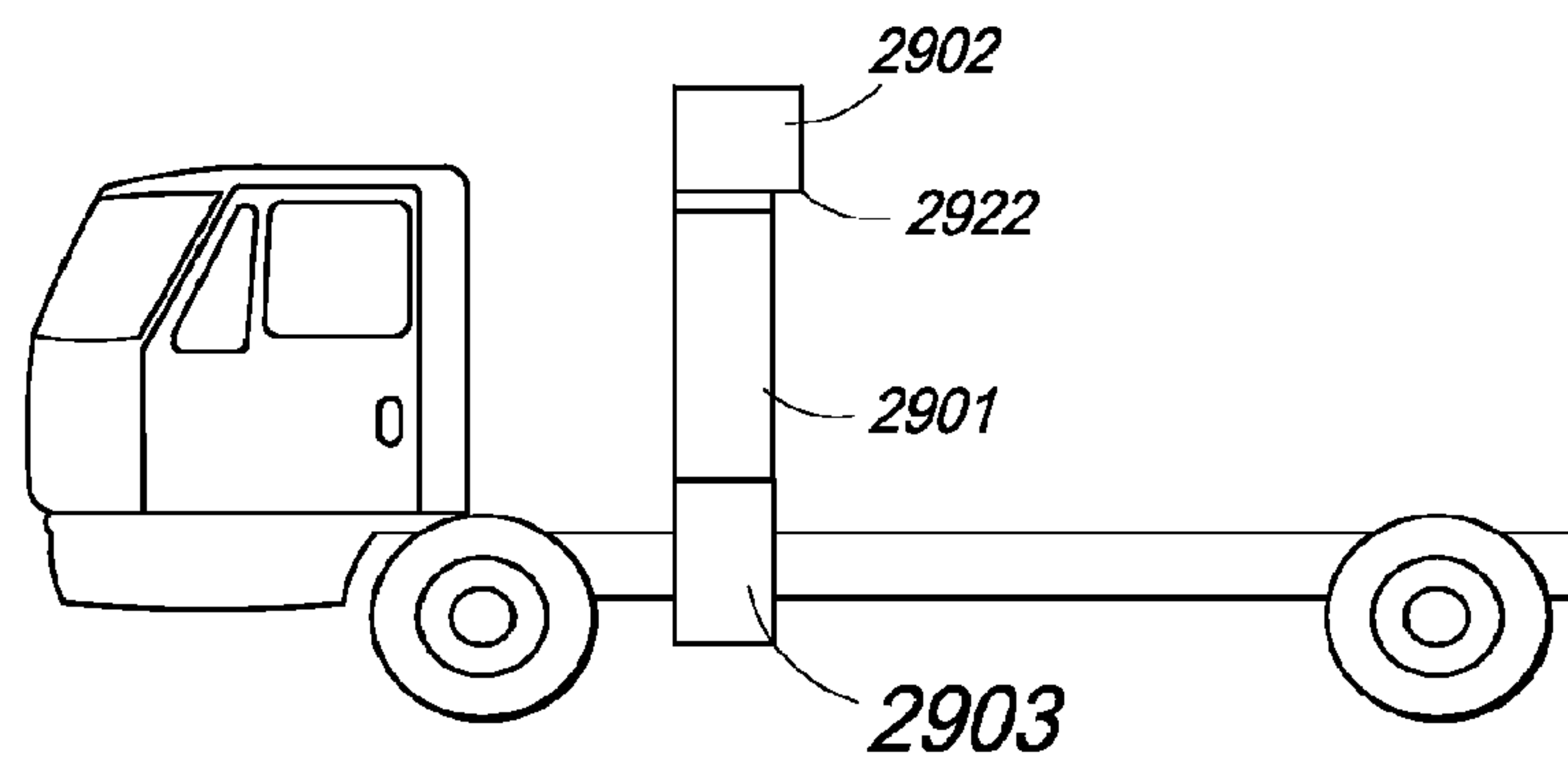


FIG. 29C

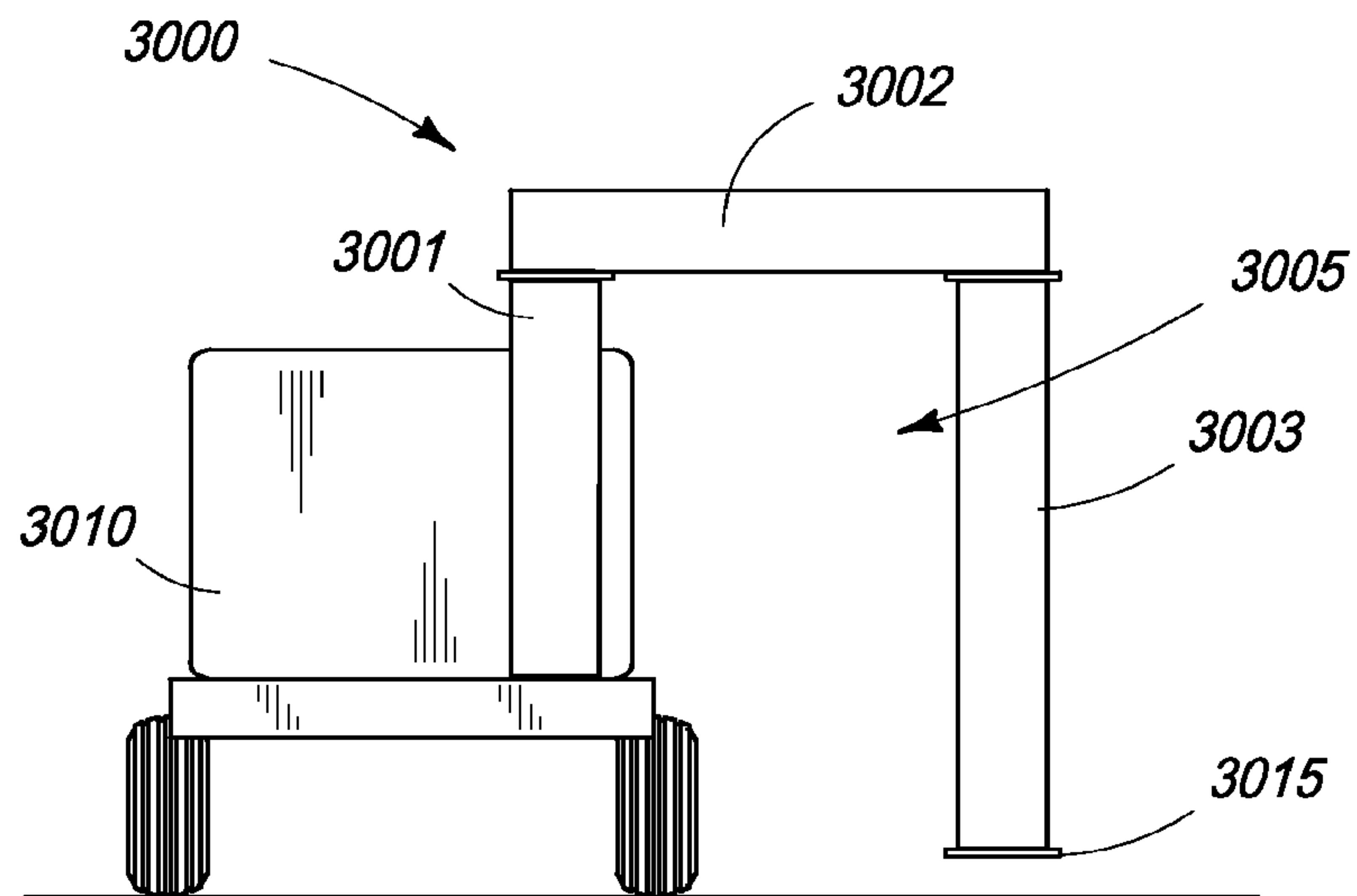


FIG. 30

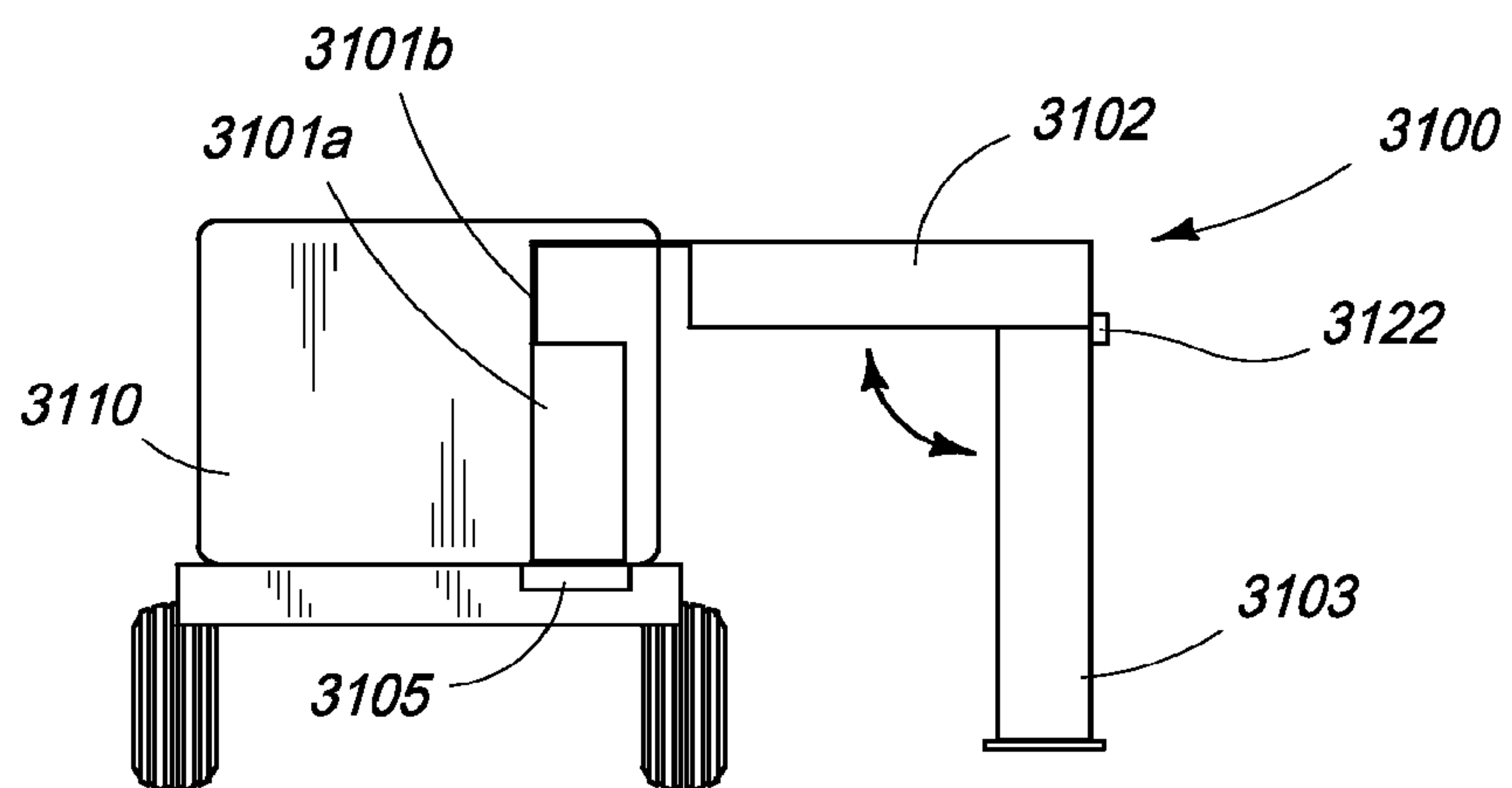
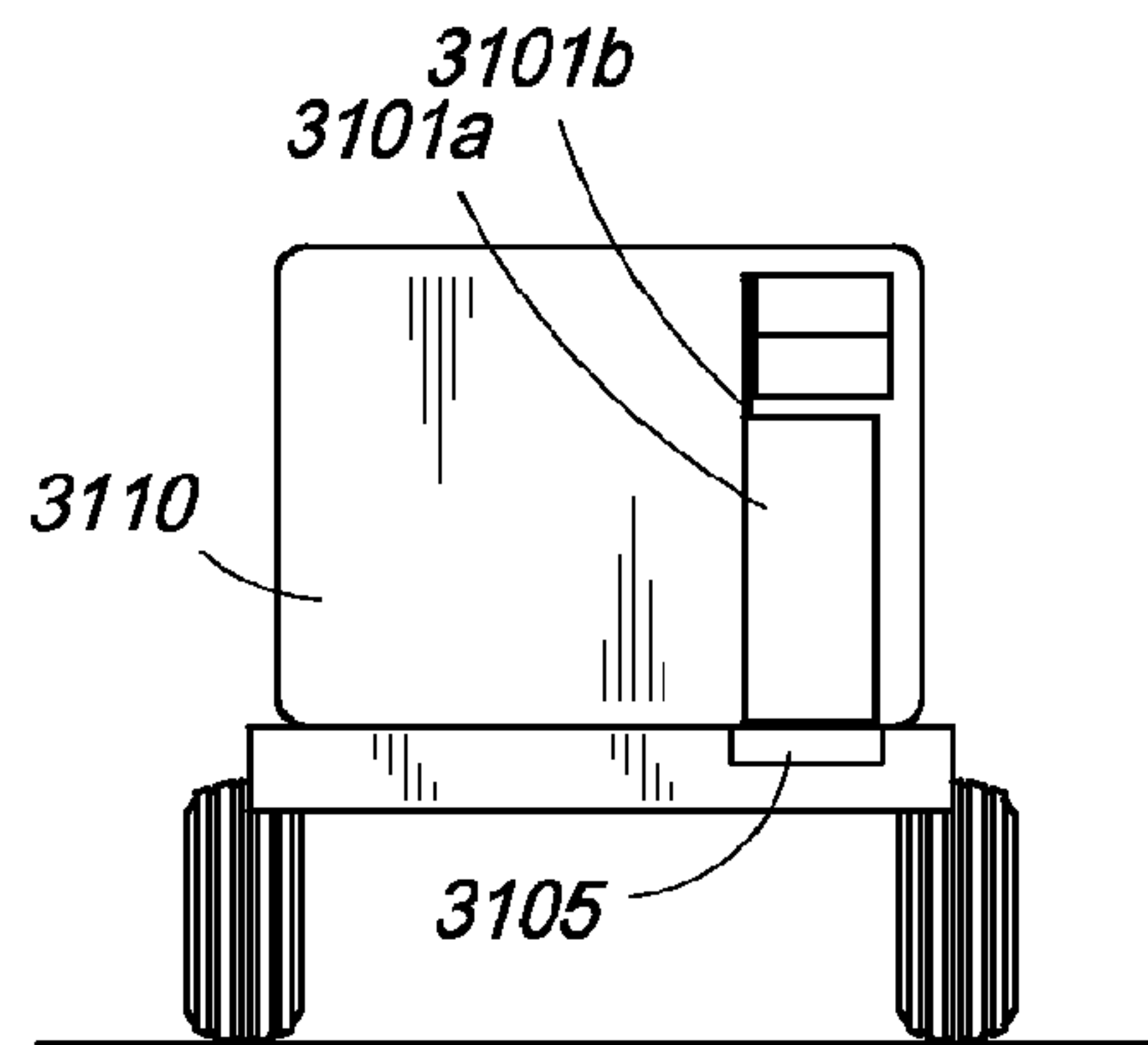
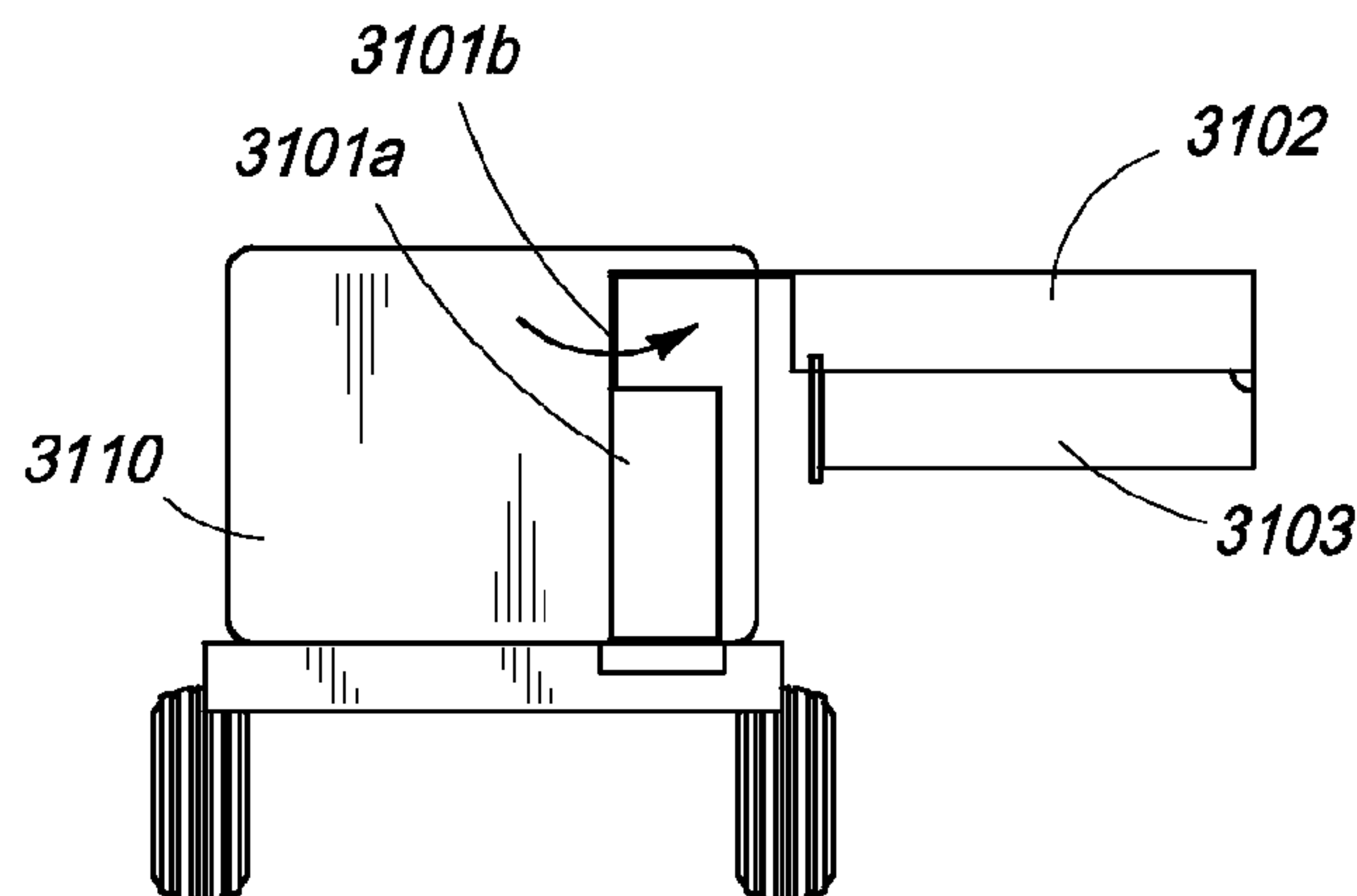


FIG. 31A

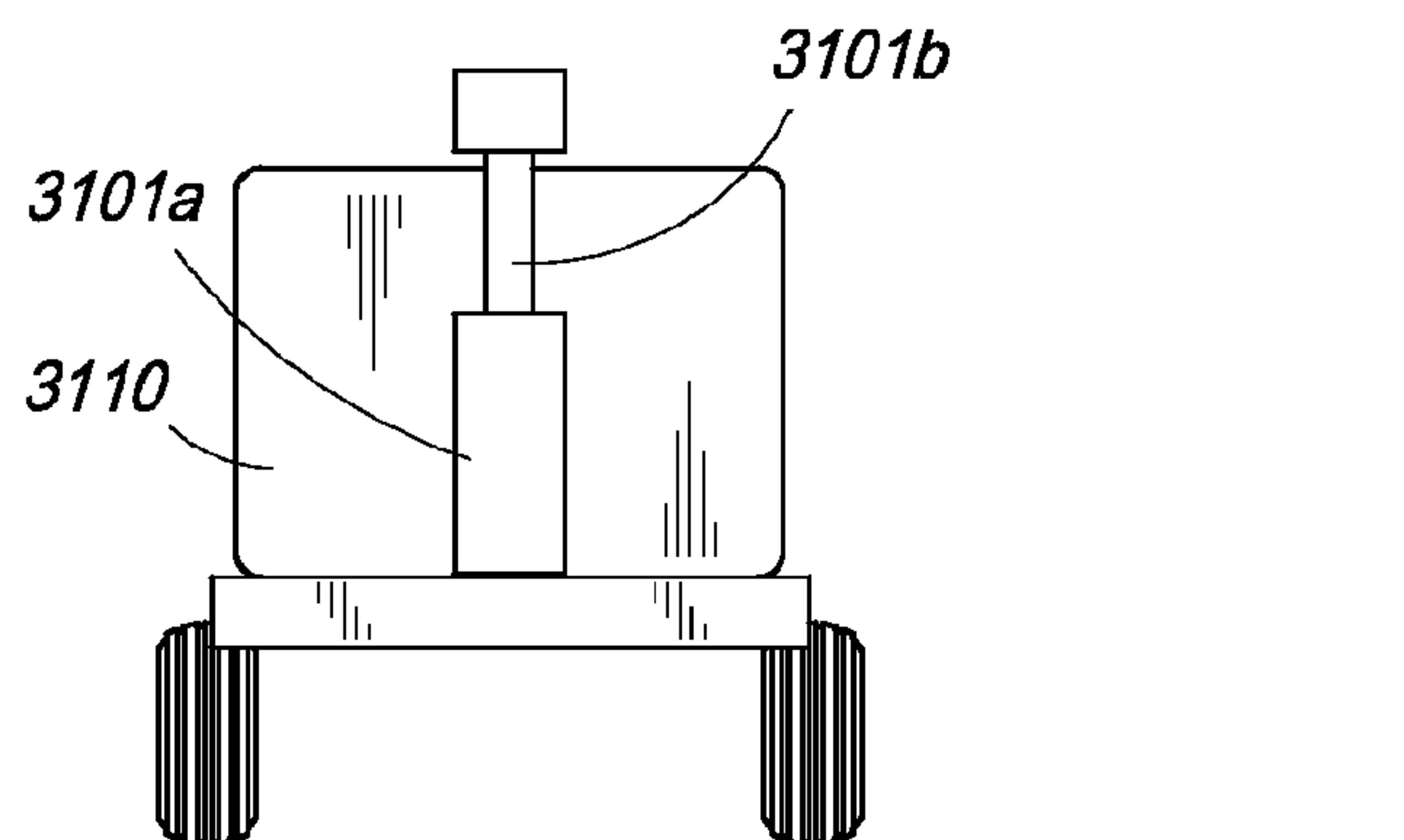
**FIG. 31B**



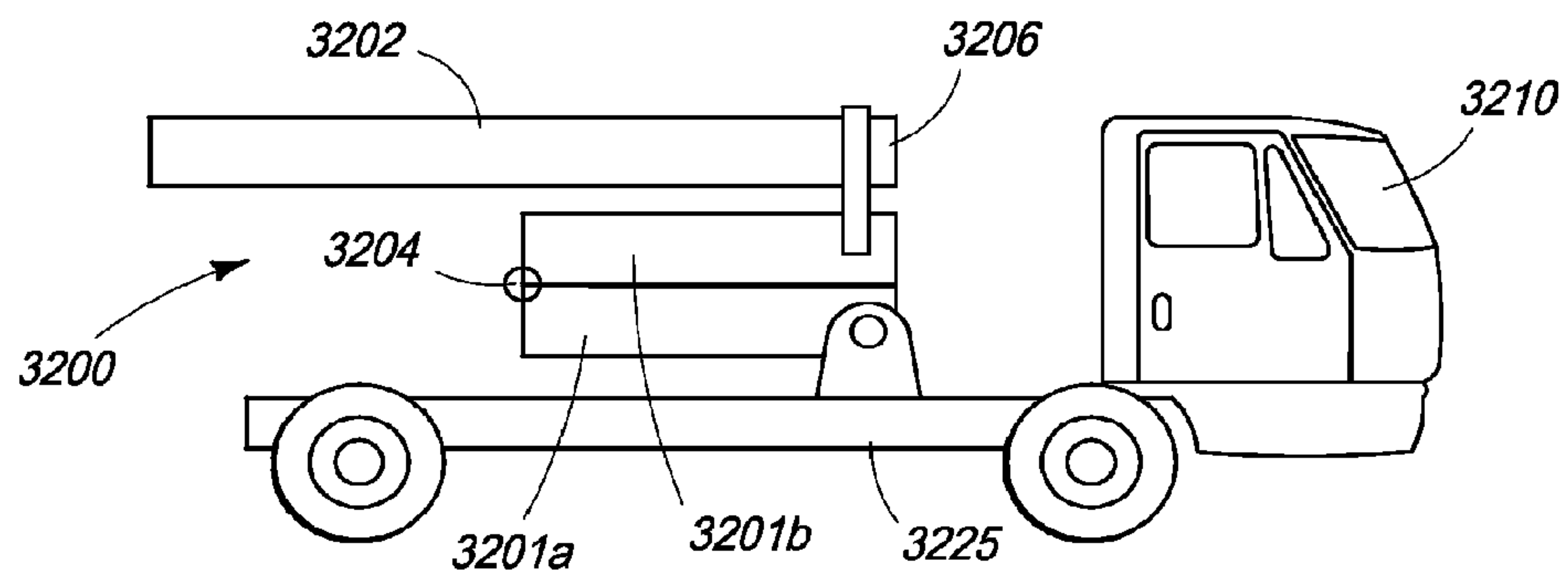
**FIG. 31C**



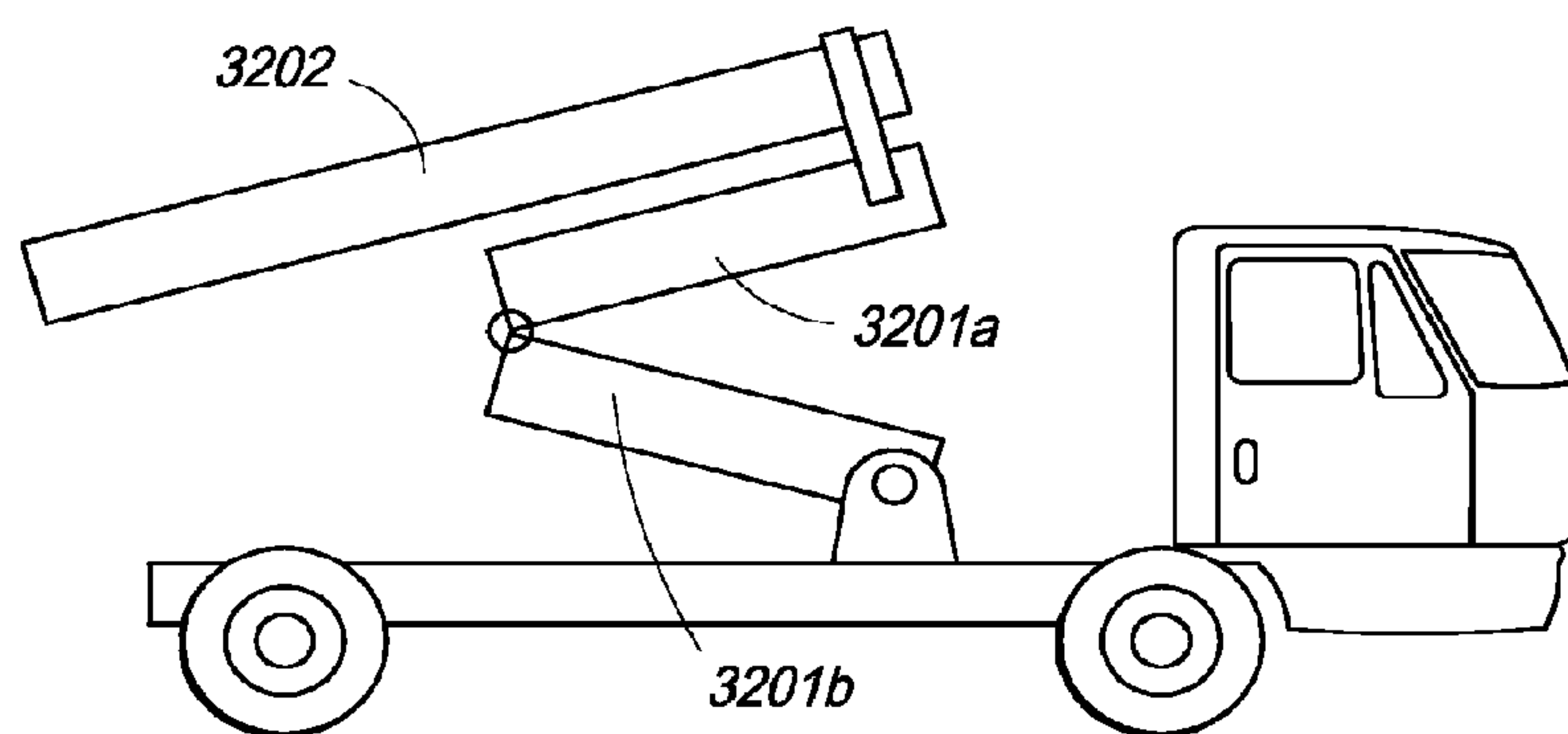
**FIG. 31D**



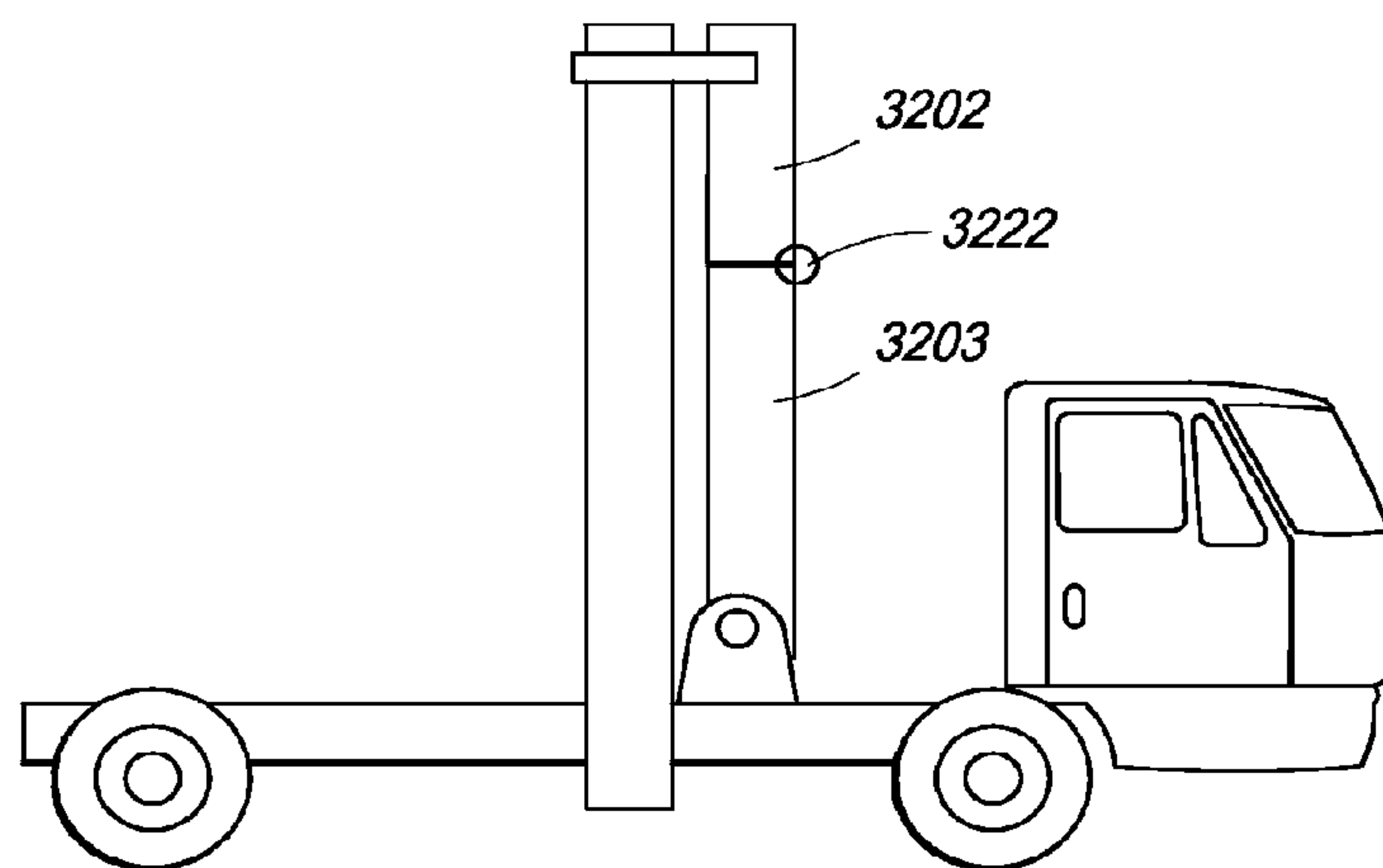




**FIG. 32A**



**FIG. 32B**



**FIG. 32C**

**COMPACT MOBILE CARGO SCANNING  
SYSTEM****CROSS-REFERENCE**

The present application is a continuation of U.S. patent application Ser. No. 12/784,630, filed on May 21, 2010 (the “’630 Application”).

The ’630 Application relies on U.S. Provisional patent application Ser. No. 61/180,471, filed on May 22, 2009, for priority.

The ’630 Application is a continuation-in-part of U.S. patent application Ser. No. 12/339,591, entitled Rotatable Boom Cargo Scanning System, filed on Dec. 19, 2008, which is a continuation-in-part of U.S. patent application Ser. No. 11/948,814, entitled, “Single Boom Cargo Scanning System”, filed on Nov. 30, 2007, which is a continuation of U.S. Pat. No. 7,322,745, entitled, “Single Boom Cargo Scanning System”, filed on Aug. 9, 2004, which relies on, for priority, U.S. Provisional Patent Application No. 60/493,935, filed on Aug. 8, 2003 and is a continuation-in-part of U.S. patent application Ser. No. 10/201,543, entitled “Self-Contained Portable Inspection System and Method”, filed on Jul. 23, 2002 and now U.S. Pat. No. 6,843,599. The ’591 application further relies on U.S. Provisional Application No. 61/014,814, filed on Dec. 19, 2007, for priority. The ’591 application is also a continuation-in-part of U.S. patent application Ser. No. 12/051,910, entitled “Single Boom Cargo Scanning System”, and filed on Mar. 20, 2008, which is a continuation of U.S. Pat. No. 7,369,463, of the same title, filed on Jan. 12, 2007, which is a continuation-in-part of U.S. Pat. No. 7,322,745.

The ’630 Application is also a continuation-in-part of U.S. patent application Ser. No. 12/263,160, entitled “Cargo Scanning System”, and filed on Oct. 31, 2008, which further relies on U.S. Provisional Patent Application No. 60/984,786, filed on Nov. 2, 2007, for priority, and is a continuation-in-part of U.S. Pat. No. 7,322,745.

The ’630 Application is also a continuation-in-part of Ser. No. 12/349,534, which is a continuation of U.S. patent application Ser. No. 10/939,986, entitled “Self-Contained Mobile Inspection System”, and filed on Sep. 13, 2004, which is a continuation-in-part of Ser. No. 10/915,687 (issued as U.S. Pat. No. 7,322,745), which is a continuation-in-part of Ser. No. 10/201,543 (issued as U.S. Pat. No. 6,843,599) and further relies on U.S. Provisional Patent Application No. 60/502,498, filed on Sep. 12, 2003, for priority.

All of the above-listed patent applications are herein incorporated by reference.

**FIELD**

The present application relates generally to a self-contained mobile inspection system and method and, more specifically, to improved methods and systems for detecting materials concealed within a wide variety of receptacles and/or cargo containers. In particular, the present application relates to improved methods and systems for inspecting receptacles and/or cargo containers using a single boom which can be folded, such that the inspection system is light-weight and relatively compact in a stowed configuration and has a low height and center of gravity lending to greater maneuverability.

**BACKGROUND**

X-ray systems are used for medical, industrial and security inspection purposes because they can cost-effectively

generate images of internal spaces not visible to the human eye. Materials exposed to X-ray radiation absorb differing amounts of X-ray radiation and, therefore, attenuate an X-ray beam to varying degrees, resulting in a transmitted level of radiation that is characteristic of the material. The attenuated radiation can be used to generate a useful depiction of the contents of the irradiated object. A typical single energy X-ray configuration used in security inspection equipment may have a fan-shaped or scanning X-ray beam that is transmitted through the object inspected. The absorption of X-rays is measured by detectors after the beam has passed through the object and an image is produced of its contents and presented to an operator.

Trade fraud, smuggling and terrorism have increased the need for such non-intrusive inspection systems in applications ranging from curbside inspection of parked vehicles to scanning in congested or high-traffic ports because transportation systems, which efficiently provide for the movement of commodities across borders, also provide opportunities for the inclusion of contraband items such as weapons, explosives, illicit drugs and precious metals. The term port, while generally accepted as referring to a seaport, also applies to a land border crossing or any port of entry.

With an increase in global commerce, port authorities require additional sea berths and associated container storage space. Additional space requirements are typically met by the introduction of higher container stacks, an expansion of ports along the coastline or by moving inland. However, these scenarios are not typically feasible. Space is generally in substantial demand and short supply. Existing ports operate under a routine that is not easily modified without causing disruption to the entire infrastructure of the port. The introduction of new procedures or technologies often requires a substantial change in existing port operating procedures in order to contribute to the port’s throughput, efficiency and operability.

With limited space and a need to expand, finding suitable space to accommodate additional inspection facilities along the normal process route remains difficult. Additionally, selected locations are not necessarily permanent enough for port operators to commit to the long term installation of inspection equipment. Moreover, systems incorporating high-energy X-ray sources, or linear accelerators (LINAC), require either a major investment in shielding material (generally in the form of concrete formations or buildings) or the use of exclusion zones (dead space) around the building itself. In either case, the building footprint is significant depending upon the size of cargo containers to be inspected.

A mobile inspection system offers an appropriate solution to the need for flexible, enhanced inspection capabilities. Because the system is relocatable and investing in a permanent building in which to accommodate the equipment is obviated, site allocation becomes less of an issue and introducing such a system becomes less disruptive. Also, a mobile X-ray system provides operators, via higher throughput, with the ability to inspect a larger array of cargo, shipments, vehicles, and other containers.

Conventional relocatable inspection systems generally comprise at least two booms, wherein one boom will contain a plurality of detectors and the other boom will contain at least one X-ray source. The detectors and X-ray source work in unison to scan the cargo on the moving vehicle. In conventional single boom relocatable inspection systems, the X-ray source is located on a truck or flatbed and the detectors on a boom structure extending outward from the truck. These systems are characterized by moving-scan-



engine systems wherein the source-detector system moves with respect to a stationary object to be inspected. Also, the detectors and the source of radiation are either mounted on a moveable bed, boom or a vehicle such that they are integrally bound with the vehicle. This limits the flexibility of dismantling the entire system for optimum portability and adjustable deployment to accommodate a wide array of different sized cargo, shipments, vehicles, and other containers. As a result these systems can be complicated to deploy and pose several disadvantages and constraints.

For example, in a moving-scan-engine system the movement of the source and detector, relative to a stationary object, may cause lateral twist and lift and fall of the detector or source, due to movement of the scanner over uneven ground, inducing distortions in the scanned images and faster wear and tear of the scanner system. Systems where the weight of the detector or source is held on a boom require high structural strength for the boom in order to have the boom stable for imaging process, thereby adding more weight into the system. Such systems that require a detector-mounted boom to unfold during deployment may cause an unstable shift of the center of gravity of the system off the base, causing the system to tip over. Further, in the case of moving-scan-engine systems using a "swing arm" boom approach, the driver driving the scanner truck is unable to gauge the possibility of hitting the detector box, mounted on a boom, with a vehicle under inspection (VUI), as the detector box is on the other side of the VUI during scanning and not visible to the driver.

Additionally, with moving-scan-engine systems, the truck supporting the scanner system is always required to move the full weight of the scanner regardless of the size and load of the VUI, putting greater strain on the scanning system. Also disadvantageous in conventional systems is that they suffer from a lack of rigidity, are difficult to implement, and/or have smaller fields of vision.

Accordingly, there is need for improved inspection methods and systems built into a fully self-contained, over-the-road-legal vehicle that can be brought to a site and rapidly deployed for inspection. The improved method and system can, therefore, service multiple inspection sites and set up surprise inspections to thwart contraband traffickers who typically divert smuggling operations from border crossings that have tough interdiction measures to softer crossings with lesser inspection capabilities. Moreover, there is an additional need for methods and systems that require minimal footprint to perform inspection and that use a sufficient range of radiation energy spectrum to encompass safe and effective scanning of light commercial vehicles as well as substantially loaded 20-foot or 40-foot ISO cargo containers. It is important that such scanning is performed without comprising the integrity of the cargo and should ideally be readily deployable in a variety of environments ranging from airports to ports of entry where a single-sided inspection mode needs to be used due to congested environments. Similar needs are addressed in U.S. Pat. No. 6,543,599, entitled "Self-Contained Portable Inspection System and Method", which is herein incorporated by reference in its entirety.

Improved methods and systems are additionally needed to keep the relative position between the radiation source and detector fixed to avoid distortion in images caused by the movement of scanner and/or detectors over uneven ground or due to unstable structures. Moreover, there is a need for improved methods and systems that can provide comprehensive cargo scanning in portable and stationary settings. Specifically, methods and systems are needed in which a

single boom is employed for generating quality images for inspection. Further, the system should be mounted on a relocatable vehicle, capable of receiving and deploying the boom.

What is also needed is a single boom cargo scanning system that enables quick and easy deployment, rigidity and tight alignment of the radiation sources and detectors, and a narrow collimated radiation beam, thus allowing for a smaller exclusion zone. In addition, what is needed is an optimal scanning system design that allows for the radiation source to be closer to the Object under Inspection ("OUI"), thereby allowing for higher penetration capability and complete scanning of the target vehicle without corner cutoff. Similar needs are addressed in the U.S. Pat. No. 7,322,745, entitled "Single Boom Cargo Scanning System" which is herein incorporated by reference in its entirety.

Further, in the mobile cargo inspection systems known in the art, the boom structures are typically heavy, thereby causing the overall weight of the scanning system to be close to, or even over the allowable axle load limits. Further, the booms are bulky when stowed such that the vehicle is approximately 4 m high above road level. This makes a mobile scanning system not only difficult to manoeuvre but also restricts its movement in different territories due to the applicable road restrictions on carriage weight. Therefore, there is also a need for a scanning system that can be stowed in a relatively compact area so that it can be easily transported on road, as well as by air. In addition, there is also a need for a scanning system which is light weight, and has a low height and center of gravity in a stowed position, thereby allowing for road transport even in challenging, steep and hilly areas.

What is also needed is a scanning system that can be deployed from a stowed configuration to an operational configuration in operating areas having limited horizontal or vertical clearance.

## SUMMARY

The present application is a self-contained mobile inspection system and method for detecting materials concealed within a wide variety of receptacles and/or cargo containers. In particular, the present application is an improved method and system for inspecting receptacles and/or cargo containers using a single boom that can be folded and unfolded, such that the inspection system is relatively compact in a stowed configuration and has a low height lending to greater maneuverability. This, and other embodiments of the present invention, shall be described in greater depth in the drawings and detailed description provided below.

In one embodiment, the present specification discloses an inspection system comprising a vehicle having a first axle proximate to a front of said vehicle and one or more rear axles proximate to a back of said vehicle wherein a first area is bounded by the rear axle extending to the front of said vehicle and a second area is bounded by the rear axle extending to the back of said vehicle; a radiological source; and a boom rotatably attached to said vehicle wherein said boom comprises a first vertical section, a second vertical section and a horizontal section and wherein, when fully deployed, said boom defines an area having a height in a range of 2000 mm to 5300 mm and a width in a range of 2000 mm to 4000 mm, wherein said system weighs less than 20,000 kg and is capable of achieving radiological penetration of at least 30 mm of steel. Optionally, the minimum penetration can be 31 mm, 40 mm, 50 mm, 60 mm, 120 mm or some increment therein.



## 5

The radiological source is attached to said vehicle. The radiological source is attached to said vehicle but not attached to said boom. The radiological source is an X-ray source is at least one of a X-ray generator with 100 kVp to 500 kVp tube voltage and 0.1 mA to 20 mA tube current, a 0.8 MV to 2.5 MV linear accelerator source with a dose output rate of less than 0.1 Gy/min at 1 m, and a 2.5 MV to 6 MV linear accelerator source with a output dose rate in a range 0.1 Gy/min at 1 m to 10 Gy/min at 1 m. The vehicle has only one rear axle but may in some configurations have more than one. The boom has a weight and wherein said boom is positioned such that the weight acts substantially over the rear axle. The boom has a weight and wherein said boom is positioned such that the weight acts over the first area.

The boom has a lattice structure comprising a plurality of beam sections connected by a plurality of nodes wherein said structure defines an internal lattice area. The detector or sensor box is connected to an outside the internal lattice area. The detector is positioned within the internal lattice area. The vehicle comprises a plurality of targets wherein each of said targets is on a different part of said vehicle.

The inspection system further comprises a camera in data communication with a controller wherein said camera captures a movement of said targets and wherein said controller determines what portion of said vehicle has moved based on the movement of said target. The controller determines a speed of said vehicle based on said movement of said targets. The controller modulates a frequency at which X-ray data is collected based upon said speed.

In another embodiment, the inspection system comprises a vehicle having a first axle proximate to a front of said vehicle and one or more rear axles proximate to a back of said vehicle wherein a first area is bounded by the rear axle extending to the front of said vehicle and a second area is bounded by the rear axle extending to the back of said vehicle; a radiological source; a boom, having a weight, rotatably attached to said vehicle wherein said boom comprises a first vertical section, a second vertical section and a horizontal section and wherein said weight is positioned to substantially act over said first area and not said second area, wherein said system weighs 15,000 kg or less.

The system is capable of achieving radiological penetration of at least 30 mm of steel. When fully deployed, the boom defines an area having a height in a range of 2000 mm to 5300 mm and a width in a range of 2000 mm to 4000 mm. The radiological source is attached to said vehicle and capable of being moved from a first position to a second position, wherein each of said first and second positions are proximate to said vehicle. The radiological source is an X-ray source is at least one of a X-ray generator with 100 kVp to 500 kVp tube voltage and 0.1 mA to 20 mA tube current, a 0.8 MV to 2.5 MV linear accelerator source with a dose output rate of less than 0.1 Gy/min at 1 m, and a 2.5 MV to 6 MV linear accelerator source with a output dose rate in a range 0.1 Gy/min at 1 m to 10 Gy/min at 1 m. The boom has a lattice structure comprising a plurality of beam sections connected by a plurality of nodes wherein said structure defines an internal lattice area.

## BRIEF DESCRIPTION OF THE DRAWINGS

These and other features and advantages of the present invention will be appreciated, as they become better understood by reference to the following detailed description when considered in connection with the accompanying drawings, wherein:

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FIG. 1 illustrates the mobile inspection system according to one embodiment of the present invention in transportation mode with the boom stowed on the vehicle;

FIG. 2a shows three sections of a boom when fully deployed, according to one embodiment of the present invention;

FIG. 2b shows a side view of one embodiment of a mobile inspection vehicle with the boom in a stowed or folded condition;

FIG. 3a depicts the functioning of a vertical support section of a boom according to one embodiment of the present invention;

FIG. 3b depicts the functioning of a vertical support section of a boom according to another embodiment of the present invention;

FIG. 4a depicts the mounting of a vertical support section of a boom on one embodiment of the mobile inspection vehicle in a deployed condition;

FIG. 4b depicts the mounting of a vertical support section of a boom on one embodiment of the mobile inspection vehicle in a stowed condition;

FIG. 5a illustrates a first configuration of an exemplary low mass lattice structure which acts to reduce the weight of the boom, as used in one embodiment of the present invention;

FIG. 5b illustrates a second configuration of an exemplary low mass lattice structure which acts to reduce the weight of the boom, as used in one embodiment of the present invention;

FIG. 5c illustrates a third configuration of an exemplary low mass lattice structure which acts to reduce the weight of the boom, as used in one embodiment of the present invention;

FIG. 5d illustrates a fourth configuration of an exemplary low mass lattice structure which acts to reduce the weight of the boom, as used in one embodiment of the present invention;

FIG. 6 shows an exemplary design for a combined boom and detector box;

FIG. 7 presents an exemplary mechanism for folding and unfolding the horizontal boom out from the vertical support;

FIG. 8a shows an exemplary locking mechanism which is used when the boom is unfolded;

FIG. 8b shows an exemplary locking mechanism which is used when the boom is unfolded;

FIG. 9 shows an additional boom support structure which can optionally be used to help the boom deployment;

FIG. 10 shows another boom support structure;

FIG. 11a illustrates a first space saving folding arrangement between a horizontal boom and vertical boom, according to one embodiment of the present invention;

FIG. 11b illustrates a second space saving folding arrangement between the horizontal boom and vertical boom, according to one embodiment of the present invention;

FIG. 12a illustrates an exemplary boom configuration which limits the rotation of the X-ray source;

FIG. 12b illustrates another exemplary boom configuration which limits the rotation of the X-ray source;

FIG. 13a illustrates an exemplary mechanism for minimizing the swinging movement of the X-ray source during boom deployment;

FIG. 13b illustrates another exemplary mechanism for minimizing the swinging movement of the X-ray source during boom deployment;

FIG. 14a illustrates a configuration for mounting the X-ray source;



FIG. 14b illustrates an alternative configuration for mounting the X-ray source;

FIG. 15a illustrates an exemplary locking mechanism for the boom and the X-ray source;

FIG. 15b illustrates another exemplary locking mechanism for the boom and the X-ray source;

FIG. 16a illustrates an alignment of x-ray beam with the detectors;

FIG. 16b illustrates another alignment of x-ray beam with the detectors;

FIG. 17a illustrates an exemplary configuration in which the scanning system of the present invention may be deployed;

FIG. 17b illustrates another exemplary configuration in which the scanning system of the present invention may be deployed;

FIG. 17c illustrates another exemplary configuration in which the scanning system of the present invention may be deployed;

FIG. 18 illustrates an exemplary sensor configuration for control of the X-ray system when operating in drive through mode according to one embodiment of the present invention;

FIG. 19 shows an exemplary location of three vision targets, with respect to a vehicle being inspected;

FIG. 20 shows the output from a scanning laser sensor as a function of time;

FIG. 21 illustrates an embodiment where a process logic controller (PLC) is used to control the traffic control and X-ray control mechanism in the scanning system of the present invention;

FIG. 22 illustrates an exemplary detector configuration according to one embodiment of the present invention;

FIG. 23 illustrates another exemplary configuration wherein the detectors are stacked, according to one embodiment of the present invention;

FIG. 24 shows a side elevation view of the mobile inspection vehicle of the present invention comprising an inspection pod in accordance with one embodiment;

FIG. 25a shows top view of the mobile inspection vehicle of the present invention comprising an inspection pod in retractable state for travel;

FIG. 25b shows top view of the mobile inspection vehicle of the present invention comprising the inspection pod in extendable state during deployment/operation;

FIG. 26a shows a side elevation view of the mobile inspection vehicle of the present invention comprising inspection pod accessible to an inspector that can be seated above front wheel level;

FIG. 26b shows top view of the mobile inspection vehicle of the present invention comprising inspection pod accessible to an inspector that can be seated above front wheel level;

FIG. 27 shows top view of the mobile inspection vehicle of the present invention that has a rotatable bed;

FIG. 28a shows an embodiment of boom structure/configuration to move pivot point of the boom forward of the rear wheels of the mobile inspection vehicle;

FIG. 28b shows vertical support of the boom of FIG. 28a extended in fully vertical orientation along with the horizontal boom being perpendicular to the vertical support;

FIG. 28c shows the horizontal boom of the boom of FIG. 28a being rotated 90 degrees to be perpendicular to the long side of the mobile vehicle;

FIG. 28d shows the vertical boom of the boom of FIG. 28a being lowered down to complete full deployment;

FIG. 29a shows an embodiment of structure/configuration of boom, when in stowed condition, in accordance with another aspect of the present invention;

FIG. 29b shows vertical support of the boom of FIG. 29a in vertical position along with causing the horizontal boom to extend outwards in a direction perpendicular to the long edge of the vehicle;

FIG. 29c shows the vertical boom of the boom of FIG. 29a being lowered down to complete full deployment;

FIG. 30 shows an embodiment of the boom structure/configuration of the present invention where the boom is deployed using an onboard crane;

FIG. 31a shows an embodiment of the boom structure/configuration of the present invention comprising four components;

FIG. 31b shows the two vertical support sections of the boom of FIG. 31a unfolded into an end-to-end configuration;

FIG. 31c shows the horizontal boom of the boom of FIG. 31a being extended perpendicular to the long edge of the vehicle through 90 degrees rotatory motion of the rotating platform;

FIG. 31d shows an embodiment of the boom of FIG. 31a where the upper vertical support is telescopically retractable/extendable to/from the lower vertical support;

FIG. 32a shows an embodiment of the boom structure/configuration of the present invention comprising four components;

FIG. 32b shows the two vertical support sections of the boom of FIG. 32a extended from horizontal (stowed position) to vertical position; and

FIG. 32c shows the folded horizontal and vertical boom sections of the boom of FIG. 32a being moved from horizontal to vertical orientation.

## DETAILED DESCRIPTION OF THE INVENTION

The present invention is directed towards a portable inspection system for generating an image representation of target objects using a radiation source, comprising a mobile vehicle; a detector array physically attached to a single, movable boom having a proximal end and a distal end and at least one source of radiation wherein the radiation source is fixedly attached to the proximal end of the boom and adjustable to a desired scanning height. The image is generated by introducing target objects between the radiation source and the detector array, thereby exposing objects to radiation and subsequently detecting the radiation. The boom can be unfolded from a first stowed configuration to a second deployed and operational configuration.

The system of the present invention is advantageous in that it provides a highly compact stowed configuration and has a low height, such that the highest part of the boom does not exceed the height of the drive cab, among other benefits. The inspection system of present invention provides a sturdy deployed configuration with the radiation source and detectors readily aligned and a selectable scan angle position, and can be converted from a stowed configuration to a deployed and operational configuration in areas having limited horizontal and vertical clearance. Further, the inspection system of the present invention is capable of using either a small or a large LINAC, at both high as well as low energies. It may also be used with conventional sources of radiation.

In one embodiment, the present invention is directed toward a new boom configuration for the mobile inspection system, which addresses many of the issues that affect boom



designs known in the art. The boom design of the present invention provides for a light weight scanning system, and the boom can also be stowed in a compact manner. This makes the resulting mobile inspection vehicle highly maneuverable. Further, owing to its low axle weights, the mobile inspection vehicle is not subject to any road restrictions and can freely move across all territories in the world.

It should be appreciated that the various mechanical and/or hydraulic movements described herein can occur by manual manipulation of the physical structures or hydraulic components or, as is preferred, by signals transmitted by a controller. In one embodiment, a computing device with a graphical user interface is deployed to receive user commands, transmit user commands to controllers that are in data communication with the various boom, bracket, winch, and/or hydraulic components described herein, and receive data from the controllers indicative of the state of each of the various boom, bracket, winch, and/or hydraulic components described herein. Any computing device and controller system can be used, including laptops, mobile devices, desktop components, and X-ray control centers, and any form of data communication can be used, including wired or wireless communications.

FIG. 1 illustrates the mobile inspection vehicle **101** of the present invention in its normal transportation mode wherein the boom **102** is stowed on the vehicle. In the embodiment of FIG. 1, the inspection vehicle **101** is a truck and the boom **102** in the stowed condition lies substantially parallel to the bed **103** of the truck **101**. The cab **104** of the truck is the highest part of the vehicle, and is typically at an approximate height of 2.6 m from the ground to the highest point. The boom **102** of the present invention is designed such that it is capable of being folded to fit into a space lower than the height of the cab **104**, that is, the highest part of the boom **102** does not exceed the height of the drive cab **104**.

Persons of ordinary skill in the art should note that the maximum standard overall vehicle dimension of a truck is typically 12 m (L)×2.5 m (W)×4 m (H). However, the overall footprint of the mobile inspection vehicle **101**, of the present invention, with the compact boom **102** when stowed thereon is 11 m (L)×2.5 m (W)×4 m (H) in accordance with one embodiment. In an alternate embodiment the footprint of the vehicle **101** is 8 m (L)×2.5 m (W)×2.6 m (H). The compact design of the vehicle **101** with the stowed boom **102**, of the present invention, offers a substantially small overall size for the inspection vehicle when used with full size inspection tunnel of 4.6 m (H)×3.5 m (W) typically.

FIG. 2a shows the boom when fully deployed. The boom comprises three sections: vertical support **201a** (connected to an X-ray source **201d**), horizontal boom **202a**, and vertical boom **203a**.

FIG. 2b shows a side view of the mobile inspection vehicle **200** when it is in use, so that the boom is in deployed condition. As mentioned, the boom design of the present invention comprises three components—vertical support **201b** (connected to a X-ray source **203d**), horizontal boom **202b** and vertical boom **203b**, which in the stowed condition can be folded parallel to each other in a manner that the total space occupied by the boom is minimized. Since the boom is collapsible to a small volume (of 1.5 m (H)×1.2 m (W)×5.0 m (L) in one embodiment) when stowed, the overall height of the inspection vehicle is substantially reduced when configured for transport. In one embodiment, the overall height of the inspection vehicle is about 2.6 m during transport when compared to a height of 4.0 m for conventional vehicles. This further allows transport of the

vehicle by aircraft (such as a C-130 military transporter) for rapid deployment where appropriate.

Referring now to FIGS. 2a and 2b together, the vertical support sections **201a**, **201b** are manufactured using a strong material, which in one embodiment is steel. One of ordinary skill in the art would appreciate that other engineering materials such as carbon fiber composite, aluminum or metal-composite structures may also be used.

An advantage of the boom structure/design of the present invention is that the overall weight of the mobile inspection vehicle **200** is substantially reduced. For example, a full size 4.6 m (H)×3.5 m (W) scanning-tunnel vehicle has a total weight of less than 25,000 kg, preferably less than 20,000 kg, and more preferably less than 15,000 kg. Persons of ordinary skill in the art would appreciate that this weight of the mobile inspection vehicle of the present invention is substantially less when compared to a standard prior art truck that would typically weigh in excess of 25,000 kg. The lighter vehicle **200** of the present invention advantageously allows the vehicle/truck to operate with a single front axle and a single rear axle. Conventional designs require at least 2 and often 3 rear axles to meet road regulations in certain countries/regions due to comparatively high weights of prior art vehicles. This system also can achieve a penetration of steel of more than 90 mm, including 100 mm, 120 mm, 150 mm, 180 mm and any increment therein.

Due to light weight, reduced number of axles and smaller overall size, the vehicle **200** of the present invention is much more capable of operating in rugged terrain than conventional prior art designs.

The functioning of the vertical support is further detailed in FIGS. 3a and 3b. As shown in FIG. 3a, the vertical support **301a** is in a near horizontal position when not deployed. In one embodiment, the vertical support **301a** is at an angle in the range of 5 to 20 degrees to the horizontal, when in stowed away position. A fixed point **302a** is provided, around which the vertical support is enabled to pivot around. Thus for deployment, the position of the vertical support **301a** changes from near horizontal in FIG. 3a to vertical as depicted by **301b** in FIG. 3b.

The rotating action of the vertical support over the fixed point **302a**, **302b** can be driven by a number of mechanisms including, but not restricted to, one or more hydraulic rams, one or more electric motors and associated gearboxes or a pulley drive system. It is preferable to be able to lock the vertical support in place once it has been rotated to the operating or stowed condition. This can be achieved by using, by way of example, conical pins (not shown) that pass through a support structure on the truck platform and into suitably located holes in the vertical support. One of ordinary skill in the art would appreciate that other locking mechanisms known in the art can also be used in place of or in addition to the example given.

In one embodiment, the X-ray source of the scanning system is mounted rigidly to the base of the vertical support such that it swings close to the road surface once the vertical support is deployed. This is illustrated in FIG. 4a. Referring to FIG. 4a, the X-ray source **401a** is mounted in an offset position on the vertical support **402a**, such that the focal point **403a** of the X-ray source is in line with the X-ray detectors (not shown) that, in one embodiment, are mounted into the horizontal and vertical boom structures (not shown in FIG. 4a). In this embodiment, the radiation source is positioned on the vertical support, which is a portion of the boom proximate to the truck, thereby offering a better alignment between the source and the detectors. In conventional inspection systems the radiation source is placed



either on the truck itself, such as on the side or back of the truck, or on the distal end of the boom.

FIG. 4*b* shows the X-ray source 401*b* along with the vertical support 402*b* in the stowed position. It may be noted from FIG. 4*b* that substantially all of the weight of the vertical support 402*b* acts over, is in alignment with, or is otherwise positioned over the rear axle 404*b* of the truck. Therefore, the vertical support 402*b* is designed to minimize the overall weight of the mobile inspection vehicle in order to ensure that the rear axle loading is kept to a reasonable level.

FIG. 28*a* shows a boom structure/configuration to move pivot point 2806 of the boom 2800 forward of the rear wheels 2804 of the mobile inspection vehicle 2810 in accordance with one embodiment of the present invention. In this embodiment, the boom 2800 comprises three components—vertical support 2801, horizontal boom 2802 and vertical boom 2803. The vertical support 2801 is mounted at its lower end to a rotating platform 2805 which is securely fixed onto the inspection vehicle chassis. An actuator is used to move the vertical support 2801 from a substantially horizontal (when stowed) to a vertical orientation about a hinge or pivot point 2806 which is attached to the rotating platform 2805. The horizontal boom 2802 is attached at one of its ends to the top of the vertical support 2801 using a pivot pin 2807. During deployment, as an actuator extends the vertical support 2801, a mechanical linkage maintains the same angle 2820 between the horizontal boom 2802 and vertical support 2801 as the angle 2815 between the vertical support 2801 and the rotating platform 2805. As a result, one actuator is used to extend two booms in one action or substantially concurrently.

FIG. 28*b* shows the vertical support 2801 extended in fully vertical orientation with reference to the rotating platform 2805 along with the horizontal boom 2802 also being perpendicular to the vertical support 2801. Once the vertical support 2801 and horizontal boom 2802 are deployed, as shown in FIG. 28*b*, another actuator is used to rotate the rotating platform 2805 through 90 degrees so that the horizontal boom 2802 is perpendicular to the long side 2825 of the vehicle and extending outwards as shown in FIG. 28*c*. Finally, as shown in FIG. 28*d*, a third actuator is used to lower the vertical boom 2803 from a hinge point 2822 at the distal end of the horizontal boom 2802.

Persons of ordinary skill in the art should note that the boom configuration of FIGS. 28*a* through 28*d* with the boom pivot point 2806 being advantageously forward of the rear wheels 2804 reduces rear axle load substantially, thereby making the inspection vehicle 2810 easier to drive and more compact while providing greater protection for the X-ray source (that is mounted at the lower end/base of the vertical support). Lower weight also contributes to faster deployment of the system. In one embodiment, the rear axle loading is below 9 tons for a full laden vehicle.

FIG. 29*a* shows a top perspective of another embodiment of structure/configuration of boom 2900 when in stowed condition, in accordance with another aspect of the present invention. In this embodiment, the boom 2900 comprises two components—a first component comprising vertical support 2901 and horizontal boom 2902 and a second component comprising vertical boom 2903. The vertical support 2901 and horizontal boom 2902 are fixed at 90 degrees to each other to form one rigid assembly of the first component. The vertical boom 2903 is hinged from the distal end 2922 of the horizontal boom 2902.

The base of vertical support 2901 is hinged about a point 2906 which, in one embodiment, is at 45 degrees to the long

edge 2925 of the side of the mobile vehicle 2910. Hinging the first component assembly (of the vertical support 2901 and horizontal boom 2902 at a fixed 90 degrees angle to each other) about the point 2906 causes the vertical support 2901 to become vertical (during deployment), from its starting horizontal aspect (when stowed), while simultaneously causing the horizontal boom 2902 to extend outwards in a direction perpendicular to the long edge 2925 of the vehicle, as shown in FIG. 29*b*. Again, as illustrated in FIG. 29*c*, once the vertical support 2901 and horizontal boom 2902 are in position, the vertical boom 2903 is lowered (using an actuator) about a hinge point at the distal end 2922 of the horizontal boom 2902 for complete deployment.

In one embodiment, it is preferred to have the vertical support 2901 comprising a first portion which is fixed rigidly to the chassis of the vehicle 2910 and a second part which is hinged from the top of the first part. In this case, the hinge will advantageously extend over an angle of greater than 90 degrees so that the intersection between the vertical support upper part and the horizontal boom 2902 lies nearer to the vehicle chassis.

FIG. 30 shows yet another embodiment of structure/configuration of boom 3000 in accordance with an aspect of the present invention. In this embodiment, the boom 3000 comprises three components—vertical support 3001, horizontal boom 3002 and vertical boom 3003. The boom 3000 comprising these three components is stowed/loaded onto the back of the mobile vehicle 3010. Vehicle 3010 is provided with a manually operated crane (not shown), such as a Hiab lift, which is used to lift the boom sections into place to form a static archway 3005 that is used in drive-through portal mode. During deployment, in one embodiment, an operator lifts the vertical boom 3003 into position. Next, the operator lifts the vertical support 3001 into position. Finally, the operator lifts the horizontal boom 3002 into position such that it forms a ‘bridge’ between the vertical support 3001 and vertical boom 3003. At this point, the operator can stow the crane and the boom is ready for use.

In an alternate embodiment of the present invention, a positioning plate 3015 is first placed into position thereby setting an exact pre-determined location for the base of the vertical boom 3003 relative to the vehicle 3010. This positioning plate 3015 may be unfolded from the side of the vehicle or it may be placed into position using the vehicle mounted crane.

In a yet another alternative embodiment of the present invention, the vertical support 3001 and the vertical boom 3003 are each hinged from their respective ends of the horizontal boom 3002 to form an assembly. The vehicle mounted crane is used to lift the assembly of three components, from stowed condition, into approximate position for deployment. With the assembly suspended on the crane, the vertical support 3001 and vertical boom 3003 are lowered from a substantially horizontal position (that they were in when stowed) to a substantially vertical position using one or more electric or manually operated winches. The “inverted U” shaped boom 3000 is then lowered into its operating position and the crane removed to its storage position. The boom 3000 is then ready for use. To stow the boom, the crane is used to lift the assembly up, the vertical support 3001 and vertical boom 3003 are winched back to a substantially horizontal aspect and the thus assembly is stored back on the vehicle 3010.

FIG. 31*a* shows still another embodiment of structure/configuration of boom 3100 in accordance with another aspect of the present invention. In this embodiment, the boom 3100 comprises four components—lower vertical



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support **3101a**, upper vertical support **3101b**, horizontal boom **3102** and vertical boom **3103**. The lower vertical support **3101a** is rigidly attached to a rotating platform **3105** while an actuator rotates the platform **3105** through 90 degrees in a plane perpendicular to the plane of the lower vertical support **3101a**. The upper vertical support **3101b** is attached to the lower vertical support **3101a** using a hinge (not shown) which can rotate the two vertical support sections by 90 degrees with respect to each other. The upper vertical support **3101b** is rigidly attached at 90 degrees to the horizontal boom **3102**. The vertical boom **3103** is hinged at the end **3122** of the horizontal boom **3102** which is farthest from the upper vertical support **3101b**. In stowed condition, the upper vertical support **3101b** is folded substantially parallel to the lower vertical support **3101a**.

To deploy the boom **3100**, the two vertical support sections **3101a**, **3101b** are unfolded into an end-to-end configuration (that is, to make a single contiguous vertical support) as shown in FIG. **31b**. The rotating platform **3105** then rotates the boom **3100** through 90 degrees such that the horizontal boom **3102** extends perpendicular to the long edge of the vehicle **3110**, as illustrated in FIG. **31c**. The vertical boom **3103** is then unfolded into the vertical direction to complete deployment of the boom, as has been depicted in FIG. **31a**. Persons of ordinary skill in the art would appreciate that the boom stow sequence is exactly opposite to the above described deployment process.

In an alternate embodiment of the present invention, the upper and lower vertical support sections **3101b**, **3101a** respectively, are replaced by a single vertical support so that the boom is deployed by simply first rotating the boom and then unfolding the vertical boom **3103**.

In another alternate embodiment of the present invention, upper vertical support **3101b** is telescopically retractable/extendable to/from the lower vertical support **3101a** as shown in FIG. **31d** and is not hinged to the lower vertical support. In other words, for deployment the upper vertical support **3101b** is simply extended vertically upwards; the platform **3105** rotated by 90 degrees and the vertical boom **3103** unfolded into vertical direction.

FIG. **32a** shows yet another embodiment of structure/configuration of boom **3200**, in stowed condition, in accordance with another aspect of the present invention. In this embodiment, the boom **3200** comprises four components—lower vertical support **3201a**, upper vertical support **3201b**, horizontal boom **3202** and vertical boom **3203** (visible in FIG. **32c**). When stowed for transport, the lower and upper vertical support sections **3201a**, **3201b** respectively, are folded back on each other with rotating joints at each of their meeting ends **3204**. The horizontal and vertical boom sections **3202**, **3203** respectively, are each folded up to each other while the horizontal boom **3202** is attached to the upper vertical support **3201b** using a pin bearing **3206**.

During deployment, an actuator is used to extend the two vertical support sections **3201a**, **3201b** from the horizontal (stowed position) to vertical position, as shown in FIG. **32b**. This causes the folded horizontal and vertical boom sections **3202**, **3203** to move from the horizontal to the vertical orientation, as illustrated in FIG. **32c**. An actuator then folds out the horizontal boom **3202** to horizontal aspect, taking the vertical boom **3203** with it. Finally, the vertical boom **3203** is lowered about its hinge point at the end **3222** of the horizontal boom **3202**. Boom stow adopts the same sequence but in reverse order.

Referring back to FIG. **32a**, in an alternate embodiment, the lower vertical support **3201a** is mounted on to a rotating platform (not shown) which can be used to set angle of the

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resultant scanning tunnel (when the boom **3200** is fully deployed) such that it is in the range, typically, of 75 to 90 degrees with respect to the long edge **3225** of the vehicle **3210**. Advantageously, X-ray source is fixed to the underside of the rotating platform so that it tracks the required beam angle.

Persons of ordinary skill in the art should note that the plurality of actuators, used for deployment or stow sequence of the boom structures of FIGS. **28** through **32** of the present invention, may be electric motor (with rotary gearbox or linear screw rod actuators), hydraulic cylinder and lever, electric winch and cable (with removable or fixed end points), manual winch and cable (with removable fixed end points) or any other actuators known to those skilled in the art. Where a rotating platform is used, boom deployment angles are adjustable in the range 75 degrees to 90 degrees with respect to the scanning direction. Also, scanning aperture of the boom structures/configurations of FIGS. **28** through **32** is typically 2000 mm (H)×2000 mm (W) minimum up to 5300 mm (H)×4000 mm (W) maximum. However, booms may alternatively be configured with a tunnel aperture outside these dimensions, such as 1000 mm (H), 3000 mm (H), 6000 mm (H), 7000 mm (H), 1000 mm (W), 3000 mm (W), 4500 mm (W), 5000 mm (W), 5500 mm (W), 6000 mm (W), 6500 mm (W), and any dimensions in between.

Again, X-ray sources may be selected from any of the following categories:

X-ray tube and generator with 100 kVp to 500 kVp tube voltage and 0.1 mA to 20 mA tube current, including X-ray sources with 160 kV and a penetration of 30 mm of steel.

0.8 MV to 2.5 MV linear accelerator source, including those sources with a low output dose rate, typically less than 0.1 Gy/min at 1 m.

2.5 MV to 6 MV linear accelerator source with high output dose rate, typically in the range 0.1 Gy/min at 1 m to 10 Gy/min at 1 m.

X-ray sources with penetration in excess of 120 mm of steel, including 180 mm of penetration and any increment therein.

X-ray sources of 450 keV with a penetration of approximately 80 mm of steel.

In one embodiment, booms of the present invention are fitted with lead or steel beam stops to reduce primary beam intensity at the extent of the surrounding radiation exclusion zone. The beam stop is advantageously formed from lead with a thickness of 10 mm to 200 mm depending on the energy of the X-ray source (the higher the energy, the thicker the primary beam stop). The booms are fitted with X-ray detectors to measure the transmitted X-rays from the source through the object under inspection. Typically these detectors are formed from high density scintillation materials such as CdWO<sub>4</sub>, ZnWO<sub>4</sub> or CsI with a thickness in the range 0.3 mm to 50 mm depending on the energy of the X-ray source and the type of transmission measurement being made.

Additionally or optionally, the booms of the present invention are fitted with position sensors to provide feedback to an automated boom deployment system. These sensors advantageously record when actuator motion is complete at both ends of travel. In one embodiment, redundant sensors are deployed for such measurements to mitigate against sensor failure.

In one embodiment for example, it is possible to complete boom deployment in less than 2 minutes. Still faster times may be achieved when suitable strengthening components



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are fitted to the various booms to mitigate actuator load. Further, boom stowage can also be completed in a similar duration of time.

The horizontal and vertical booms in the scanning system of the present invention are designed to contain as little material as possible. This allows for minimizing the weight, and hence reduces the tipping moment on the truck chassis. Several materials can be selected for manufacturing the booms, including steel, aluminum and composite materials. One of ordinary skill in the art would appreciate that other suitable light weight materials may also be used for this purpose. In one embodiment, the boom design utilizes novel lattice structures to ensure low mass in the boom. FIGS. 5a through 5d illustrate some of the exemplary low mass lattice structures which act to reduce the weight of the booms. The booms are further designed to include a light-tight, but compact housing for the X-ray detector assemblies.

Referring to FIG. 5a, a section of the boom 501a is shown in cross-section. This boom structure utilizes square profile box section components 502a, or nodes, where three such box section components 502a are physically connected by a beam section 504a. The sensor box 503a is mounted to the side of the boom structure using metal support brackets (not shown) which attach to the triangular boom section 501a.

FIG. 5b shows an alternate design in cross-section, wherein the boom has a square cross section 501b with the sensor components 503b mounted to the side and is made from four square profile box section components 502b where the components 502b are physically connected by a beam section 504b. One of ordinary skill in the art would appreciate that it would also be possible to mount the sensor box 503b within the square section 501b. This, however, would result in a weakening of the structure since the sensor box would need to form a "U" shape to allow unimpeded access of X-rays to the detectors.

FIG. 5c shows a further design in which the detector box 503c is protected within a boom section comprised of two triangular support frames 501c of the boom. Each of the triangular support frames 501c comprises three profile box section components 502c where the components 502c are physically connected by a beam section 504c. The two triangular sections are then further physically connected by beam section 505c.

FIG. 5d shows another design of the boom in which "bulkheads" 504d are mounted along the length of the boom which itself is formed from box section components 502d. The sensor box 503d in this case is encased within the boom section.

One of ordinary skill in the art would appreciate that many other structures may also be used for the boom design to fulfill the objective of low mass, including, for example, round section tubing and cast composite structures. The use of open frame lattice structures and detector enclosures such as illustrated above not only makes the boom lightweight, but also makes it less wind resistant due to flow through, while still maintaining its rigidity.

The detector box used with the boom is required to be light, tight and impervious to moisture. By way of good design, in one embodiment, the detector box is combined with the boom structure to provide additional strength while also providing good access to the detector electronics. FIG. 6 shows an exemplary design for a combined boom and detector box. Referring to FIG. 6, the boom cross section 601 is extended to include a box section 602 for the X-ray detectors by connecting a beam section 608 from one of its three profile box section components 609 where the components 609 are physically connected by beam sections 610.

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Beam section 608 physically connects to a box component 610, which then connects to a second box component 611. The detector electronics 603 are provided with removable access covers 604 on one side and a removable front cover 605 which is substantially transparent to the incoming X-rays 606. Further, a thin light-tight sheet covering 607 is provided to protect the rear side of the assembly and the side opposite to the access cover.

The lattice structures for boom and detector box illustrated in FIGS. 5 and 6 can be fabricated using any suitable technique known to persons of ordinary skill in the art. As an example, it would be advantageous to fabricate the structure shown in FIG. 6 using a welded fabrication of 50 mm×50 mm steel box section components with 2.5 mm wall thickness to which 1 mm thick steel sheet is welded to form the detector enclosure, the detector cover and the access covers. Preferably, the detector box is lined with a thermal insulation material to minimize thermal shock to the detectors due to change in ambient temperature and also to help in reducing condensation that may occur in particularly cold climates.

In one embodiment of the system of present invention, only one common engineering material is used for boom fabrication. This not only proves cost-effective, but also ensures that uneven deformation in the boom does not occur under change in ambient temperature as may be the case when multiple materials are used in a boom design.

As mentioned earlier, one objective of the present invention is to ensure a compact method of stowing the boom when not deployed. In order to fold the horizontal boom out from the vertical support for deployment, a number of mechanisms may be used. FIG. 7 presents an exemplary design for folding and unfolding boom sections, as used in one embodiment of the present invention. Referring to FIG. 7, a single hydraulic arm 701 is used to force the separation of the horizontal boom 702 from the vertical support 703. The separation is facilitated by means of an intermediate rigid coupling 704 which rotates about a point 705 on the vertical support.

In one embodiment, the unfolding action illustrated in FIG. 7 is complimented by a locking pin arrangement so that after deployment, hydraulic power can be lost without the boom folding back up. An exemplary locking mechanism is shown in FIGS. 8a and 8b. Referring to FIGS. 8a and 8b, the horizontal boom 801a is extended so that it folds back above the vertical support 802a. A dome shaped fixture 803a, 803b attached rigidly to the top of the vertical support 802a engages with locking plates 804a, 804b in the horizontal boom. The locking plates 804a, 804b are spring loaded such that they are pushed back when the boom is being folded by the dome shaped structure 803a, 803b on the vertical support 802a. Once the boom 801a is deployed fully, the locking plates 804a, 804b snap back to their resting position under the dome and the boom is locked in position. When the boom 801a is to be stowed, the locking plates 804a, 804b can be withdrawn using any suitable means, such as an electrical solenoid, electric motor, hydraulic actuator or any other device known to persons of ordinary skill in the art. A person of ordinary skill in the art would also appreciate that many other locking mechanisms may also be devised that provide a good balance between efficiency, cost and safety.

FIG. 9 shows another boom deployment structure. In this case, a first end of a support bar 901 mounts to a bearing post 902, which connects vertical support 903 to horizontal boom 904 in an angular configuration. Preferably the support bar 901 connects to the bearing post 902 at the bearing post pivot point 902a. A second end of the support bar 901 has



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integrated therein a pulley **905**, distal to the bearing **902**. A cable **906** connects to the horizontal boom **904** and passes over the pulley **905** and returns back to a winch **907** which is mounted securely onto the vertical support **903**. The winch **907** is operated during boom deployment and it acts to pull the horizontal boom **904** away from the vertical support **903**. This mechanism eliminates the need for a hydraulic actuator, although a hydraulic support **910** may be employed for safety or backup. FIG. **9** also shows a horizontal boom lock **908**, which may be used to sense when the boom deployment action has completed, so that the winch **907** can be stopped. Preferably a sensor is deployed in conjunction with the horizontal boom lock **908** to sense a locking action and transmit the sensed locking action to a controller, which then communicates a stop signal to the winch based upon the locked state.

A further enhancement of this invention is shown in FIG. **10**. Referring to FIG. **10**, the support bar **1001** is designed such that it can be rotated out of the way once the horizontal boom **1002** has been stowed with the vertical support **1003** using the mechanism of the winch **1004** and cable **1005**. As the support bar **1001** is moved away, it serves to minimize the space taken by the stowed boom.

Besides an efficient and compact folding arrangement between the vertical support and the horizontal section of the boom, the design of the present invention also incorporates a space saving folding arrangement between the horizontal boom section and vertical boom section, which is illustrated in FIGS. **11a** and **11b**. Referring to FIG. **11a**, which shows the boom in a deployed state, at the junction of the horizontal section **1101a** and vertical section **1102a**, a single folding hinge arrangement **1103a** is used. A locking pin **1104a** is also provided which engages when the booms **1101a** and **1102a** are deployed fully, and acts to minimize mechanical wobble between the two booms. A single hydraulic ram **1105a** is used to force the separation of the horizontal section **1101a** from the vertical section **1102a** when unfolding is required.

The booms in folded or stowed state are illustrated in FIG. **11b**, wherein the hydraulic ram **1105b** works in conjunction with the hinge arrangement **1103b** to fold the vertical boom **1102b** parallel to the horizontal boom **1101b**.

One of ordinary skill in the art would appreciate that the aforementioned folding arrangement between the horizontal boom and vertical boom is provided as an example only, and several other designs can be implemented successfully.

Persons of ordinary skill in the art should also note that the boom structures of the present invention allow requisite accuracy of alignment so that X-ray energy levels of less than 2 MeV can be used while also being adequate enough to penetrate 150 mm of steel, in accordance with one embodiment. Further, as a result of the use of lower X-ray energy levels, the embodiments of the present invention use smaller Linacs when compared to prior art systems, thereby saving on overall weight. As a further result of the cumulative weight savings, the present invention allows for an X-ray mobile inspection system with penetration greater than 120 mm of steel, while weighing less than 15,000 kg.

In a further aspect of this invention, the system is advantageously configured to avoid rotation of the X-ray source. This boom configuration which limits the rotation of the X-ray source is illustrated in FIGS. **12a** and **12b**. Referring to FIG. **12a**, an alternate X-ray source mounting is shown, with the boom structure in a stowed position. Here, the X-ray source **1201a** is suspended from a bracket **1202a** which is able to rotate about a point **1203a** fixed to the boom structure **1204a**. FIG. **12b** illustrates the configuration with

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the boom structure in a partially deployed position. Referring to FIG. **12b**, as the vertical support structure **1204b** is raised for boom deployment, the X-ray support bracket **1202b** lowers the X-ray source **1201b** towards its final operating point based upon a signal from a controller. This arrangement avoids the rotation of the X-ray source itself for boom deployment.

In one embodiment, the swinging movement of the X-ray source during boom deployment is also minimized by connecting a hydraulic damping system between the X-ray source bracket and the X-ray source itself. This arrangement is shown in FIGS. **13a** and **13b**. Referring to FIG. **13a**, which shows the system in an undeployed position, a hydraulic cylinder **1301a** links the X-ray support bracket **1302a** and the X-ray source **1303a**. Hydraulic cylinder **1301a** comprises fluid flow valves that are opened during boom deploy and stow, such that the cylinder can change length under the effect of gravitational pull on the X-ray source. Referring to FIG. **13b**, once the boom is deployed, the fluid valves of hydraulic cylinder **1301b** are closed, thereby locking the X-ray source **1303b** in position along with the X-ray support bracket **1302b**. One of ordinary skill in the art would appreciate that final adjustment of source position can be made by extending or retracting the hydraulic cylinder as necessary, depending on the gradient of the ground on which the main X-ray system is operating.

An alternative configuration for mounting the X-ray source is illustrated in FIGS. **14a** and **14b**. Referring to FIG. **14a**, the X-ray source **1401a** is mounted on a platform **1402a**, which is fixed rigidly to the motionless part of the rotation joint **1403a** at the base of the vertical support **1404a**. The platform **1402a** is capable of being raised and lowered for stowing and deployment respectively. Accordingly, the platform is physically slidable relative to the truck. Referring to FIG. **14b**, when the vertical support structure **1404b** is raised for boom deployment, the platform **1402b** is concurrently lowered, thereby placing the X-ray source **1401b** in its final operating position. The platform **1402b** can be moved up, down, right, or left to position the source correctly for scanning. It should be appreciated that this motion can be effectuated through a motor, engine, or hydraulic system, as is well known to persons of ordinary skill in the art.

In one embodiment, the platform on which the X-ray source is mounted is actuated using one or more hydraulic rams. Further, the hydraulic ram is operated in conjunction with a geared chain drive so that the change in length of the hydraulic ram can indirectly effect a change in position of the X-ray source relative to the boom rotation point. A mechanical arrangement is also provided to lock the relative positions of the boom and the X-ray source. One such exemplary locking mechanism is shown in FIGS. **15a** and **15b**. Referring to FIG. **15a**, which shows the system in stowed position, the vertical support section **1501a** is provided with a first locking element **1502a**, designed to mate with a corresponding, or mating, locking element or fixture **1503a** in the platform assembly **1504a**. Thus, when the boom is deployed as shown in FIG. **15b**, the first locking element **1502b** and the corresponding, or mating, locking element **1503b** are connected in a such a manner that the relative positions of the boom **1501b** and X-ray source **1504b** are fixed exactly. The locking element **1502a**, **1502b** rotates about a pivot point **1505a**, **1505b** to thereby move approximately 90 degrees and be received by the corresponding, or mating, element **1503a**, **1503b** and thereby transition from an unlocked state to a locked state. One of ordinary skill in the art would recognise that many alterna-



tive locking mechanisms are possible in addition or in place of the exemplary locking mechanism described above.

The X-ray system used with the mobile inspection system of the present invention is designed to allow use with a wide range of X-ray sources. The source of radiation may include conventional sources such as a radio-isotopic source or an X-ray tube, as well as Linear Accelerators (LINAC) or any other source known in the art capable of producing beam flux and energy sufficiently high to direct a beam to traverse the space through an object under inspection to detectors at the other side, such as a betatron. The choice of source type and its intensity and energy depends upon the sensitivity of the detectors, the radiographic density of the cargo in the space between the source and detectors, radiation safety considerations, and operational requirements, such as the inspection speed.

For example, the system of the present invention could employ source-based systems, cobalt-60 or cesium-137 and further employ the required photomultiplier tubes (PMT) as detectors. If a linear accelerator (LINAC) is optionally employed, then photodiodes and crystals are used in the detector. One of ordinary skill in the art would appreciate how to select a radiation source type, depending upon his or her inspection requirements. In one embodiment, the system is operated with a standard X-ray tube, which typically has energy in the range of 120 kVp to 450 kVp, for applications such as screening cars and small vehicles with or without passengers within the vehicle. In another embodiment, a low energy linear accelerator source, having a typical energy in the range of 0.8 MV to 2 MV, is used for the purposes of screening full size cargo in manifest verification. In yet another embodiment, a higher energy X-ray source, typically with an energy range of 2.5 MV to 6 MV, is used for scanning of full-sized containers. In this case, the image penetration capability of the X-ray source is suitable for detection of a range of illicit materials and devices including narcotics, explosives, currency, alcohol, weapons and improvised explosive devices. Those skilled in the art would further appreciate that the inspection system of the present invention may also be configured with a gamma-ray source such as Co-60 or Cs-137, to replace the X-ray source.

Regardless of whether the radiation source is an X-ray generator or a LINAC, it is mounted on the same single boom as the detector arrays, so that the need for sophisticated alignment systems each time the system is deployed is eliminated. Thus, the radiation source and detectors are substantially permanently aligned on the same single boom. The feature also allows for scanning at various degrees of offset, again without the need to realign the LINAC or X-ray generator and detectors.

The X-ray system of the present invention is further designed to operate with a very compact radiation footprint. As known in the art, X-ray scanning operates on the principle that, as X-rays pass through objects, the radiation gets attenuated, absorbed, and/or deflected owing to a number of different physical phenomena that are indicative of the nature of the material being scanned. In particular, scattering occurs when the original X-ray hits an object and is then deflected from its original path through an angle. These scatter radiations are non-directional and proportional to the total energy delivered in beam path. A narrowly collimated beam will keep the overall radiation dose minimal and therefore also reduce the amount of scatter radiation in the area surrounding the scanner, thereby reducing the "exclusion zone". The exclusion zone is an area around the scanner in which general public are not authorized to enter due to the possibility of their getting exposed to doses of radiations

scattered during the scanning process. The exclusion area is dependent upon the magnitude of current setting the intensity of the radiation source. The availability of a large enough area for the "exclusion zone" around the scanner system is one of the factors that influence the decision of positioning the mobile inspection system.

Thus, in order to achieve a compact radiation footprint, and hence a smaller exclusion zone, it is necessary to collimate the radiation beam down to a narrow fan beam of X-rays. This is illustrated in FIGS. 16a and 16b. In the embodiment shown in FIG. 16a, the X-ray beam 1601a is wide compared to the X-ray detector 1602a, so that the detector 1602a is always illuminated regardless of movement of the boom. Alternatively, as shown in FIG. 16b, the detector 1602b is wider than the illuminating beam 1601b, thereby ensuring continuous illumination at the detector regardless of movement of the boom. In either case, it is advantageous to ensure that the boom design minimizes motion between the source and sensors. The folding boom structure of the present invention can achieve this objective by mounting the X-ray source and X-ray sensors to the same folding array structure so that relative motion between the three boom assemblies (horizontal boom, vertical boom and vertical support) is minimized. In this way the X-ray source (or accelerator) and the X-ray detector are better aligned in the scanning system of the present invention, than in boom designs used with other scanning systems.

Furthermore, the X-ray system of the present invention is designed to operate in rugged conditions such as those employed in military applications. As described earlier, the compact nature of the boom design, in particular its fold-flat capability, makes the mobile inspection system of the present invention uniquely suited to military applications where it may be frequently required to transport the X-ray system in its stowed condition in aircraft or helicopters. Such frequent transportation is not feasible with other known boom configurations, where the height of the boom in its stowed condition is greater than that allowed for military transport. Further, the compact configuration lends a low center of gravity for better stability of the inspection system during road transport, as there is often a need for driving the inspection system in hilly areas, border crossings, and steep mountainous areas.

The X-ray system used with mobile inspection system of the present invention is further intended to be deployed in a variety of configurations. Some of these exemplary configurations are illustrated in FIGS. 17a through 17c. Referring to FIG. 17a, the X-ray boom structure 1701a is demounted from a vehicle or truck (not shown) and used as a standalone trailer (shown as 1702a) mounted device. The trailer mounted system of FIG. 17a, which has wheels, can be used as a scanning system by attaching the trailer to a winch system which can drag the trailer backwards and forwards along a track. Alternatively, the trailer can be fitted with a speed sensing system so that the trailer can be used to scan drive through traffic.

In an alternate configuration, illustrated in FIG. 17b, the scanning system 1701b is used as a standalone device that can be dropped off the back of a truck bed 1702b. The standalone system of FIG. 17b will normally be used in a drive through mode although it may also be used with a winch to scan unoccupied vehicles (vehicle moves through static gantry).

In a third configuration, as shown in FIG. 17c, the scanning system 1701c can be fully integrated with a truck 1702c for mobile applications. This integrated system is typically used as a drive past scanner in which the X-ray



system is driven past a stationary object at controlled speed. However, in this case, it is also possible to operate the system in a drive through mode. Here the boom base is attached directly to the truck bed or to a trailer which is then integrated with the truck bed. A suitable sensor configuration for control of the X-ray system when operating in drive through mode is shown in FIG. 14. The sensor system is used to execute two functionalities—traffic control and X-ray control.

In one embodiment, the mobile inspection vehicle **2400** of the present invention comprises an inspection pod **2405**, placed on vehicle bed **2415** along with stowed boom **2410**, as shown in the side elevation view of the vehicle **2400** of FIG. 24. The inspection pod **2405** accommodates at least one inspector who can view scanned X-ray images on a monitor while being seated facing either the front or back of the vehicle. In one embodiment, the inspection pod **2405** is sized to allow two image inspectors to be seated back to back.

Referring now to FIGS. 25a, b, the inspection pod **2505**, in one embodiment, is configured to be in retractable state and accommodated completely on-board the vehicle **2500** ready for travel as shown in the top view of FIG. 25a and in extendable state when deployed for scanning as shown in the top view of FIG. 25b. Persons of ordinary skill in the art should note that the inspection pod **2505** is sized to be comfortably accommodated on-board the vehicle **2500** such that when in retractable state it is placed next to the stowed boom **2510**. During operation, in one embodiment, when the boom **2510** is being deployed the inspection pod **2505** is also simultaneously extended thereby keeping the overall time for system deployment low.

In one embodiment, keeping in mind the overall compactness of the vehicle **2400** and the stowed boom **2410**, the inspection pod **2405** is sized at a footprint of about 2 m (L)×1 m (W)×2.5 m (H) when retracted (during travel) and of about 2 m (L)×2 m (W)×2.5 m (H) when in extended state during deployment/inspection. The sliding pod **2405** of the present invention enables a smaller footprint during travel while allowing for up to two inspectors to be seated, within, in extended state during inspection or deployment.

In an alternate embodiment of FIGS. 26a and 26b, the inspection pod **2605** is located on the mobile inspection vehicle **2600** such that the inspector is seated just above the wheel level **2615** with access to the pod **2605** through a hinged door (not shown). This configuration results in a lower overall inspection pod height. However, in this embodiment, the inspector is always seated within the pod. In the embodiment of FIGS. 25a and 25b, the placement of the pod on the vehicle along with its height allows the inspector(s) to also stand up in the pod when needed.

FIG. 27 shows a yet another embodiment of the mobile inspection vehicle **2700** of the present invention where the vehicle bed **2705**, that supports the stowed boom **2710** along with the attached X-ray source **2715** can be swiveled or rotated by a plurality of angles in the horizontal plane of the bed. In one embodiment, the bed **2705** is capable of being swiveled to angles that allow deployment of the boom **2710** at customized angles ranging from, say, 70 to 90 degrees with respect to the direction of scan. As would be evident to persons of ordinary skill in the art, the rotation of the bed **2705** is typically controlled, in one embodiment, using electric motor or hydraulic actuator with accompanying sensors to confirm rotation angle.

Referring now to FIG. 18, the sensor system comprises one or more microwave based radar speed camera **1801** mounted on the horizontal boom **1802** of the scanning

system **1800**. The use of more than one redundant sensor is advantageous in this safety critical aspect of the design. The radar sensors **1801** are used to sense the speed of a vehicle passing through the X-ray aperture of the scanning system **1800** for inspection. For maintaining accuracy of measurement, the measured speed value is updated at regular intervals. In one embodiment, the speed value is measured and updated approximately ten times a second so as to reflect the speed of the vehicle passing through the scanning system as precisely as possible. Also, for obtaining optimum scan results with a scanning system, there is generally a preferred speed at which a vehicle being scanned should pass through, however the system of present invention allows for a range of vehicle speeds. For example in one embodiment, an optimum speed for a vehicle to pass through is 8 km/h, but acceptable vehicle speeds can range between 5 km/h and 10 km/h, with optimum results.

The traffic control or the speed control mechanism of the present invention is designed to assist the driver of the vehicle being inspected to drive through the system at an acceptable speed. In one embodiment, a green traffic signal **1803** is presented to the driver when the speed of the vehicle is within acceptable range. If the driver slows down to below the lower acceptable speed limit, an amber colored up arrow **1804** is illuminated in addition to or in place of the green traffic signal **1803**. Alternatively, if the driver passes through at a speed above acceptable upper speed limit, an amber-colored down arrow **1805** is illuminated in addition to or in place of the green traffic signal **1803**.

The X-Ray control mechanism of the present invention allows for automatic determination of the frequency and energy of the X-ray beam used for illumination of the vehicle or cargo being inspected. For this purpose, the mechanism takes into account variables such as the start of the driver's cab, the end of the driver's cab, the starting point of the cargo to be inspected and the end point of cargo to be inspected. The X-ray control mechanism comprises two redundant methods for imaging the target vehicle and determining the aforementioned variables. The first method involves use of a scanning laser sensor **1806**, which forms a two dimensional image of the height above the road surface of the vehicle being inspected. The second method of imaging the vehicle involves use of a machine vision camera **1807**, which is located on the vertical support **1808**. The machine vision camera **1807** detects vision targets **1809** that are placed on the vertical boom **1810** on the opposite side. The vision targets **1809** are located such that they correspond to different parts of a cargo vehicle. Therefore, the simultaneous analysis of a number of different targets can be used to identify different parts of the vehicle driving through the inspection aperture. By combining signals from the machine vision camera **1807** and the scanning laser sensor **1806**, a robust control mechanism for switching on the X-ray beam according to the requirements can be implemented.

FIG. 19 shows an exemplary location of three vision targets (described with reference to **1809** in FIG. 18); with respect to a vehicle **1900** being inspected. In this example, the vehicle **1900** is a truck. The first target **1901** is located in line with the base of the vehicle flatbed **1901i**. The second target **1902** is located in line with the cab of the vehicle **1902i**, and the third target **1903** is located in line with the highest part of the cargo **1903i**. A vision target can comprise any material capable of being readily identified by a camera and differentially seen by a camera relative to the vehicle surface.



FIG. 20 shows the output from the scanning laser sensor (described with reference to 1806 in FIG. 18) as a function of time. Four discrete transitions are indicated, representing various parts of the vehicle being scanned. The first transition A 2001 occurs when the start of the vehicle cab is detected. The second transition B 2002 occurs when the end of the vehicle cab is detected. The third transition C 2003 occurs at the start of cargo, and the fourth transition D 2004 occurs at the end of cargo.

FIG. 20 further depicts (by means of marking with a tick) which of the three vision targets detailed in FIG. 19 will be visible at each transition 2001, 2002, 2003, 2004, as detected by the laser height scanner. Thus, as shown in FIG. 20, target3 2005, which is placed in line with highest part of the cargo, is visible during transitions A 2001, B2002 and D 2004, which indicate start of the vehicle cab, end of the vehicle cab, and end of the cargo respectively. Similarly, target2 2006, which is located in line with the cab of the vehicle, is visible during transitions B2002 and D 2004, which indicate the end of the vehicle cab and end of the cargo, respectively. Target1 2007, which is located in line with the base of the vehicle flatbed, is not visible in any of the transitions.

In one embodiment, a safety rated process logic controller (PLC) is used to control the traffic control and X-ray control mechanism. This system is illustrated in FIG. 21. A process logic controller (PLC) 2101 takes inputs regarding the vehicle speed from the radar sensors 2102, compares the values provided by the various radar sensors, and outputs traffic control signals 2103 depending on the drive-through vehicle speed. In one embodiment, the current vehicle speed is displayed on an electronic sign whose value is updated frequently, such as once per second.

The radar sensor data is also processed to provide a speed output to the X-ray system, comprising the X-ray source 2104 and the X-ray sensors 2105. The PLC 2101 changes the frequency at which each line of X-ray data is collected, in proportion to the speed of the vehicle passing through the inspection area. For example, if the system normally operates at 300 Hz at 8 km/h, the frequency is increased to 375 Hz at a drive through speed of 10 km/h and reduced to 188 Hz at a drive through speed of 5 km/h. This kind of frequency modulation in accordance with the vehicle speed results in delivery of a constant dose of radiation per unit length of the vehicle. This in turn ensures good image quality and consistent scattered radiation dose to the driver and surrounding system operators.

The PLC 2101 also receives inputs from the scanning laser sensor 2106 and the machine vision camera 2107, and controls the generation of X-Ray beam in accordance with the dimensions of the vehicle and cargo being inspected. One of ordinary skill in the art would appreciate that additional sensors can be employed in the scanning system and interfaced with the PLC 2101 to provide greater levels of safety and accuracy as required. For example, in one embodiment, a set of tire sensors can be deployed with the scanning system, which would allow the system to produce X-rays only when the driver's cab is safely past the primary X-ray beam.

It is imperative that the X-ray sensor system is designed appropriate to the application. In general, it is good practice to design a high spatial resolution sensor system, and to blur the image at the time of data display in order to create a low dose imaging system with good contrast resolution and penetration capability. This blurring can be achieved by

mixing different proportions of the sharp original image with a blurred version until a good diagnostic image is obtained for the feature of interest.

At any point in time when the radiation source is on, the detectors are snapshots of the radiation beam attenuation in the object under inspection (OUI) for a particular "slice" of the OUI. Each slice is a beam density measurement, where the density depends upon beam attenuation through the OUI. The radiation detectors convert the lateral radiation profile of the OUI into electrical signals that are processed in an image processing system, housed in the inspection trailer, while the OUI is being conducted past the source and the radiation detector.

The X-ray image processing and control system, in an exemplary embodiment, comprises computer and storage systems which record the detector snapshots and software to merge them together to form an X-ray image of the vehicle which may further be plotted on a screen or on other media. The X-ray image is viewed or automatically analyzed by OUI acquisition system such as a CRT or monitor that displays the X-ray image of the vehicle to an operator/analyst. Alternatively, the OUI acquisition systems may be a database of X-ray images of desired targets, such as automobiles, bricks or other shapes that can be compared with features in the image. As a result of this imaging, only articles that were not contained in the reference image of the container or vehicle are selectively displayed to an operator/analyst. This makes it easier to locate articles that do not correspond to a reference condition of the container or vehicle, and then to conduct a physical inspection of those articles. Also, for high-resolution applications, the electronics used to read out the detector signals may typically feature auto-zeroed, double-correlated sampling to achieve ultra-stable zero drift and low-offset-noise data acquisition. Automatic gain ranging may be used to accommodate the wide attenuation ranges that can be encountered with large containers and vehicles.

The present invention generates a graphical representation, i.e., an image, of the densities of the contents of the vehicle under inspection. This allows for easy visual interpretation of the results of the scanning of the OUI. Advantageously, the preferred software system also causes the display of a reference image simultaneously with the image generated in response to the vehicle under inspection, so that an operator of the present embodiment can easily make a visual comparison between what an object of the type being inspected should "look like", and what the OUI actually "looks like". Such "side-by-side" inspection further simplifies the detection of contraband using the present embodiment.

The present invention employs a detector configuration which provides a good compromise between image spatial resolution, contrast and penetration performance and cost. This detector configuration is schematically illustrated in FIG. 22, and is particularly useful when using a low dose, low energy X-ray source such as a linear accelerator in the energy range 0.8 MV to 2 MV. Referring to FIG. 22, a two row sensor arrangement is shown, in which both rows of sensors—2201 and 2202, are irradiated by the X-ray beam. The pulsed X-ray beam (not shown) from the linear accelerator is timed such that each X-ray pulse occurs when the object relative to the X-ray beam moves exactly by one detector spacing. This means that the two adjacent detector samples can be summed with the advantage of doubling the detected signal, while at the same time reducing the X-ray photon noise by a square root of two. This arrangement enhances the signal to noise ratio in the scanning system of



the present invention by around 40% as compared to systems using a single row of detectors.

It may be noted that when using the aforementioned detector arrangement, the design of the present invention also ensures that the boom itself is very stable, so that the X-ray beam can be collimated tightly in order to minimize the operational radiation footprint of the X-ray scanning system.

Such a detector configuration has the benefit of allowing a double drive-through rate where the vehicle moves exactly two detector widths through the X-ray beam between X-ray pulses. This can increase the nominal drive through speed from for example, 8 km/h to 16 km/h, albeit with a reduction in image penetration performance but with no reduction in spatial resolution.

Such a detector configuration has a further benefit of allowing dual-energy imaging when provided with an X-ray linear accelerator that is capable of interleaved energy operation. That is, the system can work with small and large accelerators at low and high energy. For example, two energies—of the order of 3 MV and 6 MV may be used in adjacent pulses. In one embodiment, each pulse is delivered after the object to be inspected has passed exactly one detector width through the X-ray inspection aperture. The vehicle will therefore have completely passed the detector after exactly two X-ray pulses, one at low energy and one at high energy. Although the penetration performance is somewhat compromised since only one measurement is made at each beam energy and not two, however, this information is very useful in providing materials discrimination performance.

In one embodiment, where the present invention employs dual source-based systems, it further employs the required photomultiplier tubes as detectors. In one embodiment,  $^{60}\text{Co}$  is used as a first gamma ray source and has a high specific activity of the order of 11.1 TBq (300 Ci) and a linear dimension of the active area of 6 mm. In one embodiment, the second gamma ray source is a 1.0, 1.6 or 2.0 Curie shuttered mono-energetic source of  $^{137}\text{Cs}$  gamma rays, having 662 keV energy.

In a further embodiment of the present invention, stacked detectors can be used to provide further spectral deconvolution of the X-ray beam. This is illustrated in FIG. 23. Referring to FIG. 23, one set of low energy detectors **2301** are located in the path of the X-ray beam **2302**, and a second set of detectors **2303** are shadowed from the X-ray source by the first set of detectors **2301**. In this case, the second set of detectors **2303** can see only the high energy part of the X-ray beam. This information can be effectively used to provide materials discrimination capability in the scanning system of the present invention. In another embodiment, both stacked detectors and an interleaved X-ray source may be used to provide an enhanced level of materials discrimination performance.

In one embodiment, additional collimation is advantageously provided adjacent to the detector array. This may be achieved for example, by placing thin sheets of tungsten or other suitably attenuating material parallel to the direction of the X-ray beam but orthogonal to the detector array. Such collimation acts to reduce the effect scatter created in the detector housing assembly as well as scatter generated within the object under inspection.

One of ordinary skill in the art would appreciate that spatial resolution that can be achieved in the X-ray image depends on the detector configuration chosen and on the focal spot size of the X-ray source. In one embodiment, the detectors are configured with an element size in the range of

1 mm to 10 mm and the X-ray source has a focal spot dimension in the range of 0.5 mm to 3 mm. This results in a spatial resolution generally between 1 lp/cm and 5 lp/cm.

Further, the penetration performance depends on the energy of the X-ray source. For the system of present invention, the penetration performance is typically in the range of 20-100 mm for X-ray sources below 450 kVp, between 100 mm and 200 mm for sources in the range of 450 kVp to 2 MV and between 200 mm and 400 mm for sources in the range of 2 MV to 6 MV.

In a further aspect of this invention, the X-ray imaging system is integrated with a passive gamma detection system. In this case, one or more large area detectors are located adjacent to the X-ray detector arrays in the horizontal and vertical booms and along the full length of the vertical support. This arrangement provides a large surface area for gamma-ray detection. In one embodiment, the large area gamma ray detectors are advantageously assembled from organic scintillation materials such as an organic plastic scintillator or using in-organic scintillator materials such as  $\text{NaI(Tl)}$  or  $\text{CsI(Tl)}$ . The gamma-ray detectors are advantageously also configured to allow them to be switched off while the X-ray source is switched on and then re-enabled once the X-ray beam is switched back off again. This is particularly important when using a pulsed linear accelerator source for X-ray imaging where the gamma-ray detectors can be rendered inactive during the X-ray pulse and re-activated immediately following the pulse.

In another configuration, the secondary detectors can provide a simultaneous backscatter imaging capability. In this case, X-rays from the main imaging beam may backscatter into a series of detectors which are mounted upon the vertical support. In one embodiment, the detectors may be provided with additional collimation in order to restrict the direction from which backscattered radiation is received. The backscatter image, being correlated in spatial position with the X-ray transmission image, can provide additional information about the presence, or otherwise, of low atomic number materials that are located at, or near to, the surface of the object under inspection adjacent to the X-ray source.

The novel design and the aforementioned features of the present invention enable a cost-effective, safe and completely self-contained scanning system that can be used for non-intrusive inspection of containers, trucks and passenger vehicles. The road mobile configuration and low weight design of the present scanning system allows for transport on difficult terrain, such as in border areas, apart from local roads and highways. Further, since the system takes a very short time (around 15 minutes) to be fully deployed, and there is less operational space required for deployment, it facilitates operation at multiple locations and is efficient at performing high throughput inspections. The system can scan cargo in mobile and stationary mode and the minimal operating area makes it well suited for limited space applications. Some of the other features and benefits of the mobile inspection system of the present invention are:

The boom design allows for more precise linear accelerator to detector alignment. The folded array detector box configuration shortens the distance between X-ray source and the detector, which increases penetration and provides no corner cutoff with less image distortion.

The unique scanning boom assembly can be deployed at either a ninety or a eighty degree offset to the vehicle inspected. This allows maximum flexibility in the setup of operational area while providing excellent hidden compartment and false wall detection capabilities.



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One person may deploy the boom with a single button; thus the system is safe, reliable and simple. Stowing the boom is done in the same manner.

The scanning system includes a plurality of CCTV cameras, which provide a view of the operating zone and help maintain safety.

Two modes of operation are supported—Mobile and Portal, which allow for inspection of stationary as well as moving cargos, respectively.

A training mode is provided, which offers images from a training library for simulated scans during inspector training.

The modular design of the scanning boom assembly and imaging system allows it to be easily adapted to truck chassis from several different manufacturers. This allows local trucks to be utilized in various countries and simplifies vehicle maintenance.

The above examples are merely illustrative of the many applications of the system of present invention. Although only a few embodiments of the present invention have been described herein, it should be understood that the present invention might be embodied in many other specific forms without departing from the spirit or scope of the invention. For example, other configurations of cargo, tires, tankers, doors, airplane, packages, boxes, suitcases, cargo containers, automobile semi-trailers, tanker trucks, railroad cars, and other similar objects under inspection can also be considered. Therefore, the present examples and embodiments are to be considered as illustrative and not restrictive, and the invention is not to be limited to the details given herein, but may be modified within the scope of the appended claims.

We claim:

1. An inspection system comprising:

a vehicle having a bed defining a horizontal surface;

a boom attached to said vehicle wherein said boom comprises a lower vertical support section, an upper vertical support section, a horizontal boom section and a second vertical boom section, wherein said lower and upper vertical support sections are movably attached to each other and wherein the lower vertical support section is mounted on to a platform such that an angle of a resultant scanning tunnel when the boom is fully deployed is in an angular range of 75 to 90 degrees with respect to said horizontal surface of the vehicle;

a radiological source rotatably attached to the lower vertical support section to produce a radiation beam for scanning at said angular range; and

an array of detectors attached to at least one of said sections of the boom, wherein the array of detectors remain stationary and aligned with the radiological source during the scanning operation.

2. The system of claim 1, wherein said platform is configured to be rotatable.

3. The system of claim 1, wherein said lower and upper vertical support sections are configured to be folded against each other when the boom is stowed.

4. The system of claim 1, wherein said second vertical boom section is hinged to said horizontal boom section.

5. The system of claim 1, wherein said horizontal and second vertical boom sections are configured to be folded against each other when the boom is stowed.

6. The system of claim 1, wherein the horizontal boom section is attached to the upper vertical support section using a pin bearing.

7. The system of claim 1, wherein a boom deployment angle is adjustable in the angular range of 75 degrees to 90 degrees with respect to a scanning direction.

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8. The system of claim 1, wherein said radiological source is an X-ray source is at least one of an X-ray generator with 100 kVp to 500 kVp tube voltage and 0.1 mA to 20 mA tube current, a 0.8 MV to 2.5 MV linear accelerator source with a dose output rate of less than 0.1 Gy/min at 1 m, and a 2.5 MV to 6 MV linear accelerator source with an output dose rate in a range 0.1 Gy/min at 1 m to 10 Gy/min at 1 m.

9. The system of claim 1, wherein said boom comprises X-ray detectors to measure a plurality of transmitted X-rays from the radiological source through an object under inspection.

10. The system of claim 1, wherein said boom comprises position sensors to provide feedback to an automated boom deployment system.

11. An inspection system comprising:

a vehicle having a first axle proximate to a front of said vehicle and at least one rear axle proximate to a back of said vehicle;

a boom attached to said vehicle wherein said boom has a weight and comprises a lower vertical support section, an upper vertical support section, a horizontal boom section and a second vertical boom section, wherein said lower and upper vertical support sections are pivotably attached to each other and wherein the lower vertical support section is mounted on to a platform such that an angle of a resultant scanning tunnel when the boom is fully deployed is in an angular range of 75 to 90 degrees with respect to said vehicle;

a radiological source rotatably attached to the lower vertical support section to produce a radiation beam for scanning at said angle; and

an array of detectors attached to at least one of said sections of the boom, wherein the array of detectors remain stationary and aligned with the radiological source during said scanning operation.

12. The system of claim 11, wherein said platform is adapted to rotate.

13. The system of claim 11, wherein said lower and upper vertical support sections are folded against each other when the boom is stowed.

14. The system of claim 11, wherein said second vertical boom section is hinged to said horizontal boom section.

15. The system of claim 11, wherein said horizontal and second vertical boom sections are folded against each other when the boom is stowed.

16. The system of claim 11, wherein the horizontal boom section is attached to the upper vertical support section using a pin bearing.

17. The system of claim 11, wherein a plurality of angles defining a boom deployment are adjustable in the angular range of 75 degrees to 90 degrees with respect to a scanning direction.

18. The system of claim 11, wherein said system is configured to achieve radiological penetration of at least 30 mm of steel.

19. The system of claim 11 wherein a first area is bounded by the rear axle extending to the front of said vehicle and a second area is bounded by the rear axle extending to the back of said vehicle and wherein a weight of the boom is positioned to be over said first area and not said second area and wherein said system weighs 25,000 kg or less.

20. The system of claim 11, wherein said boom has a lattice structure comprising a plurality of beam sections connected by a plurality of nodes, wherein said structure defines an internal lattice area.